

Anlage: Meßergebnisse des
Versuchskörpers SETMQ 1

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- | | |
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A

Belastungsprotokoll

SCHNITTGRÖSSEN

BEANSPRUCHUNG INFOLGE P (1. ZEILE) UND P+G (2. ZEILE)

BLATT 1

| SCHNITT NR. | | | | | | | | | | |
|-------------|-----------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|----------------|--------------------|----------------|
| I | | | | III | | V | | | VII | |
| M/MU | T KN*M | M KN*M | Q KN | M KN*M | Q KN | M KN*M | QL KN | QR KN | M KN*M | Q KN |
| 0.000 | 0.000 | 0.000 7.920 | 0.000 14.400 | 0.000 17.100 | 0.000 10.080 | 0.000 23.040 | 0.000 5.760 | 0.000 5.760 | 0.000 25.920 | 0.000 0.000 |
| 0.114 | 0.000 | 20.000 27.920 | 40.000 54.400 | 50.000 67.100 | 40.000 50.080 | 80.000 103.040 | 40.000 45.760 | 0.000 5.760 | 80.000 105.920 | 0.000 0.000 |
| 0.229 | 0.000 | 40.000 47.920 | 80.000 94.400 | 100.000 117.100 | 80.000 90.080 | 160.000 183.040 | 80.000 85.760 | 0.000 5.760 | 160.000 185.920 | 0.000 0.000 |
| 0.229/ 1 | 0.000 | 40.000 47.920 | 80.000 94.400 | 100.000 117.100 | 80.000 90.080 | 160.000 183.040 | 80.000 85.760 | 0.000 5.760 | 160.000 185.920 | 0.000 0.000 |
| 0.343 | 0.000 | 60.000 67.920 | 120.000 134.400 | 150.000 167.100 | 120.000 130.080 | 240.000 263.040 | 120.000 125.760 | 0.000 5.760 | 240.000 265.920 | 0.000 0.000 |
| 0.400 | 0.000 | 70.000 77.920 | 140.000 154.400 | 175.000 192.100 | 140.000 150.080 | 280.000 303.040 | 140.000 145.760 | 0.000 5.760 | 280.000 305.920 | 0.000 0.000 |
| 0.457 | 0.000 | 80.000 87.920 | 160.000 174.400 | 200.000 217.100 | 160.000 170.080 | 320.000 343.040 | 160.000 165.760 | 0.000 5.760 | 320.000 345.920 | 0.000 0.000 |
| 0.514 | 0.000 | 90.000 97.920 | 180.000 194.400 | 225.000 242.100 | 180.000 190.080 | 360.000 383.040 | 180.000 185.760 | 0.000 5.760 | 360.000 385.920 | 0.000 0.000 |
| 0.571 | 0.000 | 100.000 107.920 | 200.000 214.400 | 250.000 267.100 | 200.000 210.080 | 400.000 423.040 | 200.000 205.760 | 0.000 5.760 | 400.000 425.920 | 0.000 0.000 |
| 0.629 | 0.000 | 110.000 117.920 | 220.000 234.400 | 275.000 292.100 | 220.000 230.080 | 440.000 463.040 | 220.000 225.760 | 0.000 5.760 | 440.000 465.920 | 0.000 0.000 |
| 0.686 | 0.000 | 120.000 127.920 | 240.000 254.400 | 300.000 317.100 | 240.000 250.080 | 480.000 503.040 | 240.000 245.760 | 0.000 5.760 | 480.000 505.920 | 0.000 0.000 |
| 0.743 | 0.000 | 130.000 137.920 | 260.000 274.400 | 325.000 342.100 | 260.000 270.080 | 520.000 543.040 | 260.000 265.760 | 0.000 5.760 | 520.000 545.920 | 0.000 0.000 |
| 0.800 | 0.000 | 140.000 147.920 | 280.000 294.400 | 350.000 367.100 | 280.000 290.080 | 560.000 583.040 | 280.000 285.760 | 0.000 5.760 | 560.000 585.920 | 0.000 0.000 |
| 0.857 | 0.000 | 150.000 157.920 | 300.000 314.400 | 375.000 392.100 | 300.000 310.080 | 600.000 623.040 | 300.000 305.760 | 0.000 5.760 | 600.000 625.920 | 0.000 0.000 |
| 0.000/ 1 | 0.000 | 0.000 7.920 | 0.000 14.400 | 0.000 17.100 | 0.000 10.080 | 0.000 23.040 | 0.000 5.760 | 0.000 5.760 | 0.000 25.920 | 0.000 0.000 |

| SCHNITT NR. | | | | | | | | | | |
|-------------|-----------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|----------------|--------------------|----------------|
| I | | | III | | | V | | | VII | |
| M/MU | T KN*M | M KN*M | Q KN | M KN*M | Q KN | M KN*M | QL KN | QR KN | M KN*M | Q KN |
| 0.000/ 2 | 0.000 | 0.000 7.920 | 0.000 14.400 | 0.000 17.100 | 0.000 10.080 | 0.000 23.040 | 0.000 5.760 | 0.000 5.760 | 0.000 25.920 | 0.000 0.000 |
| 0.857/ 1 | 0.000 | 150.000 157.920 | 300.000 314.400 | 375.000 392.100 | 300.000 310.080 | 600.000 623.040 | 300.000 305.760 | 0.000 5.760 | 600.000 625.920 | 0.000 0.000 |
| 0.857/ 2 | 16.000 | 150.000 157.920 | 300.000 314.400 | 375.000 392.100 | 300.000 310.080 | 600.000 623.040 | 300.000 305.760 | 0.000 5.760 | 600.000 625.920 | 0.000 0.000 |
| 0.857/ 3 | 32.000 | 150.000 157.920 | 300.000 314.400 | 375.000 392.100 | 300.000 310.080 | 600.000 623.040 | 300.000 305.760 | 0.000 5.760 | 600.000 625.920 | 0.000 0.000 |
| 0.857/ 4 | 48.000 | 150.000 157.920 | 300.000 314.400 | 375.000 392.100 | 300.000 310.080 | 600.000 623.040 | 300.000 305.760 | 0.000 5.760 | 600.000 625.920 | 0.000 0.000 |
| 0.857/ 5 | 64.000 | 150.000 157.920 | 300.000 314.400 | 375.000 392.100 | 300.000 310.080 | 600.000 623.040 | 300.000 305.760 | 0.000 5.760 | 600.000 625.920 | 0.000 0.000 |
| 0.857/ 6 | 80.000 | 150.000 157.920 | 300.000 314.400 | 375.000 392.100 | 300.000 310.080 | 600.000 623.040 | 300.000 305.760 | 0.000 5.760 | 600.000 625.920 | 0.000 0.000 |
| 0.686/ 1 | 80.000 | 120.000 127.920 | 240.000 254.400 | 300.000 317.100 | 240.000 250.080 | 480.000 503.040 | 240.000 245.760 | 0.000 5.760 | 480.000 505.920 | 0.000 0.000 |
| 0.571/ 1 | 80.000 | 100.000 107.920 | 200.000 214.400 | 250.000 267.100 | 200.000 210.080 | 400.000 423.040 | 200.000 205.760 | 0.000 5.760 | 400.000 425.920 | 0.000 0.000 |
| 0.400/ 1 | 80.000 | 70.000 77.920 | 140.000 154.400 | 175.000 192.100 | 140.000 150.080 | 280.000 303.040 | 140.000 145.760 | 0.000 5.760 | 280.000 305.920 | 0.000 0.000 |
| 0.400/ 2 | 96.000 | 70.000 77.920 | 140.000 154.400 | 175.000 192.100 | 140.000 150.080 | 280.000 303.040 | 140.000 145.760 | 0.000 5.760 | 280.000 305.920 | 0.000 0.000 |
| **0.400/ 3 | 112.000 | 70.000 77.920 | 140.000 154.400 | 175.000 192.100 | 140.000 150.080 | 280.000 303.040 | 140.000 145.760 | 0.000 5.760 | 280.000 305.920 | 0.000 0.000 |
| * 0.100 | 112.000 | 17.500 25.420 | 35.000 49.400 | 43.750 60.850 | 35.000 45.080 | 70.000 93.040 | 35.000 40.760 | 0.000 5.760 | 70.000 95.920 | 0.000 0.000 |
| 0.000/ 3 | 0.000 | 0.000 7.920 | 0.000 14.400 | 0.000 17.100 | 0.000 10.080 | 0.000 23.040 | 0.000 5.760 | 0.000 5.760 | 0.000 25.920 | 0.000 0.000 |
| 0.000/ 4 | 0.000 | 0.000 7.920 | 0.000 14.400 | 0.000 17.100 | 0.000 10.080 | 0.000 23.040 | 0.000 5.760 | 0.000 5.760 | 0.000 25.920 | 0.000 0.000 |
| 0.000/ 5 | 0.000 | 0.000 7.920 | 0.000 14.400 | 0.000 17.100 | 0.000 10.080 | 0.000 23.040 | 0.000 5.760 | 0.000 5.760 | 0.000 25.920 | 0.000 0.000 |
| 0.429 | 0.000 | 75.000 82.920 | 150.000 164.400 | 187.500 204.600 | 150.000 160.080 | 300.000 323.040 | 150.000 155.760 | 0.000 5.760 | 300.000 325.920 | 0.000 0.000 |

BLATT 3

★★ = OBERLAST DER DYNAMISCHEN BEANSPRUCHUNG

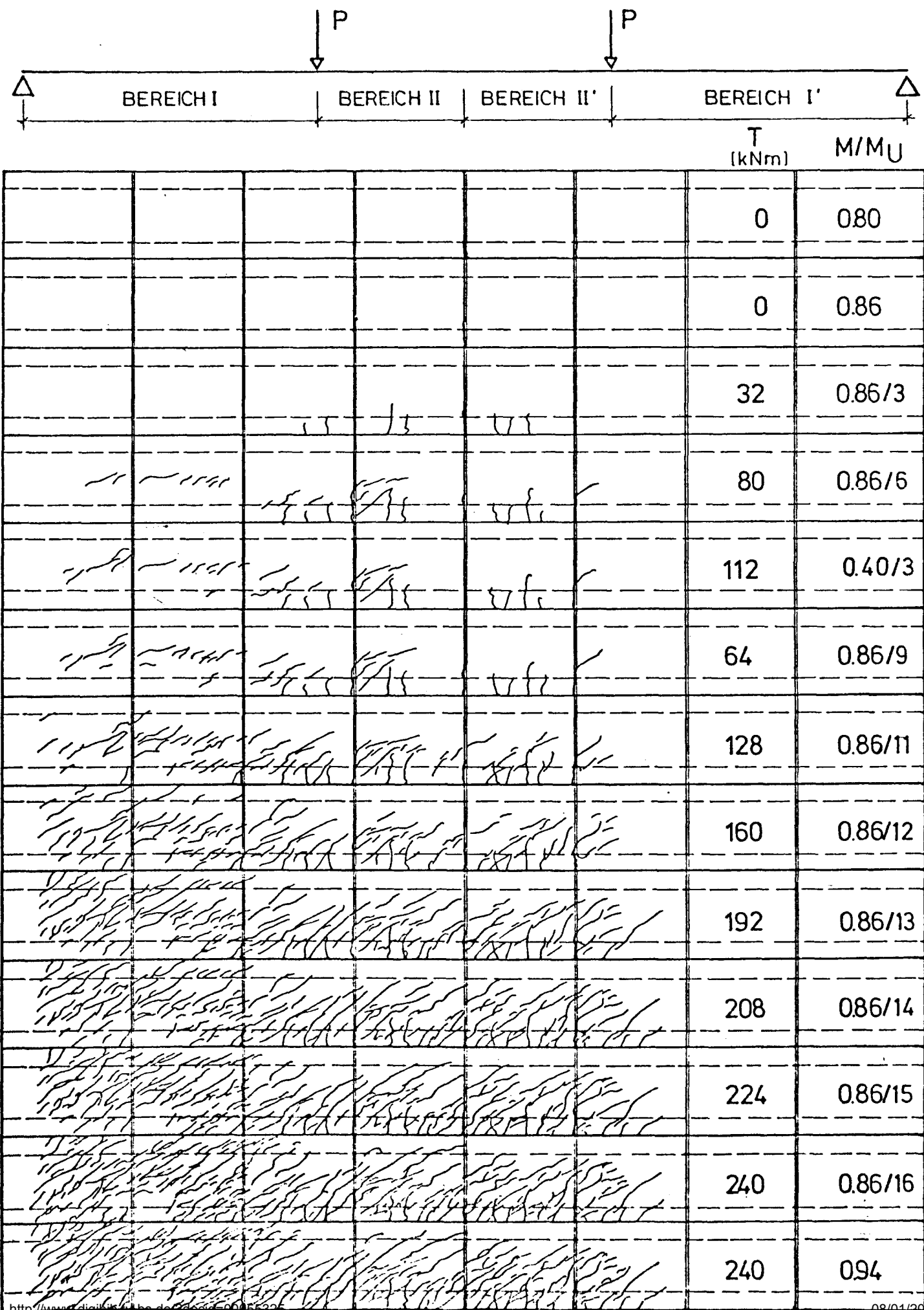
10000 LASTWECHSEL

* = UNTERLAST DER DYNAMISCHEN BEANSPRUCHUNG

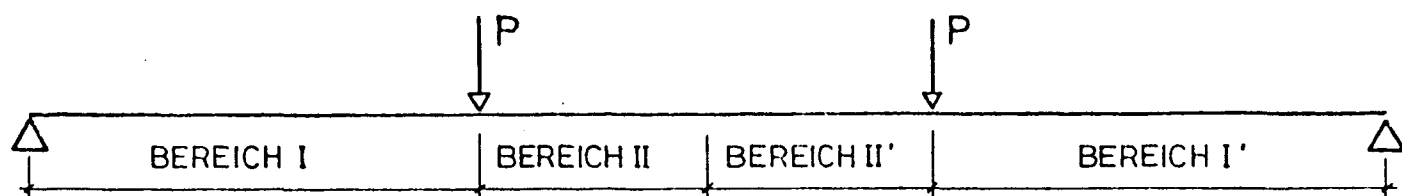
B

Rißbilder und -weiten

RISSENTWICKLUNG DES VERSUCHSBALKENS SETMQ1 VORN

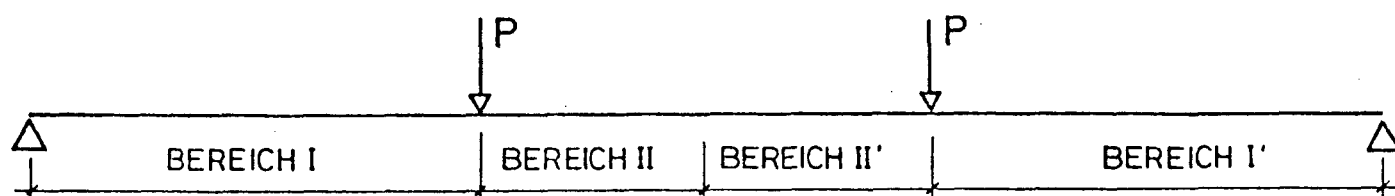


RISSENTWICKLUNG DES VERSUCHSBALKENS SETMQ 1 HINTEN



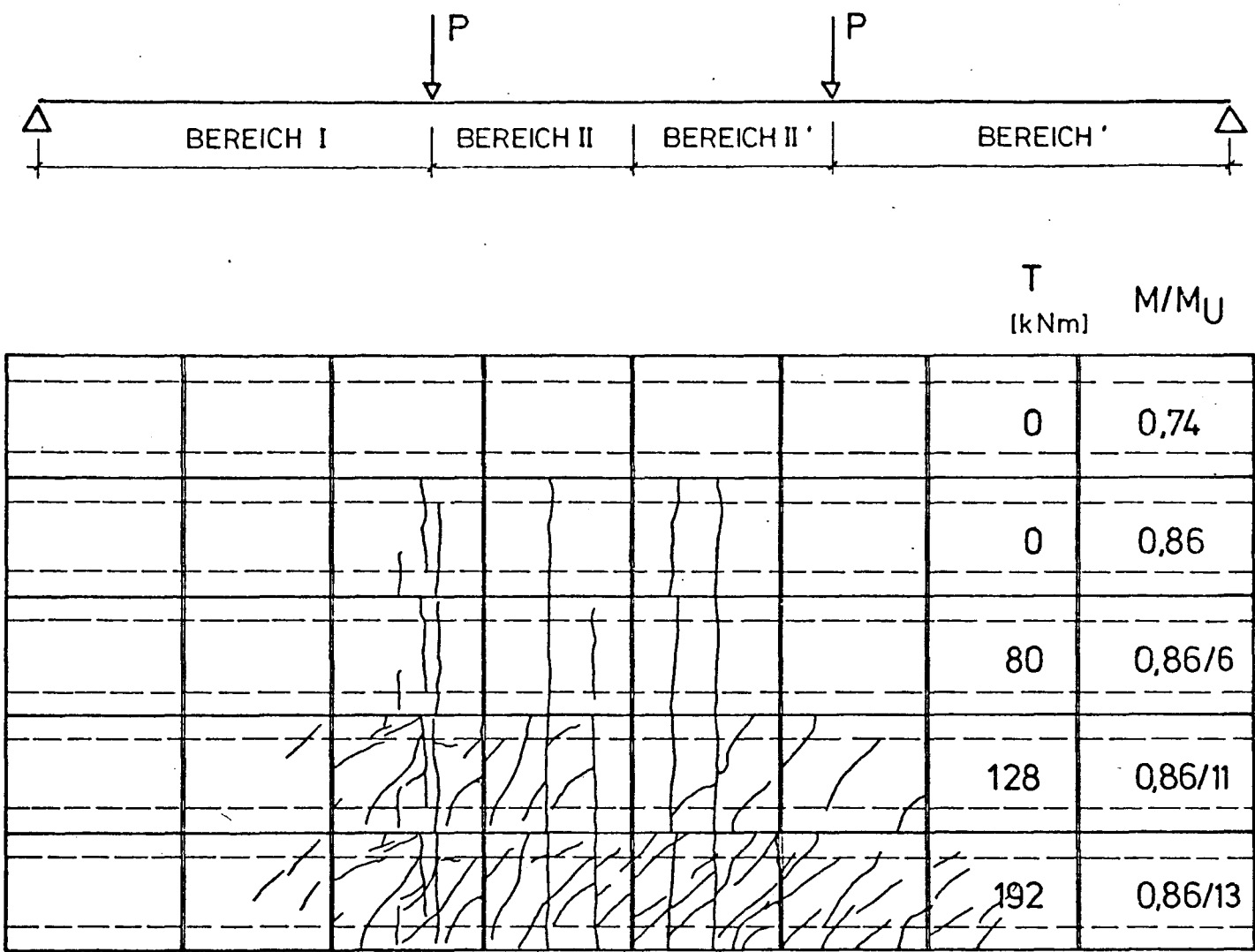
| | | | | | | T [kNm] | M/M_U |
|--|--|--|--|--|--|--------------|---------|
| | | | | | | 0 | 0,8 |
| | | | | | | 0 | 0,86 |
| | | | | | | 32 | 0,86/3 |
| | | | | | | 80 | 0,86/6 |
| | | | | | | 112 | 0,40/3 |
| | | | | | | 64 | 0,86/9 |
| | | | | | | 128 | 0,86/11 |
| | | | | | | 160 | 0,86/12 |
| | | | | | | 192 | 0,86/13 |
| | | | | | | 208 | 0,86/14 |
| | | | | | | 224 | 0,86/15 |
| | | | | | | 240 | 0,86/16 |
| | | | | | | 240 | 0,94 |

RISSENTWICKLUNG DES VERSUCHSBALKENS SETMQ1 OBEN



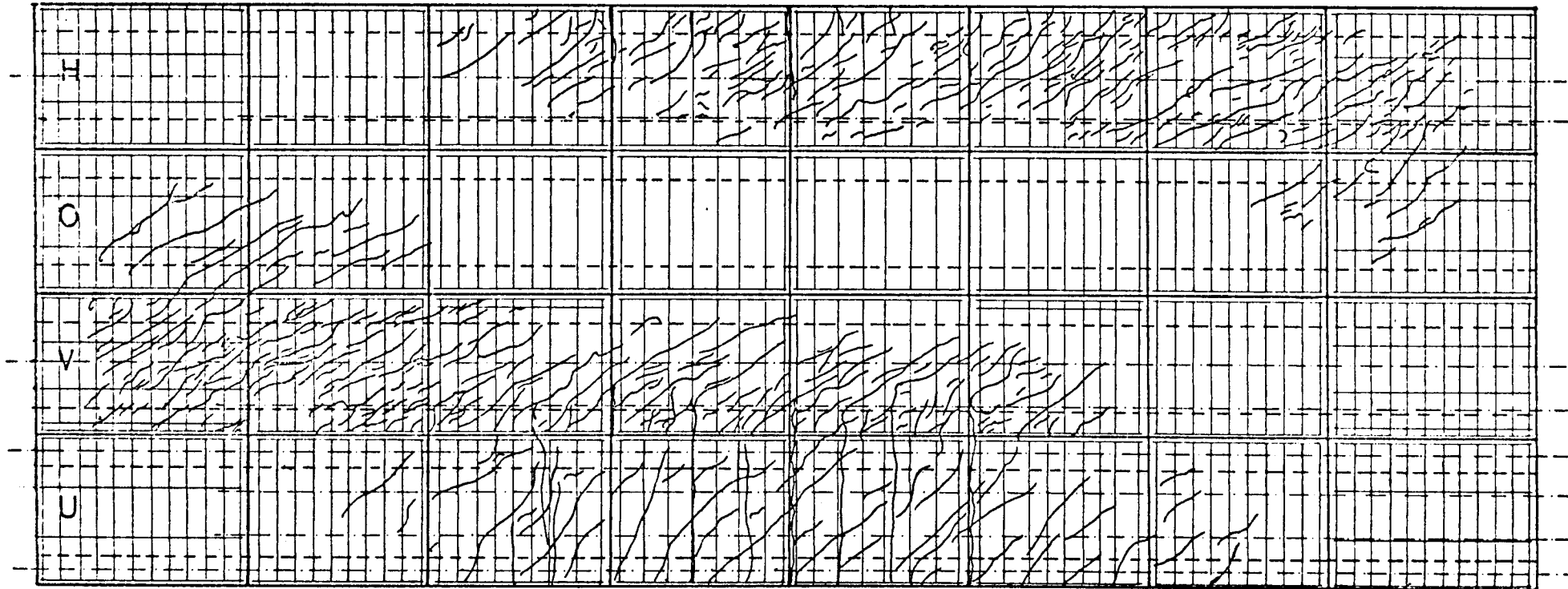
| | | | | T [kNm] | M/M _U | | |
|--|--|--|--|------------|------------------|--|--|
| | | | | 160 | 0,86/12 | | |
| | | | | 192 | 0,86/13 | | |
| | | | | 208 | 0,86/14 | | |
| | | | | 224 | 0,86/15 | | |
| | | | | 240 | 0,86/16 | | |

RISSENTWICKLUNG DES VERSUCHSBALKENS SETMQ1 UNTEN

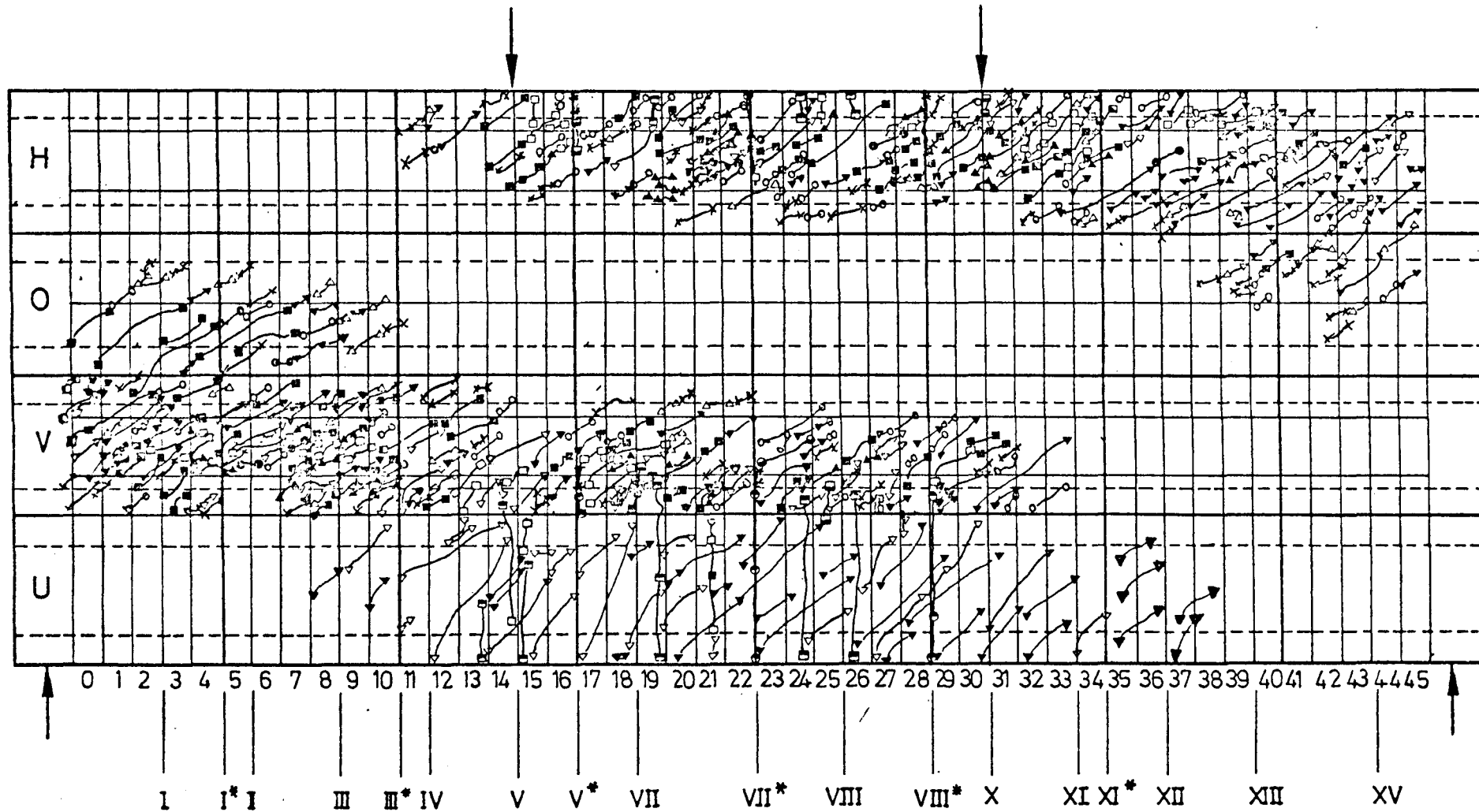


Rißbild des Versuchsbalkens SETMQ 1

mit Bewehrungsanordnung



RISSBILD DES VERSUCHSBALKENS SETMQ 1



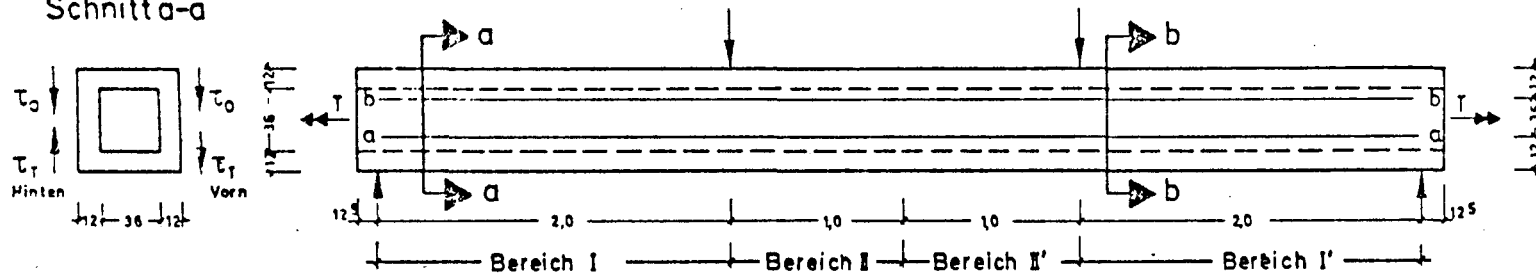
LEGENDE

M/M_U

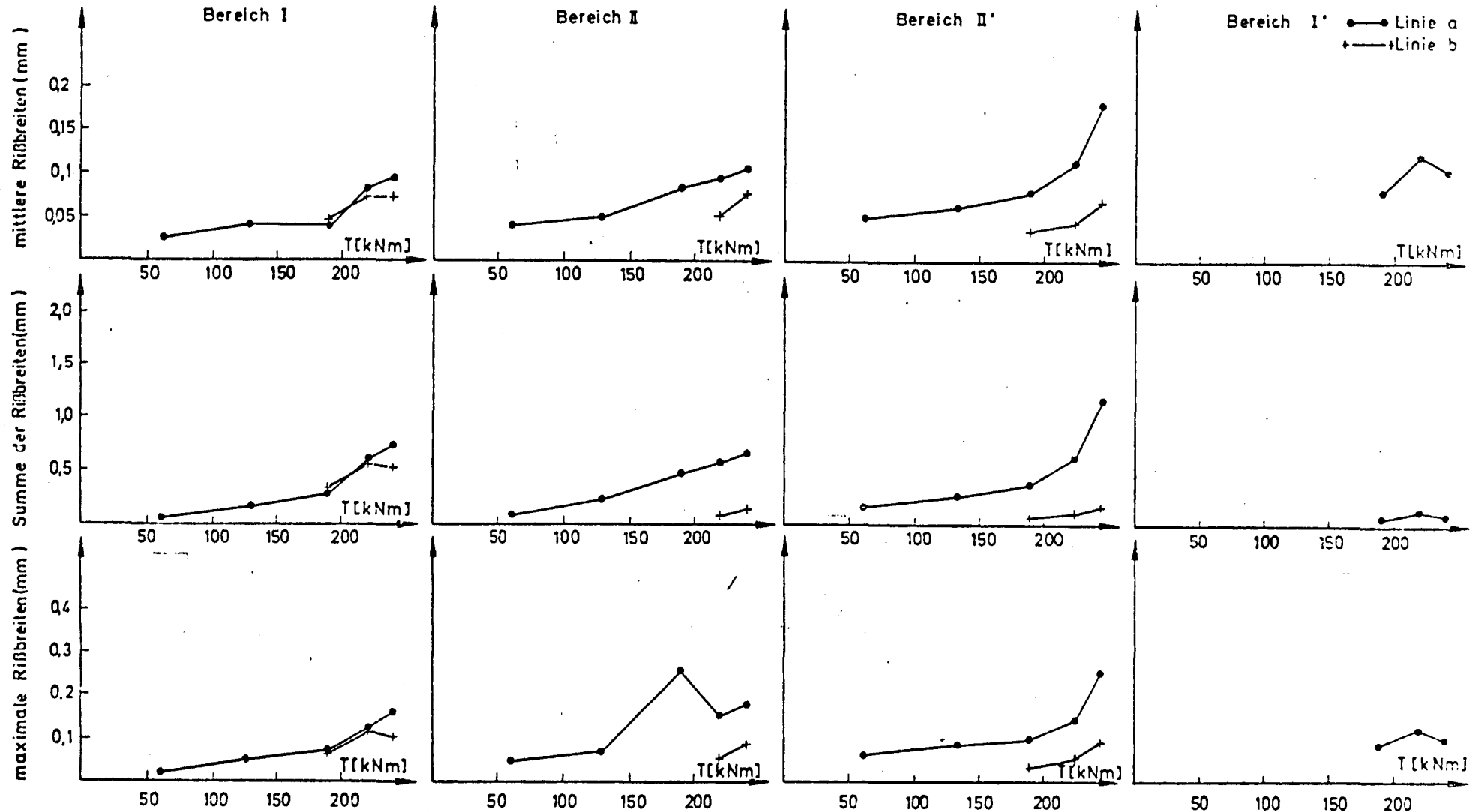
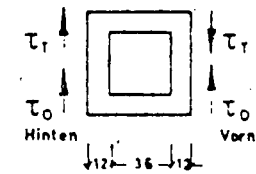
- 0,743
- × 0,800
- 0,857
- 0,857/1
- 0,857/3
- 0,857/6
- 0,400/1
- 0,400/3
- 0,857/9
- ▲ 0,857/10
- ▼ 0,857/11
- 0,857/12
- ▼ 0,857/13
- 0,857/14
- ▲ 0,857/15
- × 0,857/16
- 0,943

Gemessene Rißbreiten des Versuchsbalkens SETMQ1 an der Hinterseite

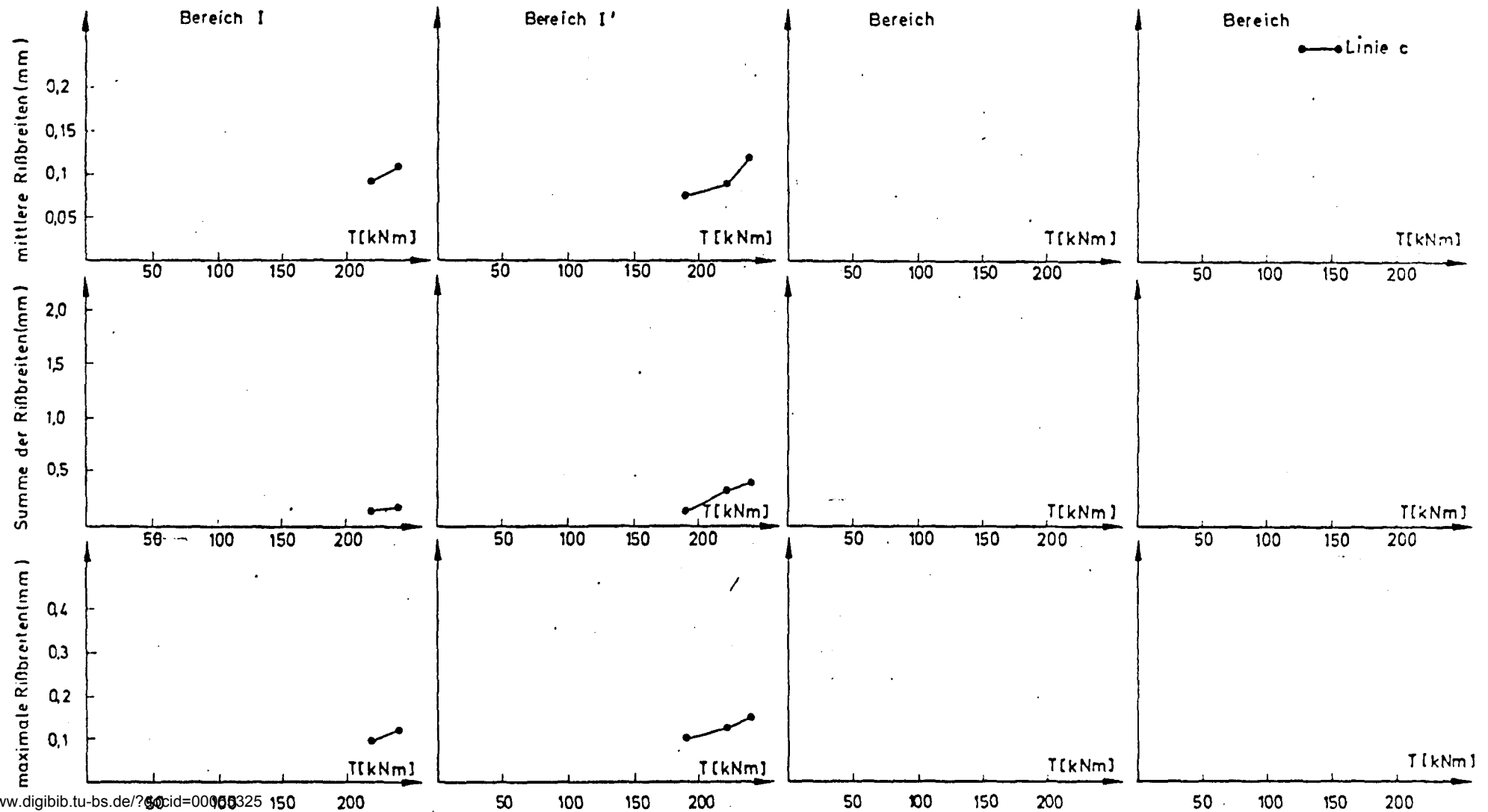
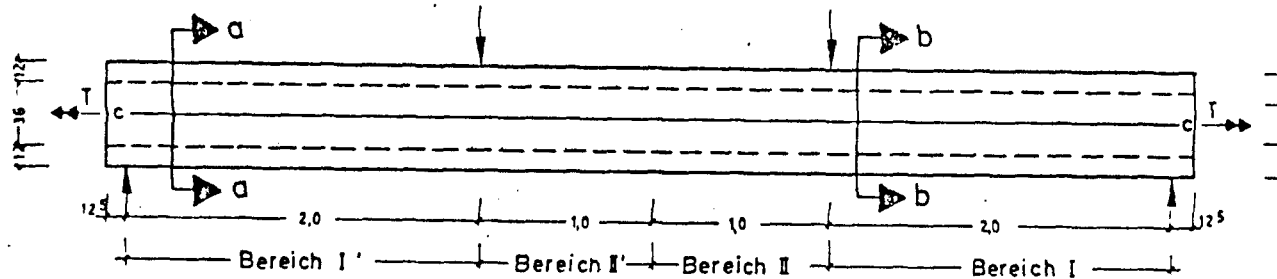
Schnitt a-a



Schnitt b-b

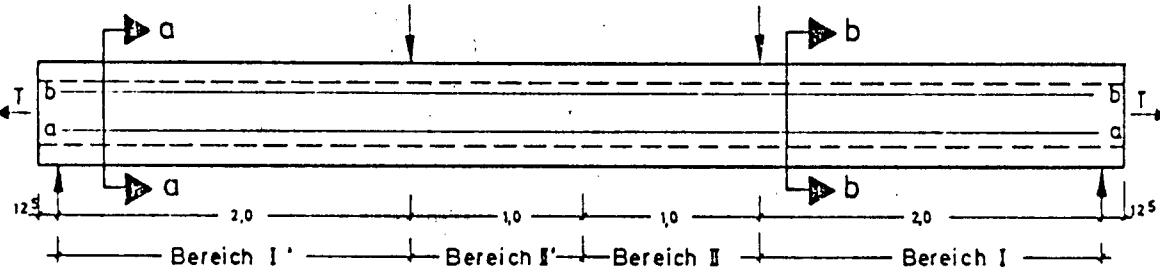
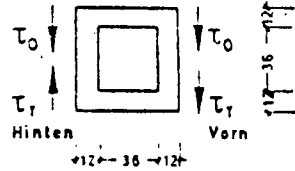


Gemessene Rißbreiten des Versuchsbalkens SETMQ1 an der Oberseite

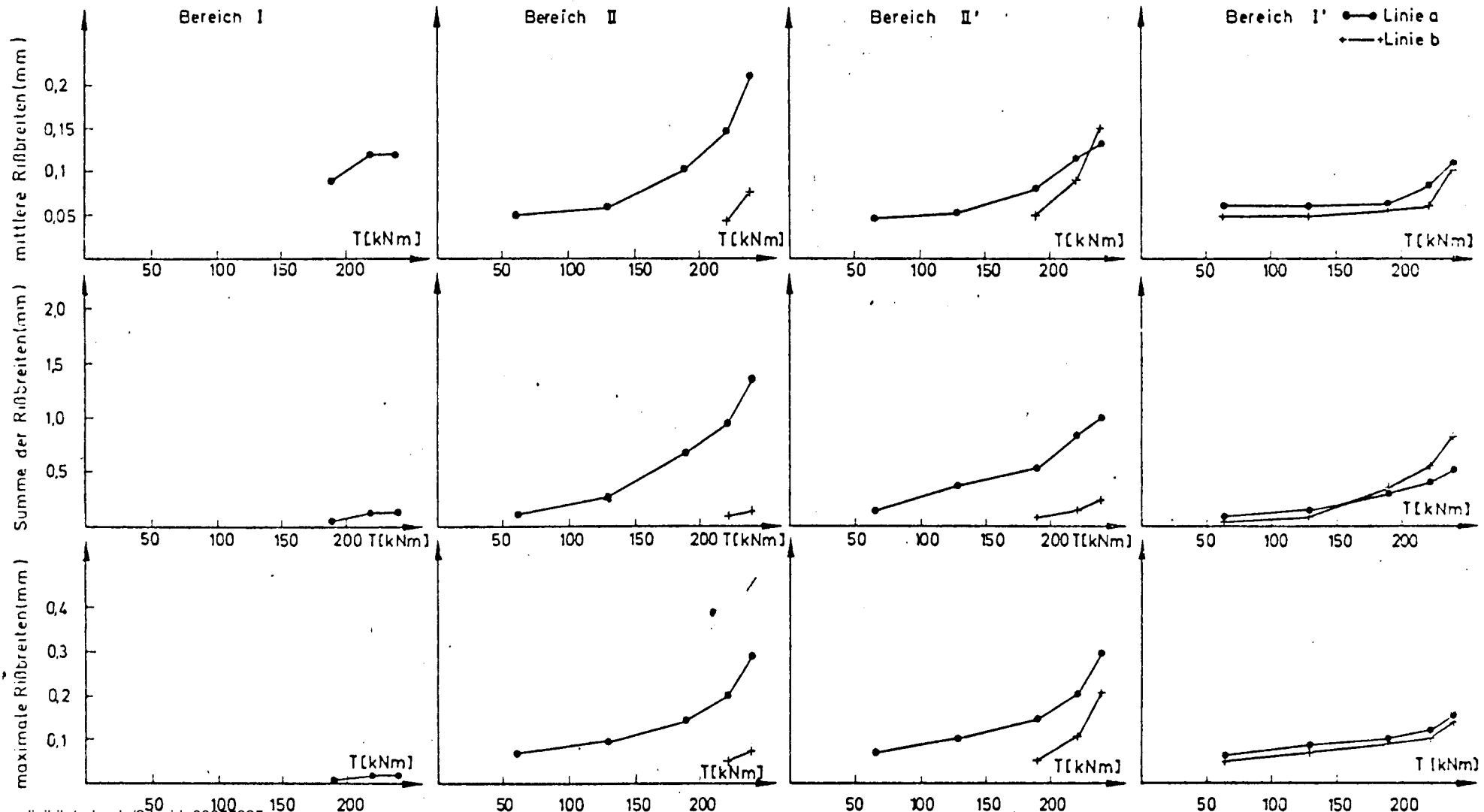
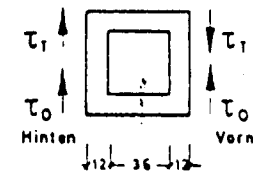


Gemessene Rißbreiten des Versuchsbalkens SETMQ1 an der Vorderseite

Schnitt a-a



Schnitt b-b



C Dehnungen der Bewehrung (Tabellenform)

SUCHSBALKEN SETMQ 1 GEPRUEFT AM 19. 5. 1978

MITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 1

BELASTUNGSGRAD M/MU

| STELLE | 0.000 | 0.114 | 0.229 | 0.229 | 0.343 | 0.457 | 0.514 | 0.571 | 0.629 | 0.686 | 0.743 | 0.800 | 0.857 | 0.000 | 0.857 |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | | | ----- | | | | | | | | | | ----- | ----- |
| | | | | 1 | | | | | | | | | | 1 | 1 |
| 1 | -0.187 | -0.183 | -0.183 | -0.177 | -0.161 | -0.169 | -0.165 | -0.155 | -0.151 | -0.161 | -0.148 | -0.155 | -0.148 | -0.183 | -0.203 |
| 2 | -0.185 | -0.185 | -0.169 | -0.175 | -0.159 | -0.167 | -0.161 | -0.151 | -0.146 | -0.155 | -0.142 | -0.149 | -0.142 | -0.181 | -0.195 |
| 3 | -0.185 | -0.181 | -0.165 | -0.183 | -0.173 | -0.163 | -0.173 | -0.157 | -0.153 | -0.155 | -0.151 | -0.144 | -0.151 | -0.191 | -0.192 |
| 4 | -0.209 | -0.205 | -0.195 | -0.213 | -0.191 | -0.199 | -0.201 | -0.195 | -0.193 | -0.213 | -0.195 | -0.211 | -0.195 | -0.215 | -0.251 |
| 7 | -0.187 | -0.203 | -0.173 | -0.181 | -0.165 | -0.173 | -0.171 | -0.159 | -0.157 | -0.169 | -0.157 | -0.165 | -0.159 | -0.187 | -0.212 |
| 9 | -0.166 | -0.187 | -0.158 | -0.166 | -0.156 | -0.168 | -0.166 | -0.160 | -0.158 | -0.170 | -0.162 | -0.170 | -0.168 | -0.166 | -0.225 |
| 11 | -0.177 | -0.191 | -0.155 | -0.163 | -0.145 | -0.143 | -0.134 | -0.114 | -0.095 | -0.081 | -0.042 | -0.017 | 0.018 | -0.021 | 0.000 |
| 12 | -0.191 | -0.191 | -0.173 | -0.183 | -0.165 | -0.169 | -0.163 | -0.148 | -0.136 | -0.138 | -0.111 | -0.101 | -0.068 | -0.132 | -0.092 |
| 13 | -0.175 | -0.177 | -0.159 | -0.169 | -0.157 | -0.163 | -0.159 | -0.149 | -0.145 | -0.155 | -0.143 | -0.147 | -0.136 | -0.163 | -0.183 |
| 14 | -0.109 | -0.093 | -0.089 | -0.091 | -0.087 | -0.077 | -0.077 | -0.079 | -0.077 | -0.075 | -0.077 | -0.073 | -0.073 | -0.075 | -0.074 |
| 15 | -0.037 | -0.039 | -0.041 | -0.037 | -0.035 | -0.031 | -0.031 | -0.035 | -0.035 | -0.035 | -0.037 | -0.035 | -0.037 | -0.015 | -0.040 |
| 16 | -0.205 | -0.217 | -0.254 | -0.240 | -0.260 | -0.281 | -0.289 | -0.299 | -0.310 | -0.314 | -0.324 | -0.332 | -0.343 | -0.195 | -0.351 |
| 19 | -0.244 | -0.250 | -0.267 | -0.267 | -0.283 | -0.295 | -0.308 | -0.318 | -0.328 | -0.338 | -0.349 | -0.357 | -0.365 | -0.232 | -0.372 |
| 22 | 2.507 | 2.499 | 2.501 | 2.489 | 2.491 | 2.505 | 2.493 | 2.489 | 2.484 | 2.484 | 2.482 | 2.482 | 2.478 | 2.464 | 2.437 |
| 23 | 2.392 | 2.408 | 2.416 | 2.359 | 2.406 | 2.380 | 2.332 | 2.384 | 2.363 | 2.367 | 2.341 | 2.320 | 2.355 | 2.414 | 2.391 |
| 24 | -0.630 | -0.604 | -0.585 | -0.583 | -0.565 | -0.540 | -0.530 | -0.524 | -0.513 | -0.501 | -0.495 | -0.483 | -0.472 | -0.598 | -0.482 |
| 27 | -0.645 | -0.615 | -0.598 | -0.592 | -0.574 | -0.553 | -0.539 | -0.531 | -0.520 | -0.510 | -0.502 | -0.487 | -0.479 | -0.611 | -0.491 |
| 28 | 2.269 | 2.301 | 2.318 | 2.320 | 2.342 | 2.369 | 2.379 | 2.388 | 2.400 | 2.412 | 2.423 | 2.437 | 2.449 | 2.297 | 2.432 |
| 29 | 2.351 | 2.377 | 2.418 | 2.400 | 2.422 | 2.449 | 2.461 | 2.470 | 2.484 | 2.496 | 2.505 | 2.519 | 2.529 | 2.377 | 2.512 |

SUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

MITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 1

BELASTUNGSGRAD M/MU

| SSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.686 | 0.571 | 0.400 | 0.400 | 0.400 | 0.100 | 0.000 | 0.429 | 0.857 | 0.857 |
|---------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | 2 | 3 | 4 | 5 | 6 | 1 | 1 | 1 | 2 | 3 | | 3 | | 7 | 8 |
| 1 | -0.203 | -0.189 | -0.214 | -0.199 | -0.195 | -0.203 | -0.195 | -0.195 | -0.205 | -0.187 | -0.208 | -0.228 | -0.218 | -0.191 | -0.191 |
| 2 | -0.193 | -0.181 | -0.203 | -0.189 | -0.187 | -0.193 | -0.185 | -0.185 | -0.193 | -0.173 | -0.189 | -0.224 | -0.214 | -0.183 | -0.183 |
| 3 | -0.197 | -0.199 | -0.216 | -0.203 | -0.206 | -0.216 | -0.208 | -0.206 | -0.224 | -0.199 | -0.220 | -0.242 | -0.224 | -0.197 | -0.201 |
| 4 | -0.254 | -0.227 | -0.238 | -0.217 | -0.197 | -0.197 | -0.207 | -0.207 | -0.211 | -0.197 | -0.207 | -0.244 | -0.242 | -0.215 | -0.211 |
| 7 | -0.212 | -0.203 | -0.251 | -0.238 | -0.240 | -0.238 | -0.222 | -0.220 | -0.228 | -0.210 | -0.220 | -0.242 | -0.238 | -0.218 | -0.222 |
| 9 | -0.221 | -0.207 | -0.230 | -0.215 | -0.213 | -0.215 | -0.203 | -0.195 | -0.207 | -0.187 | -0.189 | -0.221 | -0.228 | -0.219 | -0.222 |
| 11 | 0.038 | 0.106 | 0.155 | 0.209 | 0.239 | 0.211 | 0.196 | 0.163 | 0.163 | 0.198 | 0.128 | -0.071 | 0.016 | 0.139 | 0.170 |
| 12 | -0.091 | -0.085 | -0.118 | -0.109 | -0.118 | -0.136 | -0.134 | -0.144 | -0.159 | -0.142 | -0.159 | -0.173 | -0.138 | -0.062 | -0.072 |
| 13 | -0.177 | -0.141 | -0.102 | -0.048 | -0.007 | -0.011 | -0.011 | -0.024 | -0.028 | -0.001 | -0.034 | -0.136 | -0.114 | -0.038 | -0.022 |
| 14 | -0.077 | -0.079 | -0.075 | -0.077 | -0.075 | -0.079 | -0.075 | -0.073 | -0.070 | -0.073 | -0.066 | -0.081 | -0.083 | -0.079 | -0.077 |
| 15 | -0.045 | -0.045 | -0.039 | -0.037 | -0.031 | -0.029 | -0.025 | -0.019 | -0.015 | -0.019 | -0.005 | -0.017 | -0.025 | -0.035 | -0.031 |
| 16 | -0.355 | -0.353 | -0.347 | -0.338 | -0.322 | -0.306 | -0.283 | -0.258 | -0.250 | -0.244 | -0.189 | -0.213 | -0.285 | -0.343 | -0.331 |
| 19 | -0.380 | -0.382 | -0.375 | -0.380 | -0.382 | -0.367 | -0.349 | -0.314 | -0.314 | -0.318 | -0.256 | -0.250 | -0.320 | -0.388 | -0.391 |
| 22 | 2.443 | 2.443 | 2.460 | 2.470 | 2.482 | 2.489 | 2.476 | 2.478 | 2.478 | 2.480 | 2.484 | 2.435 | 2.439 | 2.450 | 2.462 |
| 23 | 2.388 | 2.390 | 2.386 | 2.384 | 2.382 | 2.388 | 2.388 | 2.392 | 2.402 | 2.398 | 2.412 | 2.386 | 2.382 | 2.367 | 2.371 |
| 24 | -0.479 | -0.476 | -0.456 | -0.452 | -0.440 | -0.470 | -0.479 | -0.505 | -0.503 | -0.505 | -0.550 | -0.608 | -0.546 | -0.474 | -0.466 |
| 27 | -0.491 | -0.491 | -0.496 | -0.494 | -0.491 | -0.516 | -0.526 | -0.549 | -0.543 | -0.545 | -0.582 | -0.625 | -0.563 | -0.506 | -0.501 |
| 28 | 2.443 | 2.445 | 2.466 | 2.470 | 2.482 | 2.453 | 2.435 | 2.406 | 2.406 | 2.408 | 2.357 | 2.287 | 2.359 | 2.443 | 2.458 |
| 29 | 2.515 | 2.513 | 2.521 | 2.521 | 2.525 | 2.502 | 2.482 | 2.453 | 2.455 | 2.453 | 2.410 | 2.363 | 2.431 | 2.509 | 2.511 |

VERSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

ERMITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 1

BELASTUNGSGRAD M/MU

| MESSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.943 | 1.000 |
|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | | |
| 1 | -0.181 | -0.183 | -0.007 | 0.147 | 0.219 | 0.246 | 0.299 | 0.322 | 0.322 | 0.344 |
| 2 | -0.169 | -0.169 | -0.151 | -0.103 | 0.034 | 0.102 | 0.186 | 0.244 | 0.264 | 0.293 |
| 3 | -0.201 | -0.201 | -0.199 | -0.212 | -0.199 | -0.155 | -0.083 | -0.044 | -0.034 | -0.009 |
| 4 | -0.187 | -0.152 | 0.002 | 0.027 | 0.103 | 0.144 | 0.218 | 0.279 | 0.285 | 0.314 |
| 7 | -0.212 | -0.218 | -0.218 | -0.234 | -0.232 | -0.230 | -0.183 | -0.036 | 0.001 | 0.034 |
| 9 | -0.205 | -0.207 | -0.199 | -0.197 | -0.140 | -0.088 | 0.012 | 0.119 | 0.168 | 0.220 |
| 11 | 0.231 | 0.285 | 0.352 | 0.451 | 0.625 | 0.710 | 0.790 | 0.855 | 0.890 | 0.913 |
| 12 | -0.072 | -0.091 | -0.105 | -0.132 | -0.134 | -0.138 | -0.118 | -0.085 | -0.079 | -0.050 |
| 13 | 0.018 | 0.075 | 0.293 | 0.679 | 0.896 | 1.015 | 1.124 | 1.215 | 1.276 | 1.278 |
| 14 | -0.075 | -0.070 | -0.073 | -0.073 | -0.070 | -0.058 | -0.009 | 0.028 | 0.042 | 0.065 |
| 15 | -0.029 | -0.019 | 0.047 | 0.264 | 0.533 | 0.659 | 0.806 | 0.901 | 0.983 | 0.999 |
| 16 | -0.320 | -0.281 | -0.072 | 0.394 | 0.665 | 0.844 | 1.043 | 1.213 | 1.277 | 1.296 |
| 19 | -0.392 | -0.400 | -0.406 | -0.412 | -0.433 | -0.435 | -0.412 | -0.369 | -0.398 | -0.353 |
| 22 | 2.470 | 2.493 | 2.533 | 2.638 | 2.767 | 2.833 | 2.927 | 2.995 | 3.036 | 3.065 |
| 23 | 2.367 | 2.367 | 2.359 | 2.359 | 2.341 | 2.335 | 2.351 | 2.349 | 2.345 | 2.361 |
| 24 | -0.456 | -0.435 | -0.401 | -0.310 | -0.216 | -0.150 | -0.086 | -0.035 | 0.010 | 0.035 |
| 27 | -0.500 | -0.496 | -0.496 | -0.473 | -0.461 | -0.457 | -0.438 | -0.430 | -0.426 | -0.457 |
| 28 | 2.466 | 2.486 | 2.519 | 2.568 | 2.636 | 2.687 | 2.763 | 2.809 | 2.874 | 2.887 |
| 29 | 2.509 | 2.519 | 2.531 | 2.576 | 2.609 | 2.634 | 2.677 | 2.710 | 2.749 | 2.743 |

RSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

RMITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 1*

BELASTUNGSGRAD M/MU

ESSTELLE 0.000 0.114 0.229 0.229 0.343 0.457 0.514 0.571 0.629 0.686 0.743 0.800 0.857 0.000 0.000

1 1

| | | | | | | | | | | | | | | | |
|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-----|
| 23 | 3.010 | 3.058 | 3.036 | 3.028 | 3.028 | 3.042 | 3.024 | 3.020 | 3.030 | 3.022 | 3.016 | 3.026 | 3.012 | 3.012 | 3.0 |
| 28 | 2.271 | 2.322 | 2.349 | 2.355 | 2.383 | 2.412 | 2.427 | 2.437 | 2.464 | 2.470 | 2.484 | 2.505 | 2.517 | 2.318 | 2.5 |
| 29 | 2.320 | 2.375 | 2.393 | 2.404 | 2.434 | 2.457 | 2.474 | 2.486 | 2.510 | 2.517 | 2.531 | 2.554 | 2.566 | 2.352 | 2.5 |

VERSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

ERMITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 1*

BELASTUNGSGRAD M/MU

| MESSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.686 | 0.571 | 0.400 | 0.400 | 0.400 | 0.100 | 0.000 | 0.429 | 0.857 | 0.100 |
|-----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- |
| | 2 | 3 | 4 | 5 | 6 | 1 | 1 | 1 | 2 | 3 | | 3 | | 7 | |
| 23 | 3.022 | 2.994 | 3.018 | 3.020 | 3.010 | 3.010 | 3.016 | 3.014 | 3.008 | 3.012 | 3.032 | 3.008 | 3.014 | 2.973 | 2.973 |
| 28 | 2.527 | 2.523 | 2.542 | 2.546 | 2.546 | 2.509 | 2.492 | 2.443 | 2.451 | 2.455 | 2.400 | 2.328 | 2.429 | 2.513 | 2.513 |
| 29 | 2.566 | 2.558 | 2.576 | 2.580 | 2.580 | 2.545 | 2.523 | 2.471 | 2.484 | 2.488 | 2.432 | 2.363 | 2.461 | 2.505 | 2.505 |

VERSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

ERMITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 1*

BELASTUNGSGRAD M/MU

| MESSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.943 | 1.000 |
|-----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | | |
| | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | | |
| ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- |
| 23 | 2.989 | 2.975 | 2.987 | 2.987 | 2.953 | 2.979 | 3.002 | 2.981 | 2.977 | 3.008 |
| 28 | 2.550 | 2.539 | 2.568 | 2.597 | 2.654 | 2.710 | 2.782 | 2.817 | 2.876 | 2.882 |
| 29 | 2.580 | 2.572 | 2.607 | 2.658 | 2.699 | 2.740 | 2.794 | 2.810 | 2.851 | 2.825 |

ERSUCHSBALKEN SETMO1 GEPRUEFT AM 19. 5. 1978

ERMITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 3

BELASTUNGSGRAD M/MU

MESSTELLE 0.000 0.114 0.229 0.229 0.343 0.457 0.514 0.571 0.629 0.686 0.743 0.800 0.857 0.000 0.000

| | 1 | | | | | | | | | | | | | | 1 |
|----|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 1 | -0.129 | -0.105 | -0.090 | -0.088 | -0.074 | -0.062 | -0.051 | -0.045 | -0.041 | -0.037 | -0.029 | -0.021 | -0.017 | -0.002 | -0.000 |
| 2 | 0.033 | 0.045 | 0.051 | 0.047 | 0.045 | 0.053 | 0.067 | 0.053 | 0.045 | 0.039 | 0.094 | 0.084 | 0.084 | 0.002 | 0.000 |
| 3 | -0.131 | -0.107 | -0.095 | -0.090 | -0.078 | -0.064 | -0.053 | -0.045 | -0.039 | -0.033 | -0.023 | -0.014 | -0.006 | -0.076 | -0.000 |
| 4 | -0.125 | -0.103 | -0.093 | -0.089 | -0.078 | -0.068 | -0.058 | -0.052 | -0.050 | -0.045 | -0.039 | -0.033 | -0.027 | -0.072 | -0.000 |
| 7 | -0.121 | -0.101 | -0.078 | -0.087 | -0.074 | -0.062 | -0.052 | -0.046 | -0.041 | -0.037 | -0.029 | -0.023 | -0.019 | -0.064 | -0.000 |
| 8 | -0.103 | -0.091 | -0.081 | -0.091 | -0.091 | -0.093 | -0.091 | -0.093 | -0.097 | -0.101 | -0.101 | -0.103 | -0.107 | -0.069 | -0.000 |
| 9 | -0.084 | -0.078 | -0.068 | -0.074 | -0.068 | -0.080 | -0.072 | -0.076 | -0.082 | -0.088 | -0.088 | -0.092 | -0.092 | -0.048 | -0.000 |
| 11 | -0.045 | -0.035 | -0.033 | -0.029 | -0.023 | -0.027 | -0.015 | -0.013 | -0.013 | -0.011 | -0.006 | 0.002 | 0.008 | -0.006 | 0.000 |
| 12 | -0.080 | -0.054 | -0.054 | -0.048 | -0.052 | -0.058 | -0.044 | -0.039 | -0.035 | -0.033 | -0.033 | -0.029 | -0.029 | -0.029 | -0.000 |
| 13 | -0.047 | -0.049 | -0.043 | -0.045 | -0.045 | -0.045 | -0.045 | -0.047 | -0.047 | -0.047 | -0.049 | -0.047 | -0.047 | -0.025 | -0.000 |
| 14 | -0.057 | -0.023 | -0.033 | -0.016 | -0.023 | -0.031 | -0.018 | -0.016 | -0.018 | -0.018 | -0.018 | -0.016 | -0.023 | 0.004 | -0.000 |
| 15 | -0.027 | -0.009 | -0.011 | -0.011 | -0.017 | -0.019 | -0.021 | -0.025 | -0.025 | -0.023 | -0.027 | -0.031 | -0.035 | 0.018 | -0.000 |
| 16 | -0.209 | -0.254 | -0.306 | -0.312 | -0.367 | -0.433 | -0.470 | -0.499 | -0.533 | -0.570 | -0.603 | -0.644 | -0.683 | -0.293 | -0.000 |
| 19 | -0.253 | -0.306 | -0.356 | -0.362 | -0.421 | -0.487 | -0.526 | -0.561 | -0.596 | -0.641 | -0.676 | -0.723 | -0.764 | -0.347 | -0.000 |
| 22 | 2.940 | 2.948 | 2.954 | 2.952 | 2.946 | 2.952 | 2.942 | 2.942 | 2.940 | 2.936 | 2.938 | 2.968 | 2.995 | 2.989 | 3.000 |
| 23 | 2.485 | 2.485 | 2.501 | 2.483 | 2.477 | 2.475 | 2.469 | 2.464 | 2.464 | 2.458 | 2.454 | 2.450 | 2.448 | 2.454 | 2.400 |
| 27 | -0.869 | -0.820 | -0.775 | -0.761 | -0.715 | -0.676 | -0.633 | -0.609 | -0.580 | -0.551 | -0.525 | -0.496 | -0.467 | -0.837 | -0.000 |
| 28 | 2.057 | 2.132 | 2.151 | 2.147 | 2.196 | 2.254 | 2.276 | 2.303 | 2.330 | 2.360 | 2.389 | 2.426 | 2.455 | 2.063 | 2.400 |
| 29 | 2.392 | 2.435 | 2.484 | 2.484 | 2.529 | 2.585 | 2.609 | 2.636 | 2.665 | 2.700 | 2.728 | 2.761 | 2.794 | 2.402 | 2.700 |
| 30 | 3.735 | 3.763 | 3.798 | 3.796 | 3.827 | 3.868 | 3.886 | 3.905 | 3.925 | 3.946 | 3.964 | 3.985 | 4.010 | 3.733 | 4.000 |
| 31 | 3.735 | 3.757 | 3.788 | 3.854 | 3.882 | 3.909 | 3.919 | 3.932 | 3.950 | 4.006 | 4.020 | 4.034 | 4.057 | 3.780 | 4.200 |

VERSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

 MITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 3

| MESSSTELLE | BELASTUNGSGRAD M/MU | | | | | | | | | | | | | | |
|------------|---------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.686 | 0.571 | 0.400 | 0.400 | 0.400 | 0.100 | 0.000 | 0.429 | 0.857 | 0.857 |
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- |
| | 2 | 3 | 4 | 5 | 6 | 1 | 1 | 1 | 2 | 3 | | 3 | | 7 | |
| 1 | -0.033 | -0.033 | -0.031 | -0.025 | -0.027 | -0.031 | -0.033 | -0.043 | -0.035 | -0.033 | -0.043 | -0.076 | -0.043 | -0.017 | -0.017 |
| 2 | 0.203 | 0.164 | 0.069 | 0.248 | 0.184 | 0.162 | 0.197 | 0.180 | 0.184 | 0.187 | 0.189 | 0.166 | 0.170 | 0.197 | 0.203 |
| 3 | -0.019 | -0.019 | -0.027 | -0.023 | -0.031 | -0.039 | -0.043 | -0.056 | -0.051 | -0.049 | -0.066 | -0.084 | -0.051 | -0.019 | -0.019 |
| 4 | -0.039 | -0.031 | -0.019 | 0.002 | 0.012 | 0.010 | 0.008 | 0.004 | 0.008 | 0.010 | -0.002 | -0.037 | -0.011 | 0.014 | 0.014 |
| 7 | -0.031 | -0.033 | -0.039 | -0.039 | -0.046 | -0.052 | -0.052 | -0.058 | -0.054 | -0.050 | -0.058 | -0.076 | -0.058 | -0.037 | -0.037 |
| 8 | -0.124 | -0.121 | -0.113 | -0.099 | -0.085 | -0.073 | -0.069 | -0.060 | -0.056 | -0.052 | -0.034 | -0.060 | -0.075 | -0.085 | -0.085 |
| 9 | -0.113 | -0.111 | -0.123 | -0.123 | -0.129 | -0.117 | -0.109 | -0.094 | -0.088 | -0.084 | -0.058 | -0.070 | -0.096 | -0.125 | -0.125 |
| 11 | 0.035 | 0.080 | 0.180 | 0.248 | 0.351 | 0.351 | 0.334 | 0.306 | 0.320 | 0.332 | 0.289 | 0.127 | 0.191 | 0.293 | 0.306 |
| 12 | -0.017 | -0.023 | -0.033 | -0.033 | -0.037 | -0.037 | -0.015 | -0.017 | -0.002 | -0.002 | 0.016 | -0.011 | -0.011 | -0.009 | -0.009 |
| 13 | -0.035 | -0.021 | 0.049 | 0.076 | 0.113 | 0.102 | 0.104 | 0.102 | 0.107 | 0.111 | 0.111 | 0.053 | 0.051 | 0.082 | 0.104 |
| 14 | -0.023 | -0.023 | -0.037 | -0.037 | -0.041 | -0.014 | -0.010 | -0.008 | 0.002 | 0.000 | 0.021 | 0.008 | -0.006 | -0.018 | -0.018 |
| 15 | -0.029 | -0.029 | -0.011 | -0.005 | 0.001 | -0.005 | 0.005 | 0.022 | 0.020 | 0.020 | 0.044 | 0.024 | 0.003 | -0.021 | -0.021 |
| 16 | -0.702 | -0.700 | -0.700 | -0.692 | -0.679 | -0.603 | -0.568 | -0.496 | -0.486 | -0.484 | -0.340 | -0.316 | -0.507 | -0.698 | -0.698 |
| 19 | -0.803 | -0.814 | -0.836 | -0.848 | -0.863 | -0.797 | -0.740 | -0.651 | -0.643 | -0.645 | -0.477 | -0.401 | -0.616 | -0.848 | -0.848 |
| 22 | 3.057 | 3.089 | 3.360 | 3.441 | 3.480 | 3.477 | 3.473 | 3.463 | 3.475 | 3.484 | 3.480 | 3.319 | 3.393 | 3.445 | 3.445 |
| 23 | 2.428 | 2.423 | 2.421 | 2.421 | 2.419 | 2.417 | 2.421 | 2.428 | 2.434 | 2.434 | 2.454 | 2.417 | 2.403 | 2.399 | 2.417 |
| 27 | -0.473 | -0.459 | -0.465 | -0.461 | -0.453 | -0.516 | -0.555 | -0.633 | -0.615 | -0.617 | -0.736 | -0.839 | -0.668 | -0.481 | -0.481 |
| 28 | 2.473 | 2.445 | 2.498 | 2.494 | 2.519 | 2.416 | 2.387 | 2.328 | 2.284 | 2.291 | 2.157 | 2.055 | 2.235 | 2.453 | 2.453 |
| 29 | 2.771 | 2.771 | 2.802 | 2.829 | 2.849 | 2.790 | 2.718 | 2.632 | 2.632 | 2.630 | 2.502 | 2.398 | 2.572 | 2.792 | 2.792 |
| 30 | 4.059 | 4.071 | 4.112 | 4.114 | 4.118 | 4.065 | 4.028 | 3.967 | 3.973 | 3.973 | 3.880 | 3.808 | 3.923 | 4.092 | 4.114 |
| 31 | 4.213 | 4.201 | 4.106 | 4.108 | 4.108 | 4.118 | 4.075 | 4.020 | 4.026 | 4.016 | 3.930 | 3.655 | 3.810 | 3.952 | 3.952 |

VERSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

ERMITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 3

BELASTUNGSGRAD M/MU

| MESSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.943 | 1.000 |
|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | | |
| | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | | |
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- |
| 1 | -0.006 | 0.000 | 0.004 | 0.068 | 0.466 | 0.528 | 0.622 | 0.682 | 0.696 | 0.677 |
| 2 | 0.209 | 0.213 | 0.209 | 0.301 | 0.421 | 0.453 | 0.525 | 0.583 | 0.640 | 0.649 |
| 3 | -0.012 | -0.012 | -0.012 | -0.008 | 0.004 | 0.027 | 0.059 | 0.088 | 0.125 | 0.150 |
| 4 | 0.037 | 0.055 | 0.135 | 0.357 | 0.544 | 0.622 | 0.710 | 0.776 | 0.842 | 0.805 |
| 7 | -0.031 | -0.027 | -0.027 | -0.029 | 0.002 | 0.020 | 0.053 | 0.076 | 0.115 | 0.164 |
| 8 | -0.062 | -0.052 | 0.071 | 0.317 | 0.471 | 0.556 | 0.681 | 0.784 | 0.864 | 0.765 |
| 9 | -0.119 | -0.119 | -0.062 | 0.008 | 0.355 | 0.499 | 0.607 | 0.694 | 0.772 | 0.667 |
| 11 | 0.388 | 0.488 | 0.681 | 0.866 | 0.879 | 0.932 | 1.006 | 1.047 | 1.080 | 0.905 |
| 12 | -0.005 | -0.009 | -0.013 | -0.009 | 0.024 | 0.053 | 0.121 | 0.170 | 0.250 | 0.295 |
| 13 | 0.129 | 0.189 | 0.281 | 0.579 | 0.690 | 0.741 | 0.821 | 0.858 | 0.885 | 0.720 |
| 14 | -0.016 | -0.018 | -0.021 | -0.014 | 0.055 | 0.113 | 0.187 | 0.242 | 0.285 | 0.314 |
| 15 | -0.011 | 0.012 | 0.143 | 0.831 | 1.012 | 1.122 | 1.241 | 1.311 | 1.365 | 1.069 |
| 16 | -0.683 | -0.665 | -0.636 | -0.622 | -0.548 | -0.509 | -0.427 | -0.371 | -0.371 | -0.371 |
| 19 | -0.875 | -0.902 | -0.945 | -1.019 | -1.091 | -1.140 | -1.146 | -1.175 | -1.302 | -1.171 |
| 22 | 3.477 | 3.506 | 3.570 | 3.689 | 3.802 | 3.864 | 3.970 | 4.026 | 4.094 | 3.954 |
| 23 | 2.409 | 2.407 | 2.409 | 2.417 | 2.440 | 2.452 | 2.499 | 2.519 | 2.558 | 2.515 |
| 27 | -0.463 | -0.449 | -0.455 | -0.434 | -0.373 | -0.375 | -0.350 | -0.338 | -0.282 | -0.356 |
| 28 | 2.479 | 2.504 | 2.640 | 2.942 | 3.106 | 3.243 | 3.377 | 3.422 | 3.566 | 3.112 |
| 29 | 2.817 | 2.856 | 2.901 | 2.971 | 3.069 | 3.116 | 3.172 | 3.203 | 3.303 | 3.123 |
| 30 | 4.114 | 4.145 | 4.168 | 4.303 | 4.546 | 4.659 | 4.792 | 4.880 | 5.026 | 4.741 |
| 31 | 3.954 | 3.964 | 3.985 | 4.010 | 4.053 | 4.079 | 4.145 | 4.162 | 4.281 | 4.178 |

RSUCHSBALKEN SETMO1 GEPRUEFT AM 19. 5. 1978

ERMittelTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 3*

BELASTUNGSGRAD M/MU

| MESSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.686 | 0.571 | 0.400 | 0.400 | 0.400 | 0.100 | 0.000 | 0.429 | 0.857 | 0.857 |
|-----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | 2 | 3 | 4 | 5 | 6 | 1 | 1 | 1 | 2 | 3 | | 3 | | 7 | |
| 30 | 3.987 | 3.991 | 3.999 | 4.026 | 4.032 | 3.950 | 3.901 | 3.819 | 3.827 | 3.827 | 3.710 | 3.593 | 3.739 | 3.960 | 3.960 |
| 31 | 3.537 | 3.541 | 3.554 | 3.560 | 3.564 | 3.508 | 3.473 | 3.414 | 3.422 | 3.426 | 3.332 | 3.278 | 3.420 | 3.590 | 3.600 |

VERSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

ERMITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 3*

BELASTUNGSGRAD M/MU

| MESSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.943 | 1.000 |
|-----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | | |
| | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | | |
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | | |
| 30 | 4.012 | 4.053 | 4.277 | 4.498 | 4.784 | 4.942 | 5.112 | 5.227 | 5.467 | 5.192 |
| 31 | 3.621 | 3.642 | 3.689 | 3.753 | 3.802 | 3.853 | 3.880 | 3.913 | 4.075 | 4.165 |

RSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

RMITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 5

BELASTUNGSGRAD M/MU

| ESSTELLE | 0.000 | 0.114 | 0.229 | 0.229 | 0.343 | 0.457 | 0.514 | 0.571 | 0.629 | 0.686 | 0.743 | 0.800 | 0.857 | 0.000 | 0.857 |
|----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|
| | | | | ----- | | | | | | | | | | ----- | ----- |
| | | | | 1 | | | | | | | | | | 1 | 1 |
| 1 | -0.029 | -0.027 | -0.013 | -0.011 | -0.005 | 0.010 | 0.016 | 0.020 | 0.028 | 0.034 | 0.040 | 0.053 | 0.063 | 0.012 | 0.05 |
| 2 | -0.068 | -0.052 | -0.032 | -0.034 | -0.021 | 0.007 | 0.020 | 0.032 | 0.055 | 0.073 | 0.090 | 0.116 | 0.145 | 0.016 | 0.13 |
| 3 | -0.033 | -0.023 | -0.013 | -0.013 | -0.003 | 0.016 | 0.024 | 0.028 | 0.038 | 0.047 | 0.055 | 0.067 | 0.081 | 0.010 | 0.07 |
| 4 | -0.084 | -0.086 | -0.076 | -0.070 | -0.066 | -0.056 | -0.054 | -0.048 | -0.043 | -0.041 | -0.037 | -0.033 | -0.029 | -0.033 | -0.04 |
| 7 | -0.092 | -0.088 | -0.076 | -0.078 | -0.078 | -0.068 | -0.066 | -0.064 | -0.058 | -0.058 | -0.053 | -0.051 | -0.047 | -0.045 | -0.06 |
| 8 | -0.413 | -0.399 | -0.393 | -0.301 | -0.379 | -0.446 | -0.444 | -0.479 | -0.495 | -0.350 | -0.360 | -0.379 | -0.374 | -0.440 | -0.52 |
| 9 | -0.062 | -0.058 | -0.060 | -0.058 | -0.068 | -0.072 | -0.078 | -0.085 | -0.087 | -0.093 | -0.093 | -0.091 | -0.095 | -0.023 | -0.10 |
| 11 | -0.080 | -0.078 | -0.074 | -0.072 | -0.076 | -0.074 | -0.074 | -0.076 | -0.076 | -0.080 | -0.084 | -0.092 | -0.094 | -0.037 | -0.09 |
| 12 | -0.064 | -0.068 | -0.064 | -0.064 | -0.068 | -0.064 | -0.064 | -0.066 | -0.064 | -0.066 | -0.072 | -0.078 | -0.085 | -0.034 | -0.08 |
| 13 | -0.016 | -0.026 | -0.024 | -0.022 | -0.030 | -0.032 | -0.037 | -0.041 | -0.045 | -0.051 | -0.049 | -0.041 | -0.037 | 0.016 | -0.03 |
| 14 | -0.029 | -0.029 | -0.027 | -0.025 | -0.033 | -0.037 | -0.039 | -0.045 | -0.047 | -0.052 | -0.054 | -0.037 | -0.019 | 0.016 | -0.00 |
| 15 | -0.041 | -0.041 | -0.045 | -0.039 | -0.051 | -0.055 | -0.059 | -0.066 | -0.068 | -0.076 | -0.082 | -0.082 | -0.082 | -0.009 | -0.00 |
| 16 | -0.193 | -0.257 | -0.341 | -0.343 | -0.427 | -0.522 | -0.579 | -0.630 | -0.686 | -0.756 | -0.819 | -0.901 | -0.979 | -0.324 | -1.03 |
| 19 | -0.164 | -0.236 | -0.330 | -0.330 | -0.427 | -0.534 | -0.597 | -0.655 | -0.716 | -0.796 | -0.866 | -0.961 | -1.053 | -0.336 | -1.10 |
| 22 | 2.337 | 2.337 | 2.316 | 2.335 | 2.327 | 2.321 | 2.312 | 2.308 | 2.306 | 2.298 | 2.306 | 2.319 | 2.343 | 2.245 | 2.30 |
| 23 | 1.304 | 1.259 | 1.199 | 1.279 | 1.152 | 1.271 | 1.269 | 1.259 | 1.261 | 1.259 | 1.263 | 1.290 | 1.302 | 1.222 | 1.27 |
| 24 | -1.035 | -0.943 | -0.853 | -0.871 | -0.787 | -0.678 | -0.631 | -0.588 | -0.524 | -0.448 | -0.366 | -0.274 | -0.105 | -0.984 | -0.07 |
| 27 | -0.501 | -0.428 | -0.360 | -0.372 | -0.278 | -0.191 | -0.157 | -0.118 | -0.060 | 0.002 | 0.065 | 0.139 | 0.221 | -0.569 | 0.18 |
| 28 | 2.218 | 2.300 | 2.357 | 2.382 | 2.454 | 2.526 | 2.585 | 2.620 | 2.671 | 2.729 | 2.795 | 2.885 | 3.000 | 2.281 | 2.99 |
| 29 | 2.086 | 2.168 | 2.248 | 2.254 | 2.330 | 2.406 | 2.467 | 2.511 | 2.560 | 2.613 | 2.687 | 2.792 | 2.921 | 2.186 | 2.95 |
| 30 | 3.862 | 3.929 | 3.989 | 3.970 | 4.028 | 4.100 | 4.126 | 4.151 | 4.190 | 4.241 | 4.301 | 4.379 | 4.471 | 3.884 | 4.46 |
| 31 | 4.493 | 4.560 | 4.620 | 4.620 | 4.675 | 4.729 | 4.778 | 4.803 | 4.842 | 4.883 | 4.961 | 5.026 | 5.096 | 4.556 | 5.15 |

RSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

RMITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 5

| BELASTUNGSGRAD M/MU | | | | | | | | | | | | | | | |
|---------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|
| ESSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.686 | 0.571 | 0.400 | 0.400 | 0.400 | 0.100 | 0.000 | 0.429 | 0.857 | 0.8 |
| | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | | --- | | --- | --- |
| | 2 | 3 | 4 | 5 | 6 | 11 | 1 | 1 | 2 | 3 | | 3 | | 7 | |
| 1 | 0.055 | 0.057 | 0.061 | 0.065 | 0.069 | 0.067 | 0.063 | 0.055 | 0.059 | 0.059 | 0.046 | 0.005 | 0.030 | 0.063 | 0.0 |
| 2 | 0.159 | 0.161 | 0.174 | 0.180 | 0.194 | 0.161 | 0.139 | 0.102 | 0.108 | 0.110 | 0.067 | 0.036 | 0.106 | 0.198 | 0.2 |
| 3 | 0.081 | 0.084 | 0.088 | 0.092 | 0.102 | 0.096 | 0.090 | 0.079 | 0.084 | 0.084 | 0.055 | 0.008 | 0.042 | 0.088 | 0.0 |
| 4 | -0.045 | -0.048 | -0.052 | -0.058 | -0.072 | -0.086 | -0.088 | -0.090 | -0.084 | -0.084 | -0.054 | -0.043 | -0.070 | -0.050 | -0.0 |
| 7 | -0.066 | -0.066 | -0.068 | -0.074 | -0.076 | -0.090 | -0.096 | -0.098 | -0.094 | -0.092 | -0.051 | -0.051 | -0.082 | -0.084 | -0.0 |
| 8 | -0.622 | -0.622 | -0.598 | -0.503 | -0.477 | -0.514 | -0.542 | -0.559 | -0.557 | -0.538 | -0.514 | -0.575 | -0.198 | -0.169 | -0.1 |
| 9 | -0.109 | -0.115 | -0.119 | -0.122 | -0.095 | -0.076 | -0.066 | -0.044 | -0.038 | -0.034 | 0.007 | 0.001 | -0.036 | -0.054 | -0.0 |
| 11 | -0.098 | -0.094 | -0.050 | 0.012 | 0.047 | 0.049 | 0.043 | 0.039 | 0.049 | 0.053 | 0.069 | 0.030 | 0.008 | 0.028 | 0.0 |
| 12 | -0.089 | -0.087 | -0.078 | -0.066 | 0.030 | 0.036 | 0.034 | 0.034 | 0.038 | 0.046 | 0.092 | 0.036 | 0.016 | -0.030 | 0.0 |
| 13 | -0.032 | -0.028 | 0.014 | 0.070 | 0.127 | 0.127 | 0.119 | 0.115 | 0.123 | 0.127 | 0.148 | 0.111 | 0.080 | 0.094 | 0.1 |
| 14 | -0.011 | -0.013 | -0.011 | -0.011 | 0.007 | 0.007 | 0.007 | 0.014 | 0.020 | 0.018 | 0.044 | 0.034 | 0.005 | 0.012 | 0.0 |
| 15 | -0.096 | -0.092 | -0.082 | -0.074 | -0.007 | 0.010 | 0.018 | 0.028 | 0.037 | 0.039 | 0.071 | 0.045 | 0.006 | -0.045 | -0.0 |
| 16 | -1.068 | -1.068 | -1.080 | -1.074 | -1.060 | -0.959 | -0.879 | -0.756 | -0.739 | -0.733 | -0.483 | -0.388 | -0.710 | -1.088 | -1.0 |
| 19 | -1.166 | -1.185 | -1.246 | -1.275 | -1.330 | -1.221 | -1.121 | -0.961 | -0.950 | -0.953 | -0.649 | -0.497 | -0.846 | -1.269 | -1.3 |
| 22 | 2.280 | 2.280 | 2.298 | 2.327 | 2.347 | 2.298 | 2.269 | 2.238 | 2.240 | 2.243 | 2.236 | 2.179 | 2.165 | 2.275 | 2.2 |
| 23 | 1.275 | 1.267 | 1.338 | 1.345 | 1.392 | 1.263 | 1.230 | 1.183 | 1.199 | 1.195 | 1.199 | 1.177 | 1.154 | 1.269 | 1.2 |
| 24 | -0.027 | -0.025 | 0.098 | 0.135 | 0.178 | -0.089 | -0.280 | -0.508 | -0.518 | -0.518 | -0.806 | -1.011 | -0.703 | 0.018 | 0.0 |
| 27 | 0.207 | 0.203 | 0.236 | 0.234 | 0.201 | 0.094 | -0.046 | -0.204 | -0.208 | -0.206 | -0.450 | -0.663 | -0.362 | 0.117 | 0.1 |
| 28 | 3.024 | 3.035 | 3.047 | 3.080 | 3.197 | 3.018 | 2.903 | 2.716 | 2.729 | 2.733 | 2.497 | 2.298 | 2.558 | 3.098 | 3.1 |
| 29 | 2.997 | 3.007 | 3.059 | 3.090 | 3.235 | 2.987 | 2.851 | 2.652 | 2.650 | 2.652 | 2.408 | 2.250 | 2.531 | 3.133 | 3.1 |
| 30 | 4.498 | 4.482 | 4.525 | 4.560 | 4.590 | 4.436 | 4.321 | 4.188 | 4.176 | 4.174 | 3.997 | 3.852 | 4.052 | 4.492 | 4.5 |
| 31 | 5.178 | 5.201 | 5.234 | 5.273 | 5.398 | 5.250 | 5.119 | 4.955 | 4.975 | 4.979 | 4.794 | 4.417 | 4.620 | 5.074 | 5.1 |

VERSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

ERMITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 5

BELASTUNGSGRAD M/MU

| MESSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.943 | 1.000 |
|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | | |
| | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | | |
| ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- |
| 1 | 0.075 | 0.081 | 0.085 | 0.088 | 0.114 | 0.133 | 0.207 | 0.229 | 0.244 | 0.272 |
| 2 | 0.221 | 0.244 | 0.266 | 0.305 | 0.387 | 0.435 | 0.513 | 0.552 | 0.597 | 0.580 |
| 3 | 0.102 | 0.116 | 0.131 | 0.155 | 0.207 | 0.244 | 0.318 | 0.359 | 0.468 | 0.595 |
| 4 | -0.058 | -0.070 | -0.048 | 0.004 | 0.053 | 0.092 | 0.170 | 0.201 | 0.215 | 0.238 |
| 7 | -0.076 | -0.086 | -0.094 | -0.076 | 0.012 | 0.062 | 0.174 | 0.257 | 0.415 | 0.571 |
| 8 | -0.128 | -0.081 | -0.009 | 0.124 | 0.227 | 0.258 | 2.476 | 3.315 | 3.580 | 2.835 |
| 9 | -0.058 | -0.036 | 0.005 | 0.073 | 0.295 | 0.494 | 0.593 | 0.656 | 0.960 | 0.843 |
| 11 | 0.071 | 0.133 | 0.279 | 0.410 | 0.517 | 0.591 | 0.683 | 0.729 | 0.724 | 0.466 |
| 12 | 0.059 | 0.163 | 0.297 | 0.467 | 0.623 | 0.722 | 0.857 | 0.948 | 1.032 | 0.498 |
| 13 | 0.174 | 0.277 | 0.386 | 0.524 | 0.653 | 0.721 | 0.836 | 0.885 | 0.881 | 0.622 |
| 14 | 0.024 | 0.044 | 0.135 | 0.279 | 0.404 | 0.480 | 0.591 | 0.640 | 0.695 | 0.428 |
| 15 | 0.020 | 0.131 | 0.285 | 0.460 | 0.704 | 0.827 | 0.969 | 1.055 | 1.170 | 0.985 |
| 16 | -1.064 | -1.047 | -1.018 | -0.971 | -0.922 | -0.928 | -0.854 | -0.846 | -0.914 | -1.113 |
| 19 | -1.343 | -1.415 | -1.527 | -1.710 | -1.963 | -2.189 | -2.283 | -2.456 | -3.117 | -3.361 |
| 22 | 2.302 | 2.347 | 2.392 | 2.454 | 2.523 | 2.569 | 2.663 | 2.704 | 2.858 | 2.425 |
| 23 | 1.316 | 1.384 | 1.478 | 1.618 | 1.761 | 1.852 | 1.963 | 2.002 | 2.225 | 1.622 |
| 24 | 0.121 | 0.264 | 0.420 | 0.572 | 0.739 | 0.872 | 1.004 | 1.065 | 1.254 | 0.513 |
| 27 | 0.112 | 0.131 | 0.141 | 0.143 | 0.076 | 0.086 | 0.217 | 0.281 | 0.566 | 0.078 |
| 28 | 3.213 | 3.404 | 3.616 | 3.862 | 4.283 | 4.589 | 4.831 | 5.016 | 5.464 | 5.386 |
| 29 | 3.248 | 3.328 | 3.416 | 3.558 | 3.790 | 3.975 | 4.096 | 4.172 | 4.480 | 4.363 |
| 30 | 4.541 | 4.603 | 4.679 | 4.818 | 4.993 | 5.137 | 5.303 | 5.385 | 5.724 | 5.091 |
| 31 | 5.201 | 5.314 | 5.478 | 5.663 | 5.887 | 6.035 | 6.193 | 6.318 | 6.922 | 7.287 |

SUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

 MITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 5

BELASTUNGSGRAD M/MU

| STELLE | 0,000 | 0,114 | 0,229 | 0,229 | 0,343 | 0,457 | 0,514 | 0,571 | 0,629 | 0,686 | 0,743 | 0,800 | 0,857 | 0,000 | 0,857 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | | | ----- | | | | | | | | | | ----- | ----- |
| | | | | 1 | | | | | | | | | | 1 | 1 |
| 22 | 1.669 | 1.685 | 1.683 | 1.685 | 1.683 | 1.671 | 1.675 | 1.665 | 1.663 | 1.657 | 1.667 | 1.683 | 1.720 | 1.683 | 1.70 |
| 23 | 2.417 | 2.431 | 2.431 | 2.431 | 2.425 | 2.411 | 2.417 | 2.405 | 2.403 | 2.399 | 2.409 | 2.427 | 2.474 | 2.370 | 2.40 |
| 28 | 1.848 | 1.903 | 1.973 | 1.969 | 2.034 | 2.110 | 2.092 | 2.106 | 2.145 | 2.190 | 2.303 | 2.443 | 2.599 | 1.622 | 2.47 |
| 29 | 2.322 | 2.387 | 2.459 | 2.461 | 2.529 | 2.611 | 2.656 | 2.699 | 2.755 | 2.827 | 2.977 | 3.157 | 3.358 | 2.344 | 3.36 |
| 30 | 3.834 | 3.873 | 3.946 | 3.942 | 3.988 | 4.041 | 4.078 | 4.119 | 4.152 | 4.197 | 4.312 | 4.474 | 4.671 | 3.818 | 4.63 |
| 31 | 3.349 | 3.394 | 3.449 | 3.451 | 3.500 | 3.560 | 3.585 | 3.615 | 3.652 | 3.693 | 3.808 | 3.989 | 4.211 | 3.306 | 4.17 |

SUCHSBALKEN SETMQ 1 GEPRUEFT AM 19. 5. 1978

MITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 5

| | BELASTUNGSGRAD M/MU | | | | | | | | | | | | | | |
|---------|---------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| SSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.686 | 0.571 | 0.400 | 0.400 | 0.400 | 0.100 | 0.000 | 0.429 | 0.857 | 0.857 |
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | | ----- | | ----- | ----- |
| | 2 | 3 | 4 | 5 | 6 | 1 | 1 | 1 | 2 | 3 | | 3 | | 7 | 8 |
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- |
| 22 | 1.749 | 1.755 | 1.773 | 1.796 | 1.829 | 1.771 | 1.742 | 1.712 | 1.720 | 1.724 | 1.722 | 1.749 | 1.752 | 1.864 | 1.88 |
| 23 | 2.447 | 2.447 | 2.460 | 2.476 | 2.509 | 2.431 | 2.396 | 2.362 | 2.370 | 2.370 | 2.372 | 2.337 | 2.314 | 2.462 | 2.48 |
| 28 | 2.425 | 2.359 | 2.266 | 2.205 | 2.299 | 2.133 | 2.018 | 1.864 | 1.864 | 1.862 | 1.641 | 1.450 | 1.706 | 2.314 | 2.23 |
| 29 | 3.457 | 3.531 | 3.671 | 3.763 | 3.938 | 3.525 | 3.280 | 3.018 | 3.013 | 3.013 | 2.738 | 2.545 | 2.814 | 3.533 | 3.75 |
| 30 | 4.626 | 4.581 | 4.569 | 4.583 | 4.712 | 4.474 | 4.316 | 4.135 | 4.135 | 4.129 | 3.922 | 3.766 | 3.959 | 4.632 | 4.59 |
| 31 | 4.277 | 4.349 | 4.488 | 4.574 | 4.644 | 4.234 | 4.016 | 3.792 | 3.790 | 3.790 | 3.562 | 3.404 | 3.607 | 4.217 | 4.49 |

VERSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

ERMITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 5°

BELASTUNGSGRAD M/MU

| MESSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.943 | 1.000 |
|-----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | | |
| | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | | |
| ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- |
| 22 | 1.911 | 1.948 | 2.005 | 2.083 | 2.180 | 2.248 | 2.336 | 2.400 | 2.648 | 2.112 |
| 23 | 2.509 | 2.552 | 2.653 | 2.778 | 2.899 | 2.989 | 3.092 | 3.191 | 3.525 | 3.166 |
| 28 | 2.242 | 2.377 | 2.535 | 2.679 | 2.833 | 2.899 | 2.991 | 3.229 | 3.683 | 2.482 |
| 29 | 3.919 | 4.081 | 4.293 | 4.580 | 5.237 | 6.100 | 6.968 | 8.161 | | |
| 30 | 4.649 | 4.755 | 4.850 | 5.029 | 5.273 | 5.464 | 5.624 | 5.784 | 6.435 | 5.571 |
| 31 | 4.632 | 4.792 | 4.907 | 5.100 | 5.394 | 5.669 | 5.893 | 6.125 | 7.244 | 8.250 |

SUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

MITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 7

BELASTUNGSGRAD M/MU

| STELLE | 0.000 | 0.114 | 0.229 | 0.229 | 0.343 | 0.457 | 0.514 | 0.571 | 0.629 | 0.686 | 0.743 | 0.800 | 0.857 | 0.000 | 0.85 |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|
| | | | | ----- | | | | | | | | | | ----- | ----- |
| | | | | 1 | | | | | | | | | | 1 | 1 |
| 1 | -1.037 | -0.152 | -0.138 | -0.130 | -0.140 | -0.095 | -0.079 | -0.113 | -0.037 | -0.070 | -0.042 | -0.009 | 0.012 | -0.138 | -0.02 |
| 2 | -0.117 | -0.103 | -0.083 | -0.083 | -0.072 | -0.058 | -0.050 | -0.044 | -0.037 | -0.027 | -0.017 | -0.005 | 0.012 | -0.091 | 0.00 |
| 3 | -0.064 | -0.056 | -0.019 | -0.040 | -0.032 | -0.017 | -0.011 | -0.003 | 0.007 | 0.018 | 0.030 | 0.044 | 0.063 | -0.013 | 0.05 |
| 4 | -0.094 | -0.088 | -0.072 | -0.072 | -0.066 | -0.049 | -0.041 | -0.035 | -0.027 | -0.016 | -0.008 | 0.002 | 0.014 | -0.043 | 0.00 |
| 7 | -0.099 | -0.101 | -0.093 | -0.083 | -0.071 | -0.081 | -0.058 | -0.056 | -0.050 | -0.056 | -0.040 | -0.046 | -0.019 | -0.038 | -0.04 |
| 8 | -0.111 | -0.093 | -0.097 | -0.056 | -0.075 | -0.093 | -0.036 | -0.060 | -0.105 | -0.068 | -0.070 | -0.083 | -0.048 | 0.026 | 0.01 |
| 9 | -0.051 | -0.063 | -0.063 | -0.063 | -0.074 | -0.080 | -0.084 | -0.092 | -0.092 | -0.096 | -0.098 | -0.100 | -0.092 | -0.029 | -0.09 |
| 11 | -0.060 | -0.052 | -0.046 | -0.044 | -0.040 | -0.032 | -0.026 | -0.024 | -0.019 | -0.019 | -0.024 | -0.030 | -0.036 | -0.026 | -0.01 |
| 12 | -0.088 | -0.082 | -0.070 | -0.072 | -0.070 | -0.060 | -0.056 | -0.054 | -0.052 | -0.049 | -0.056 | -0.064 | -0.070 | -0.054 | -0.08 |
| 13 | 0.033 | 0.031 | 0.033 | 0.031 | 0.025 | 0.023 | 0.023 | 0.019 | 0.017 | 0.019 | 0.025 | 0.019 | 0.019 | 0.076 | 0.05 |
| 14 | -0.031 | -0.045 | -0.037 | -0.035 | -0.041 | -0.047 | -0.047 | -0.052 | -0.054 | -0.062 | -0.076 | -0.086 | -0.066 | -0.003 | -0.07 |
| 15 | -0.060 | -0.068 | -0.068 | -0.064 | -0.074 | -0.083 | -0.081 | -0.085 | -0.089 | -0.089 | -0.087 | -0.083 | -0.085 | -0.036 | -0.09 |
| 16 | -0.251 | -0.341 | -0.444 | -0.456 | -0.563 | -0.688 | -0.760 | -0.824 | -0.896 | -0.986 | -1.074 | -1.202 | -1.345 | -0.520 | -1.43 |
| 19 | -0.253 | -0.354 | -0.460 | -0.471 | -0.584 | -0.711 | -0.787 | -0.855 | -0.931 | -1.025 | -1.113 | -1.241 | -1.382 | -0.508 | -1.45 |
| 22 | 1.873 | 1.844 | 1.844 | 1.801 | 1.795 | 1.760 | 1.772 | 1.758 | 1.754 | 1.737 | 1.764 | 1.766 | 1.797 | 1.610 | 1.67 |
| 24 | -0.754 | -0.683 | -0.600 | -0.598 | -0.518 | -0.424 | -0.371 | -0.321 | -0.266 | -0.200 | -0.124 | -0.009 | 0.334 | -0.697 | 0.37 |
| 27 | -0.583 | -0.489 | -0.409 | -0.362 | -0.282 | -0.191 | -0.138 | -0.091 | -0.027 | 0.028 | 0.113 | 0.293 | 0.624 | -0.495 | 0.53 |
| 28 | 2.310 | 2.371 | 2.437 | 2.449 | 2.515 | 2.583 | 2.634 | 2.673 | 2.718 | 2.765 | 2.843 | 2.936 | 3.119 | 2.349 | 3.12 |
| 29 | 2.283 | 2.342 | 2.408 | 2.412 | 2.476 | 2.554 | 2.597 | 2.636 | 2.683 | 2.732 | 2.792 | 2.896 | 3.085 | 2.311 | 3.09 |
| 30 | 3.860 | 3.911 | 3.974 | 3.966 | 4.014 | 4.075 | 4.108 | 4.139 | 4.176 | 4.221 | 4.272 | 4.348 | 4.463 | 3.944 | 4.51 |
| 31 | 3.721 | 3.770 | 3.819 | 3.821 | 3.868 | 3.926 | 3.959 | 3.987 | 4.026 | 4.068 | 4.117 | 4.174 | 4.334 | 3.725 | 4.33 |

UCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

MITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 7

BELASTUNGSGRAD M/MU

| STELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.686 | 0.571 | 0.400 | 0.400 | 0.400 | 0.100 | 0.000 | 0.429 | 0.857 | 0.857 |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | 2 | 3 | 4 | 5 | 6 | 1 | 1 | 1 | 2 | 3 | | 3 | | 7 | |
| 1 | -0.015 | -0.009 | -0.009 | -0.035 | -0.064 | -0.101 | -0.054 | -0.077 | 0.010 | 0.008 | -0.021 | -0.185 | -0.161 | -0.085 | -0.085 |
| 2 | 0.010 | 0.008 | 0.008 | 0.008 | 0.000 | -0.017 | -0.025 | -0.037 | -0.033 | -0.033 | -0.058 | -0.095 | -0.052 | 0.002 | 0.002 |
| 3 | 0.065 | 0.063 | 0.067 | 0.069 | 0.069 | 0.050 | 0.044 | 0.030 | 0.034 | 0.034 | 0.018 | -0.003 | 0.020 | 0.073 | 0.073 |
| 4 | 0.014 | 0.014 | 0.027 | 0.037 | 0.043 | 0.025 | 0.018 | 0.008 | 0.012 | 0.014 | 0.008 | -0.025 | -0.008 | 0.033 | 0.033 |
| 7 | -0.044 | -0.032 | -0.048 | -0.052 | -0.058 | -0.067 | -0.063 | -0.065 | -0.048 | -0.050 | -0.036 | -0.036 | -0.067 | -0.050 | -0.050 |
| 8 | 0.018 | -0.001 | -0.013 | -0.011 | 0.014 | 0.014 | 0.038 | 0.040 | 0.026 | 0.024 | 0.024 | -0.042 | -0.066 | -0.040 | -0.040 |
| 9 | -0.088 | -0.088 | -0.053 | -0.045 | -0.025 | -0.043 | -0.049 | -0.039 | -0.033 | -0.031 | 0.002 | -0.021 | -0.065 | -0.065 | -0.065 |
| 11 | -0.044 | -0.042 | -0.017 | 0.075 | 0.321 | 0.330 | 0.291 | 0.266 | 0.278 | 0.291 | 0.280 | 0.143 | 0.155 | 0.147 | 0.250 |
| 12 | -0.084 | -0.086 | -0.086 | -0.084 | -0.080 | -0.064 | -0.056 | -0.047 | -0.039 | -0.037 | -0.033 | -0.058 | -0.052 | -0.082 | -0.082 |
| 13 | 0.057 | 0.053 | 0.059 | 0.076 | 0.117 | 0.141 | 0.150 | 0.160 | 0.166 | 0.168 | 0.197 | 0.164 | 0.135 | 0.104 | 0.120 |
| 14 | -0.068 | -0.066 | -0.062 | -0.054 | -0.041 | -0.037 | -0.033 | -0.023 | -0.015 | -0.013 | 0.016 | -0.007 | -0.039 | -0.052 | -0.052 |
| 15 | -0.093 | -0.091 | -0.089 | -0.081 | -0.070 | -0.070 | -0.058 | -0.048 | -0.038 | -0.036 | -0.003 | -0.021 | -0.062 | -0.085 | -0.085 |
| 16 | -1.495 | -1.510 | -1.555 | -1.573 | -1.619 | -1.485 | -1.368 | -1.191 | -1.179 | -1.177 | -0.865 | -0.719 | -1.128 | -1.629 | -1.650 |
| 19 | -1.512 | -1.526 | -1.579 | -1.596 | -1.623 | -1.489 | -1.368 | -1.189 | -1.177 | -1.177 | -0.855 | -0.672 | -1.101 | -1.621 | -1.640 |
| 22 | 1.664 | 1.666 | 1.682 | 1.684 | 1.709 | 1.641 | 1.614 | 1.586 | 1.592 | 1.596 | 1.586 | 1.514 | 1.491 | 1.622 | 1.630 |
| 24 | 0.414 | 0.416 | 0.428 | 0.416 | 0.367 | 0.079 | -0.108 | -0.319 | -0.323 | -0.325 | -0.578 | -0.724 | -0.422 | 0.354 | 0.350 |
| 27 | 0.560 | 0.562 | 0.599 | 0.599 | 0.607 | 0.271 | 0.065 | -0.169 | -0.177 | -0.173 | -0.446 | -0.599 | -0.356 | 0.484 | 0.500 |
| 28 | 3.155 | 3.168 | 3.182 | 3.184 | 3.254 | 3.053 | 2.909 | 2.730 | 2.730 | 2.720 | 2.509 | 2.390 | 2.634 | 3.188 | 3.220 |
| 29 | 3.126 | 3.131 | 3.155 | 3.165 | 3.188 | 2.979 | 2.843 | 2.675 | 2.671 | 2.669 | 2.449 | 2.305 | 2.558 | 3.118 | 3.140 |
| 30 | 4.535 | 4.541 | 4.572 | 4.586 | 4.675 | 4.521 | 4.416 | 4.278 | 4.274 | 4.272 | 4.110 | 3.993 | 4.178 | 4.623 | 4.650 |
| 31 | 4.353 | 4.359 | 4.382 | 4.396 | 4.415 | 4.240 | 4.129 | 3.992 | 3.992 | 3.994 | 3.835 | 3.713 | 3.899 | 4.357 | 4.350 |

VERSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

ERMITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 7

| MESSTELLE | BELASTUNGSGRAD M/MU | | | | | | | | | |
|-----------|---------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.943 | 1.000 |
| | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | | |
| 1 | -0.058 | -0.079 | -0.025 | -0.054 | -0.015 | 0.041 | 0.125 | 0.223 | 0.346 | 0.874 |
| 2 | 0.006 | -0.005 | -0.017 | -0.019 | 0.162 | 0.322 | 0.468 | 0.626 | 0.944 | 2.595 |
| 3 | 0.083 | 0.085 | 0.092 | 0.116 | 0.227 | 0.287 | 0.352 | 0.404 | 0.459 | 1.751 |
| 4 | 0.060 | 0.068 | 0.092 | 0.166 | 0.368 | 0.528 | 0.671 | 0.809 | 1.150 | 1.070 |
| 7 | -0.036 | -0.050 | -0.058 | -0.009 | 0.167 | 0.254 | 0.373 | 0.494 | 0.547 | 0.529 |
| 8 | -0.023 | 0.238 | 0.523 | 0.893 | 0.989 | 1.032 | 1.153 | 1.137 | 1.184 | 0.685 |
| 9 | -0.033 | 0.012 | 0.612 | 0.951 | 1.215 | 1.400 | 1.532 | 1.640 | 1.807 | 0.903 |
| 11 | 0.360 | 0.488 | 0.683 | 0.942 | 1.297 | 1.537 | 1.771 | 1.974 | 2.441 | 2.664 |
| 12 | -0.070 | 0.020 | 0.523 | 0.858 | 1.154 | 1.326 | 1.460 | 1.546 | 1.661 | 1.024 |
| 13 | 0.145 | 0.223 | 0.345 | 0.488 | 0.815 | 1.016 | 1.189 | 1.320 | 1.466 | 0.975 |
| 14 | -0.023 | -0.011 | 0.057 | 0.229 | 0.572 | 0.800 | 0.936 | 1.038 | 1.157 | 0.574 |
| 15 | -0.060 | -0.036 | -0.013 | 0.096 | 0.330 | 0.535 | 0.697 | 0.880 | 1.104 | 0.668 |
| 16 | -1.668 | -1.686 | -1.697 | -1.727 | -1.803 | -1.910 | -1.916 | -1.941 | -2.185 | -3.035 |
| 19 | -1.660 | -1.738 | -1.834 | -1.968 | -2.226 | -2.440 | -2.534 | -2.688 | -3.565 | |
| 22 | 1.653 | 1.709 | 1.748 | 1.818 | 1.907 | 1.965 | 2.033 | 2.086 | 2.201 | 2.127 |
| 24 | 0.336 | 0.412 | 0.621 | 0.839 | 0.974 | 1.089 | 1.149 | 1.209 | 1.478 | 1.671 |
| 27 | 0.499 | 0.562 | 0.669 | 0.780 | 1.000 | 1.242 | 1.349 | 1.464 | 1.805 | 3.162 |
| 28 | 3.256 | 3.328 | 3.470 | 3.632 | 3.852 | 4.012 | 4.110 | 4.184 | 4.433 | 4.466 |
| 29 | 3.161 | 3.217 | 3.441 | 3.615 | 3.839 | 3.999 | 4.087 | 4.145 | 4.356 | 4.638 |
| 30 | 4.677 | 4.759 | 4.896 | 5.053 | 5.285 | 5.445 | 5.558 | 5.689 | 6.161 | 6.285 |
| 31 | 4.402 | 4.466 | 4.671 | 4.870 | 5.127 | 5.334 | 5.488 | 5.638 | 6.053 | 7.562 |

SUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

 MITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 7"

BELASTUNGSGRAD M/MU

| STELLE | 0.000 | 0.114 | 0.229 | 0.229 | 0.343 | 0.457 | 0.514 | 0.571 | 0.629 | 0.686 | 0.743 | 0.800 | 0.857 | 0.000 | 0.857 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | | | ----- | | | | | | | | | | ----- | ----- |
| | | | | 1 | | | | | | | | | | 1 | 1 |
| 23 | 1.255 | 1.253 | 1.243 | 1.241 | 1.230 | 1.218 | 1.210 | 1.206 | 1.200 | 1.193 | 1.206 | 1.224 | 1.269 | 1.173 | 1.29 |
| 28 | 2.320 | 2.381 | 2.447 | 2.449 | 2.513 | 2.593 | 2.636 | 2.677 | 2.732 | 2.827 | 2.962 | 3.118 | 3.278 | 2.326 | 3.27 |
| 29 | 3.035 | 3.100 | 3.164 | 3.166 | 3.232 | 3.308 | 3.345 | 3.388 | 3.441 | 3.525 | 3.673 | 3.831 | 4.045 | 3.061 | 4.19 |
| 30 | 3.433 | 3.496 | 3.545 | 3.554 | 3.628 | 3.687 | 3.724 | 3.759 | 3.798 | 3.866 | 4.007 | 4.176 | 4.359 | 3.504 | 4.42 |
| 31 | 3.821 | 3.862 | 3.909 | 3.911 | 3.954 | 4.009 | 4.040 | 4.069 | 4.106 | 4.159 | 4.295 | 4.453 | 4.642 | 3.782 | 4.64 |

RSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

MITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 7*

BELASTUNGSGRAD M/MU

| ESSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.686 | 0.571 | 0.400 | 0.400 | 0.400 | 0.100 | 0.000 | 0.429 | 0.857 | 0.857 |
|----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- |
| | 2 | 3 | 4 | 5 | 6 | 1 | 1 | 1 | 2 | 3 | | 3 | | 7 | |
| 23 | 1.249 | 1.251 | 1.255 | 1.265 | 1.281 | 1.214 | 1.177 | 1.146 | 1.146 | 1.146 | 1.152 | 1.132 | 1.080 | 1.216 | 1.216 |
| 28 | 3.248 | 3.190 | 3.157 | 3.137 | 3.139 | 2.925 | 2.792 | 2.621 | 2.613 | 2.611 | 2.381 | 2.207 | 2.478 | 3.205 | 3.110 |
| 29 | 4.355 | 4.445 | 4.634 | 4.735 | 4.831 | 4.382 | 4.067 | 3.747 | 3.739 | 3.739 | 3.462 | 3.343 | 3.620 | 4.650 | 4.810 |
| 30 | 4.430 | 4.416 | 4.445 | 4.461 | 4.492 | 4.237 | 4.085 | 3.917 | 3.923 | 3.927 | 3.743 | 3.607 | 3.837 | 4.578 | 4.510 |
| 31 | 4.703 | 4.730 | 4.790 | 4.825 | 4.870 | 4.570 | 4.381 | 4.178 | 4.174 | 4.172 | 3.983 | 3.849 | 4.028 | 4.683 | 4.710 |

VERSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

ERMITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 7*

BELASTUNGSGRAD M/MU

| MESSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.943 | 1.000 |
|-----------|-------|-------|-------|-------|-------|-------|-------|--------|-------|-------|
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | | |
| | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | | |
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- |
| 23 | 1.237 | 1.267 | 1.330 | 1.417 | 1.534 | 1.610 | 1.684 | 1.735 | 1.971 | 2.113 |
| 28 | 3.071 | 3.190 | 3.437 | 3.523 | 3.632 | 3.681 | 3.658 | 3.568 | 3.104 | 2.504 |
| 29 | 5.020 | 5.242 | 5.521 | 5.862 | 6.591 | 7.862 | 9.076 | 10.084 | | |
| 30 | 4.543 | 4.638 | 4.794 | 5.135 | 5.500 | 5.788 | 6.001 | 6.258 | 7.400 | 3.433 |
| 31 | 4.839 | 4.917 | 5.003 | 5.202 | 5.537 | 5.784 | 5.956 | 6.141 | 6.979 | 8.701 |

RSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

MITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 8

BELASTUNGSGRAD M/MU

| MESSSTELLE | 0.000 | 0.114 | 0.229 | 0.229 | 0.343 | 0.457 | 0.514 | 0.571 | 0.629 | 0.686 | 0.743 | 0.800 | 0.857 | 0.900 | 0.950 |
|------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | | | ----- | | | | | | | | | | ----- | ----- |
| | | | | 1 | | | | | | | | | | 1 | 1 |
| 1 | -0.049 | -0.039 | -0.027 | -0.025 | -0.015 | 0.004 | 0.012 | 0.022 | 0.035 | 0.047 | 0.063 | 0.084 | 0.107 | 0.006 | 0.111 |
| 3 | -0.068 | -0.052 | -0.040 | -0.038 | -0.032 | -0.017 | -0.009 | -0.001 | 0.005 | 0.020 | 0.030 | 0.046 | 0.063 | -0.013 | 0.066 |
| 4 | -0.045 | -0.031 | -0.021 | -0.017 | -0.009 | -0.004 | 0.004 | 0.008 | 0.012 | 0.024 | 0.030 | 0.041 | 0.055 | 0.008 | 0.066 |
| 7 | -0.057 | -0.041 | -0.025 | -0.021 | -0.010 | 0.008 | 0.016 | 0.027 | 0.037 | 0.053 | 0.064 | 0.078 | 0.092 | 0.010 | 0.099 |
| 9 | -0.029 | -0.035 | -0.043 | -0.043 | -0.056 | -0.066 | -0.072 | -0.080 | -0.089 | -0.086 | -0.084 | -0.047 | -0.023 | -0.005 | -0.011 |
| 11 | -0.039 | -0.035 | -0.029 | -0.027 | -0.025 | -0.019 | -0.015 | -0.013 | -0.013 | -0.011 | -0.017 | -0.017 | -0.005 | -0.011 | -0.006 |
| 12 | -0.031 | -0.025 | -0.019 | -0.017 | -0.015 | -0.007 | -0.003 | -0.001 | -0.001 | 0.003 | -0.001 | -0.001 | 0.003 | 0.001 | 0.006 |
| 13 | 0.006 | 0.002 | -0.002 | 0.000 | -0.008 | -0.010 | -0.010 | -0.012 | -0.010 | 0.004 | 0.008 | 0.045 | 0.057 | 0.045 | 0.059 |
| 14 | 0.010 | 0.008 | 0.004 | 0.004 | -0.004 | -0.011 | -0.013 | -0.017 | -0.023 | -0.019 | -0.008 | 0.022 | 0.036 | 0.044 | 0.044 |
| 15 | -0.012 | -0.020 | -0.028 | -0.026 | -0.041 | -0.053 | -0.055 | -0.061 | -0.074 | -0.082 | -0.082 | -0.100 | -0.160 | -0.004 | -0.177 |
| 16 | -0.146 | -0.228 | -0.325 | -0.335 | -0.436 | -0.557 | -0.624 | -0.686 | -0.756 | -0.838 | -0.920 | -1.039 | -1.160 | -0.392 | -1.233 |
| 19 | -0.152 | -0.232 | -0.333 | -0.341 | -0.446 | -0.573 | -0.647 | -0.713 | -0.786 | -0.877 | -0.963 | -1.095 | -1.232 | -0.419 | -1.311 |
| 22 | 0.842 | 0.840 | 0.834 | 0.830 | 0.819 | 0.807 | 0.797 | 0.793 | 0.787 | 0.789 | 0.797 | 0.805 | 0.834 | 0.777 | 0.811 |
| 23 | 0.341 | 0.341 | 0.333 | 0.329 | 0.316 | 0.304 | 0.294 | 0.290 | 0.284 | 0.281 | 0.290 | 0.298 | 0.327 | 0.251 | 0.280 |
| 24 | -0.789 | -0.714 | -0.629 | -0.627 | -0.545 | -0.449 | -0.395 | -0.344 | -0.284 | -0.200 | -0.130 | 0.085 | 0.408 | -0.746 | 0.433 |
| 27 | -0.770 | -0.692 | -0.610 | -0.606 | -0.526 | -0.430 | -0.378 | -0.327 | -0.272 | -0.193 | -0.109 | 0.205 | 0.505 | -0.734 | 0.511 |
| 30 | 4.064 | 4.109 | 4.156 | 4.158 | 4.205 | 4.261 | 4.291 | 4.322 | 4.357 | 4.404 | 4.454 | 4.534 | 4.716 | 4.064 | 4.733 |

VERSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

ERMittelTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 8

BELASTUNGSGRAD M/MU

| MESSSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.686 | 0.571 | 0.400 | 0.400 | 0.400 | 0.100 | 0.000 | 0.429 | 0.857 | 0.857 |
|------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|
| | 2 | 3 | 4 | 5 | 6 | 1 | 1 | 1 | 2 | 3 | | 3 | | 7 | 8 |
| 1 | 0.117 | 0.117 | 0.119 | 0.119 | 0.117 | 0.096 | 0.086 | 0.068 | 0.070 | 0.068 | 0.039 | 0.016 | 0.053 | 0.123 | 0.12 |
| 3 | 0.086 | 0.075 | 0.081 | 0.081 | 0.079 | 0.061 | 0.051 | 0.032 | 0.036 | 0.034 | 0.014 | -0.003 | 0.024 | 0.083 | 0.09 |
| 4 | 0.069 | 0.067 | 0.053 | 0.053 | 0.049 | 0.041 | 0.037 | 0.026 | 0.030 | 0.030 | 0.022 | 0.008 | 0.024 | 0.059 | 0.06 |
| 7 | 0.103 | 0.107 | 0.115 | 0.121 | 0.129 | 0.113 | 0.105 | 0.086 | 0.092 | 0.094 | 0.068 | 0.031 | 0.066 | 0.113 | 0.12 |
| 9 | 0.003 | 0.032 | 0.085 | 0.133 | 0.258 | 0.252 | 0.207 | 0.139 | 0.145 | 0.149 | 0.141 | 0.075 | 0.022 | 0.051 | 0.17 |
| 11 | -0.007 | -0.009 | -0.015 | -0.017 | -0.033 | -0.025 | -0.017 | -0.011 | -0.007 | -0.007 | -0.005 | -0.013 | -0.007 | -0.019 | -0.02 |
| 12 | 0.003 | 0.005 | 0.008 | 0.018 | 0.069 | 0.083 | 0.090 | 0.094 | 0.102 | 0.112 | 0.112 | 0.077 | 0.083 | 0.059 | 0.07 |
| 13 | 0.067 | 0.075 | 0.092 | 0.108 | 0.112 | 0.090 | 0.079 | 0.075 | 0.079 | 0.081 | 0.092 | 0.071 | 0.053 | 0.088 | 0.10 |
| 14 | 0.044 | 0.038 | 0.046 | 0.063 | 0.147 | 0.147 | 0.135 | 0.122 | 0.129 | 0.129 | 0.145 | 0.127 | 0.096 | 0.147 | 0.15 |
| 15 | -0.213 | -0.265 | -0.341 | -0.386 | -0.297 | -0.219 | -0.160 | -0.094 | -0.090 | -0.088 | -0.026 | 0.008 | -0.041 | -0.154 | -0.21 |
| 16 | -1.294 | -1.306 | -1.347 | -1.360 | -1.382 | -1.253 | -1.144 | -0.980 | -0.967 | -0.969 | -0.680 | -0.548 | -0.902 | -1.374 | -1.40 |
| 19 | -1.390 | -1.403 | -1.456 | -1.468 | -1.489 | -1.349 | -1.234 | -1.060 | -1.045 | -1.047 | -0.735 | -0.600 | -0.984 | -1.491 | -1.51 |
| 22 | 0.811 | 0.813 | 0.819 | 0.826 | 0.850 | 0.799 | 0.764 | 0.737 | 0.741 | 0.739 | 0.750 | 0.733 | 0.702 | 0.813 | 0.82 |
| 23 | 0.292 | 0.292 | 0.298 | 0.308 | 0.333 | 0.281 | 0.247 | 0.220 | 0.222 | 0.218 | 0.226 | 0.193 | 0.158 | 0.275 | 0.28 |
| 24 | 0.473 | 0.486 | 0.531 | 0.549 | 0.580 | 0.223 | -0.013 | -0.280 | -0.282 | -0.284 | -0.582 | -0.746 | -0.418 | 0.477 | 0.52 |
| 27 | 0.538 | 0.531 | 0.540 | 0.540 | 0.583 | 0.242 | 0.012 | -0.259 | -0.259 | -0.261 | -0.567 | -0.758 | -0.438 | 0.513 | 0.53 |
| 30 | 4.749 | 4.751 | 4.776 | 4.786 | 4.825 | 4.614 | 4.476 | 4.322 | 4.324 | 4.322 | 4.154 | 4.054 | 4.240 | 4.778 | 4.80 |

VERSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

ERMITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 8

BELASTUNGSGRAD M/MU

| MESSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.943 | 1.000 |
|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | | |
| | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | | |
| ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- |
| 1 | 0.127 | 0.125 | 0.131 | 0.150 | 0.265 | 0.341 | 0.406 | 0.476 | 0.642 | 1.877 |
| 3 | 0.090 | 0.094 | 0.094 | 0.106 | 0.200 | 0.262 | 0.309 | 0.361 | 0.467 | 1.975 |
| 4 | 0.065 | 0.061 | 0.061 | 0.094 | 0.234 | 0.330 | 0.410 | 0.484 | 0.564 | 1.234 |
| 7 | 0.138 | 0.148 | 0.158 | 0.222 | 0.398 | 0.493 | 0.544 | 0.567 | 0.653 | 1.183 |
| 9 | 0.291 | 0.420 | 0.492 | 0.613 | 0.792 | 0.899 | 0.987 | 1.081 | 1.396 | 1.925 |
| 11 | -0.029 | -0.021 | 0.211 | 0.579 | 0.981 | 1.193 | 1.357 | 1.507 | 1.642 | 2.002 |
| 12 | 0.102 | 0.207 | 0.361 | 0.550 | 0.817 | 0.987 | 1.116 | 1.235 | 1.459 | 2.882 |
| 13 | 0.120 | 0.155 | 0.330 | 0.615 | 0.927 | 1.141 | 1.307 | 1.486 | 1.761 | 2.110 |
| 14 | 0.188 | 0.305 | 0.408 | 0.533 | 0.712 | 0.831 | 0.925 | 1.010 | 1.170 | 1.578 |
| 15 | -0.226 | 0.082 | 0.669 | 1.029 | 1.392 | 1.620 | 1.819 | 2.055 | 2.232 | 3.706 |
| 16 | -1.409 | -1.460 | -1.522 | -1.598 | -1.659 | -1.727 | -1.709 | -1.676 | -1.715 | -3.454 |
| 19 | -1.524 | -1.561 | -1.579 | -1.624 | -1.684 | -1.774 | -1.805 | -1.860 | -2.388 | -7.162 |
| 22 | 0.842 | 0.907 | 1.004 | 1.129 | 1.289 | 1.379 | 1.453 | 1.525 | 1.774 | 1.677 |
| 23 | 0.298 | 0.345 | 0.402 | 0.453 | 0.523 | 0.566 | 0.607 | 0.642 | 0.796 | 0.550 |
| 24 | 0.560 | 0.609 | 0.759 | 0.909 | 1.116 | 1.274 | 1.369 | 1.467 | 1.816 | 2.991 |
| 27 | 0.556 | 0.632 | 0.702 | 0.763 | 0.963 | 1.164 | 1.281 | 1.388 | 1.804 | 2.160 |
| 30 | 4.819 | 4.875 | 5.043 | 5.265 | 5.499 | 5.690 | 5.825 | 5.981 | 6.573 | 7.854 |

SUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

 MITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT III

BELASTUNGSGRAD M/MU

| STELLE | 0.000 | 0.114 | 0.229 | 0.229 | 0.343 | 0.457 | 0.514 | 0.571 | 0.629 | 0.686 | 0.743 | 0.800 | 0.857 | 0.900 | 0.957 |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | | | ----- | | | | | | | | | | ----- | ----- |
| | | | | 1 | | | | | | | | | | 1 | 1 |
| 1 | -0.068 | -0.054 | -0.040 | -0.042 | -0.032 | -0.015 | -0.007 | 0.001 | 0.010 | 0.020 | 0.028 | 0.038 | 0.051 | -0.027 | 0.069 |
| 2 | -0.033 | -0.023 | -0.015 | -0.013 | -0.009 | 0.001 | 0.006 | 0.012 | 0.016 | 0.026 | 0.034 | 0.045 | 0.055 | -0.001 | 0.057 |
| 3 | -0.066 | -0.052 | -0.042 | -0.042 | -0.034 | -0.017 | -0.011 | -0.003 | 0.003 | 0.012 | 0.020 | 0.030 | 0.040 | -0.032 | 0.036 |
| 4 | -0.057 | -0.045 | -0.033 | -0.033 | -0.023 | -0.006 | 0.002 | 0.008 | 0.016 | 0.027 | 0.033 | 0.043 | 0.051 | -0.016 | 0.049 |
| 7 | -0.053 | -0.035 | -0.017 | -0.017 | -0.004 | 0.014 | 0.025 | 0.033 | 0.043 | 0.055 | 0.064 | 0.076 | 0.088 | 0.002 | 0.084 |
| 8 | 0.035 | 0.037 | 0.033 | 0.033 | 0.023 | 0.021 | 0.017 | 0.012 | 0.008 | 0.006 | 0.000 | -0.004 | -0.006 | 0.057 | -0.014 |
| 11 | -0.025 | -0.017 | -0.011 | -0.009 | -0.005 | 0.007 | 0.011 | 0.018 | 0.024 | 0.032 | 0.040 | 0.053 | 0.069 | 0.016 | 0.073 |
| 12 | -0.037 | -0.029 | -0.023 | -0.023 | -0.017 | -0.005 | -0.001 | 0.006 | 0.012 | 0.020 | 0.028 | 0.043 | 0.061 | 0.004 | 0.065 |
| 13 | 0.006 | 0.006 | 0.002 | 0.002 | -0.004 | -0.006 | -0.010 | -0.012 | -0.017 | -0.019 | -0.025 | -0.033 | -0.035 | 0.018 | -0.037 |
| 14 | -0.010 | -0.004 | -0.004 | -0.004 | -0.006 | -0.008 | -0.008 | -0.010 | -0.012 | -0.014 | -0.016 | -0.020 | -0.024 | 0.012 | -0.035 |
| 15 | -0.029 | -0.029 | -0.033 | -0.035 | -0.041 | -0.050 | -0.054 | -0.056 | -0.062 | -0.066 | -0.068 | -0.070 | -0.064 | -0.013 | -0.076 |
| 16 | -0.119 | -0.174 | -0.246 | -0.255 | -0.328 | -0.421 | -0.468 | -0.511 | -0.558 | -0.616 | -0.663 | -0.725 | -0.780 | -0.224 | -0.817 |
| 19 | -0.101 | -0.161 | -0.239 | -0.245 | -0.325 | -0.421 | -0.473 | -0.518 | -0.571 | -0.631 | -0.684 | -0.752 | -0.814 | -0.220 | -0.857 |
| 22 | 1.355 | 1.355 | 1.349 | 1.349 | 1.343 | 1.330 | 1.326 | 1.324 | 1.318 | 1.312 | 1.312 | 1.308 | 1.310 | 1.318 | 1.287 |
| 23 | 1.279 | 1.283 | 1.279 | 1.277 | 1.271 | 1.261 | 1.256 | 1.254 | 1.248 | 1.242 | 1.242 | 1.238 | 1.242 | 1.248 | 1.217 |
| 24 | -0.708 | -0.645 | -0.581 | -0.579 | -0.515 | -0.446 | -0.407 | -0.370 | -0.331 | -0.288 | -0.244 | -0.173 | -0.103 | -0.678 | -0.119 |
| 27 | -0.706 | -0.643 | -0.579 | -0.577 | -0.511 | -0.442 | -0.403 | -0.366 | -0.329 | -0.288 | -0.247 | -0.197 | -0.123 | -0.672 | -0.136 |
| 28 | 1.591 | 1.658 | 1.705 | 1.712 | 1.775 | 1.829 | 1.870 | 1.909 | 1.946 | 1.972 | 2.013 | 2.050 | 2.106 | 1.695 | 2.104 |
| 29 | 2.454 | 2.503 | 2.552 | 2.554 | 2.603 | 2.657 | 2.688 | 2.716 | 2.747 | 2.780 | 2.813 | 2.852 | 2.899 | 2.480 | 2.885 |
| 30 | 4.016 | 4.052 | 4.087 | 4.087 | 4.120 | 4.159 | 4.180 | 4.202 | 4.223 | 4.243 | 4.268 | 4.293 | 4.321 | 4.014 | 4.303 |
| 31 | 3.234 | 3.270 | 3.305 | 3.303 | 3.336 | 3.375 | 3.394 | 3.416 | 3.437 | 3.457 | 3.478 | 3.494 | 3.521 | 3.213 | 3.496 |

VERSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

ERMITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 11

BELASTUNGSGRAD M/MU

| MESSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.943 | 1.000 |
|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | | |
| 1 | 0.077 | 0.081 | 0.088 | 0.096 | 0.147 | 0.180 | 0.240 | 0.272 | 0.305 | 0.301 |
| 2 | 0.147 | 0.160 | 0.176 | 0.207 | 0.346 | 0.431 | 0.589 | 0.691 | 0.734 | 0.544 |
| 3 | 0.053 | 0.053 | 0.063 | 0.085 | 0.211 | 0.278 | 0.334 | 0.377 | 0.398 | 0.301 |
| 4 | 0.057 | 0.057 | 0.049 | 0.043 | 0.047 | 0.051 | 0.088 | 0.101 | 0.107 | 0.115 |
| 7 | 0.127 | 0.133 | 0.213 | 0.318 | 0.448 | 0.491 | 0.534 | 0.563 | 0.599 | 0.476 |
| 8 | -0.008 | 0.061 | 0.170 | 0.306 | 0.494 | 0.811 | 0.959 | 1.071 | 1.199 | 0.841 |
| 11 | 0.065 | 0.050 | 0.026 | 0.026 | 0.077 | 0.106 | 0.213 | 0.248 | 0.241 | 0.223 |
| 12 | 0.240 | 0.291 | 0.589 | 0.940 | 1.090 | 1.176 | 1.258 | 1.312 | 1.379 | 0.956 |
| 13 | -0.043 | -0.045 | -0.037 | -0.006 | 0.063 | 0.123 | 0.188 | 0.240 | 0.330 | 0.258 |
| 14 | 0.501 | 0.599 | 0.721 | 1.088 | 1.341 | 1.486 | 1.581 | 1.663 | 1.764 | 1.236 |
| 15 | -0.070 | -0.054 | -0.009 | 0.445 | 0.687 | 0.804 | 0.888 | 0.975 | 1.079 | 0.806 |
| 16 | -0.912 | -0.951 | -0.994 | -1.064 | -1.172 | -1.244 | -1.267 | -1.304 | -1.489 | -1.417 |
| 19 | -0.883 | -0.873 | -0.865 | -0.853 | -0.824 | -0.824 | -0.814 | -0.820 | -0.906 | -0.887 |
| 22 | 1.281 | 1.289 | 1.304 | 1.332 | 1.375 | 1.406 | 1.435 | 1.459 | 1.554 | 1.422 |
| 23 | 1.236 | 1.252 | 1.324 | 1.426 | 1.494 | 1.545 | 1.603 | 1.642 | 1.693 | 1.373 |
| 24 | -0.074 | -0.064 | -0.045 | -0.017 | 0.082 | 0.127 | 0.279 | 0.353 | 0.612 | 0.232 |
| 27 | 0.059 | 0.152 | 0.363 | 0.450 | 0.546 | 0.638 | 0.694 | 0.780 | 0.975 | 0.439 |
| 28 | 2.059 | 2.112 | 2.159 | 2.252 | 2.371 | 2.434 | 2.471 | 2.508 | 2.603 | 2.217 |
| 29 | 2.944 | 2.979 | 3.035 | 3.150 | 3.308 | 3.404 | 3.464 | 3.509 | 3.622 | 3.143 |
| 30 | 4.342 | 4.373 | 4.426 | 4.467 | 4.533 | 4.588 | 4.644 | 4.685 | 4.839 | 4.603 |
| 31 | 3.671 | 3.714 | 3.774 | 3.979 | 4.223 | 4.383 | 4.488 | 4.572 | 4.759 | 4.049 |

SUCHSBALKEN SETMD1 GEPRUEFT AM 19. 5. 1978

MITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT

BELASTUNGSGRAD M/MU

| SSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.686 | 0.571 | 0.400 | 0.400 | 0.400 | 0.100 | 0.000 | 0.429 | 0.857 | 0.857 |
|---------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | | ----- | | ----- | ----- |
| | 2 | 3 | 4 | 5 | 6 | 1 | 1 | 1 | 2 | 3 | | 3 | | 7 | 8 |
| 1 | 0.053 | 0.055 | 0.061 | 0.063 | 0.067 | 0.055 | 0.049 | 0.032 | 0.034 | 0.034 | 0.014 | -0.019 | 0.010 | 0.063 | 0.071 |
| 2 | 0.059 | 0.059 | 0.069 | 0.071 | 0.077 | 0.073 | 0.069 | 0.061 | 0.063 | 0.065 | 0.071 | 0.061 | 0.090 | 0.135 | 0.141 |
| 3 | 0.036 | 0.038 | 0.042 | 0.044 | 0.046 | 0.032 | 0.028 | 0.014 | 0.016 | 0.016 | -0.003 | -0.025 | 0.001 | 0.046 | 0.041 |
| 4 | 0.051 | 0.051 | 0.051 | 0.051 | 0.049 | 0.041 | 0.035 | 0.023 | 0.023 | 0.021 | 0.000 | -0.018 | 0.008 | 0.051 | 0.051 |
| 7 | -0.084 | 0.086 | 0.094 | 0.101 | 0.109 | 0.101 | 0.094 | 0.082 | 0.084 | 0.086 | 0.061 | 0.022 | 0.064 | 0.113 | 0.121 |
| 8 | -0.020 | -0.020 | -0.020 | -0.022 | -0.020 | -0.006 | 0.004 | 0.021 | 0.027 | 0.023 | 0.051 | 0.045 | 0.012 | -0.014 | -0.010 |
| 11 | 0.071 | 0.067 | 0.063 | 0.057 | 0.048 | 0.046 | 0.046 | 0.040 | 0.038 | 0.034 | 0.022 | 0.014 | 0.042 | 0.081 | 0.071 |
| 12 | 0.077 | 0.102 | 0.160 | 0.186 | 0.225 | 0.221 | 0.213 | 0.195 | 0.201 | 0.209 | 0.180 | 0.075 | 0.114 | 0.182 | 0.201 |
| 13 | -0.041 | -0.043 | -0.047 | -0.051 | -0.058 | -0.037 | -0.021 | -0.004 | -0.002 | -0.004 | 0.014 | 0.012 | -0.008 | -0.037 | -0.034 |
| 14 | -0.022 | -0.006 | 0.115 | 0.279 | 0.445 | 0.417 | 0.378 | 0.324 | 0.337 | 0.355 | 0.308 | 0.193 | 0.195 | 0.339 | 0.410 |
| 15 | -0.072 | -0.076 | -0.084 | -0.086 | -0.089 | -0.078 | -0.068 | -0.054 | -0.052 | -0.052 | -0.023 | -0.021 | -0.056 | -0.072 | -0.072 |
| 16 | -0.644 | -0.852 | -0.881 | -0.891 | -0.910 | -0.815 | -0.739 | -0.620 | -0.612 | -0.612 | -0.390 | -0.298 | -0.581 | -0.689 | -0.901 |
| 19 | -0.883 | -0.885 | -0.908 | -0.902 | -0.894 | -0.793 | -0.715 | -0.594 | -0.586 | -0.584 | -0.349 | -0.265 | -0.565 | -0.694 | -0.894 |
| 22 | 1.283 | 1.281 | 1.277 | 1.277 | 1.277 | 1.269 | 1.269 | 1.269 | 1.273 | 1.271 | 1.304 | 1.293 | 1.271 | 1.277 | 1.277 |
| 23 | 1.215 | 1.217 | 1.222 | 1.230 | 1.238 | 1.230 | 1.228 | 1.224 | 1.228 | 1.232 | 1.244 | 1.207 | 1.189 | 1.213 | 1.224 |
| 24 | -0.099 | -0.099 | -0.084 | -0.080 | -0.070 | -0.177 | -0.263 | -0.388 | -0.390 | -0.394 | -0.573 | -0.684 | -0.446 | -0.095 | -0.080 |
| 27 | -0.113 | -0.103 | -0.084 | -0.041 | 0.043 | -0.086 | -0.191 | -0.335 | -0.337 | -0.335 | -0.534 | -0.672 | -0.435 | -0.019 | 0.016 |
| 28 | 2.104 | 2.120 | 2.143 | 2.170 | 2.213 | 2.112 | 2.069 | 1.979 | 1.979 | 2.009 | 1.851 | 1.638 | 1.804 | 2.018 | 2.030 |
| 29 | 2.897 | 2.897 | 2.918 | 2.930 | 2.959 | 2.854 | 2.784 | 2.688 | 2.686 | 2.683 | 2.540 | 2.448 | 2.628 | 2.913 | 2.930 |
| 30 | 4.313 | 4.315 | 4.332 | 4.338 | 4.350 | 4.284 | 4.241 | 4.176 | 4.180 | 4.178 | 4.083 | 4.002 | 4.128 | 4.309 | 4.326 |
| 31 | 3.505 | 3.507 | 3.546 | 3.570 | 3.601 | 3.513 | 3.449 | 3.365 | 3.357 | 3.357 | 3.234 | 3.174 | 3.353 | 3.591 | 3.634 |

SUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

 MITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 11*

BELASTUNGSGRAD M/MU

| SSTELLE | 0.000 | 0.114 | 0.229 | 0.229 | 0.343 | 0.457 | 0.514 | 0.571 | 0.629 | 0.686 | 0.743 | 0.800 | 0.857 | 0.000 | 0.857 |
|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | | | ----- | | | | | | | | | | ----- | ----- |
| | | | | 1 | | | | | | | | | | 1 | 1 |
| 23 | 0.285 | 0.391 | 0.406 | 0.317 | 0.149 | 0.377 | 0.397 | 0.404 | 0.393 | 0.367 | 0.363 | 0.358 | 0.358 | 0.162 | 0.307 |
| 28 | 2.407 | 2.454 | 2.501 | 2.505 | 2.548 | 2.604 | 2.632 | 2.661 | 2.690 | 2.725 | 2.756 | 2.790 | 2.836 | 2.413 | 2.814 |
| 30 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 |

SUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

 MITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 11*

| | BELASTUNGSGRAD M/MU | | | | | | | | | | | | | | |
|--------|---------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| STELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.686 | 0.571 | 0.400 | 0.400 | 0.400 | 0.100 | 0.000 | 0.429 | 0.857 | 0.657 |
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | | ----- | | ----- | ----- |
| | 2 | 3 | 4 | 5 | 6 | 1 | 1 | 1 | 2 | 3 | | 3 | | 7 | 8 |
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- |
| 23 | 0.467 | 0.478 | 0.443 | 0.238 | 0.441 | 0.451 | 0.506 | 0.504 | 0.313 | 0.525 | 0.531 | 0.716 | 0.712 | 0.728 | 0.738 |
| 28 | 2.825 | 2.827 | 2.848 | 2.858 | 2.881 | 2.790 | 2.733 | 2.647 | 2.643 | 2.641 | 2.505 | 2.407 | 2.587 | 2.654 | 2.866 |
| 30 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 |

VERSUCHSBALKEN SETMQ GEPRUEFT AM 19. 5. 1978

ERMITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 11*

| BELASTUNGSGRAD M/MU | | | | | | | | | | |
|---------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| MESSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.943 | 1.000 |
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | | |
| | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | | |
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- |
| 23 | 0.749 | 0.765 | 0.859 | 0.976 | 1.038 | 1.081 | 1.170 | 1.215 | 1.268 | 0.927 |
| 28 | 2.873 | 2.922 | 2.963 | 3.096 | 3.224 | 3.304 | 3.353 | 3.386 | 3.482 | 3.059 |
| 30 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 | 1.799 |

BUCHSALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

MITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 13

BELASTUNGSGRAD M/MU

| STELLE | 0.000 | 0.114 | 0.229 | 0.229 | 0.343 | 0.457 | 0.514 | 0.571 | 0.629 | 0.686 | 0.743 | 0.800 | 0.857 | 0.000 | 0.857 |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | | | ----- | | | | | | | | | | ----- | ----- |
| | | | | 1 | | | | | | | | | | 1 | 1 |
| 1 | -0.045 | -0.033 | -0.023 | -0.021 | -0.015 | -0.002 | 0.002 | 0.006 | 0.008 | 0.012 | 0.014 | 0.018 | 0.022 | -0.021 | 0.016 |
| 2 | -0.060 | -0.050 | -0.042 | -0.040 | -0.036 | -0.026 | -0.021 | -0.019 | -0.015 | -0.011 | -0.009 | -0.007 | -0.003 | -0.046 | -0.011 |
| 3 | -0.062 | -0.048 | -0.042 | -0.038 | -0.036 | -0.028 | -0.021 | -0.019 | -0.015 | -0.013 | -0.011 | -0.007 | -0.005 | -0.040 | -0.013 |
| 4 | -0.031 | -0.021 | -0.015 | -0.013 | -0.009 | 0.001 | 0.005 | 0.008 | 0.010 | 0.014 | 0.016 | 0.020 | 0.024 | -0.005 | 0.020 |
| 7 | -0.057 | -0.045 | -0.039 | -0.035 | -0.033 | -0.023 | -0.018 | -0.014 | -0.010 | -0.006 | -0.004 | 0.000 | 0.000 | -0.033 | -0.004 |
| 8 | 0.004 | 0.008 | 0.006 | 0.008 | 0.004 | 0.004 | 0.004 | 0.004 | 0.002 | 0.002 | 0.000 | -0.002 | -0.002 | 0.016 | -0.008 |
| 9 | 0.025 | 0.027 | 0.027 | 0.029 | 0.025 | 0.027 | 0.027 | 0.027 | 0.025 | 0.025 | 0.023 | 0.021 | 0.021 | 0.043 | 0.015 |
| 11 | 0.025 | 0.033 | 0.037 | 0.039 | 0.039 | 0.047 | 0.051 | 0.053 | 0.055 | 0.059 | 0.061 | 0.068 | 0.082 | 0.059 | 0.096 |
| 12 | -0.047 | -0.039 | -0.035 | -0.033 | -0.033 | -0.025 | -0.021 | -0.017 | -0.013 | -0.011 | -0.004 | 0.002 | 0.006 | -0.019 | 0.006 |
| 13 | 0.004 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.018 | 0.002 |
| 14 | -0.004 | 0.002 | 0.002 | 0.004 | 0.000 | 0.002 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.006 | 0.010 | 0.004 |
| 15 | 0.339 | 0.347 | 0.345 | 0.343 | 0.337 | 0.335 | 0.333 | 0.333 | 0.331 | 0.327 | 0.325 | 0.323 | 0.323 | 0.351 | 0.497 |
| 16 | -0.107 | -0.140 | -0.183 | -0.185 | -0.234 | -0.286 | -0.312 | -0.339 | -0.368 | -0.399 | -0.425 | -0.456 | -0.485 | -0.158 | -0.497 |
| 19 | -0.115 | -0.148 | -0.191 | -0.193 | -0.240 | -0.287 | -0.314 | -0.339 | -0.366 | -0.396 | -0.421 | -0.452 | -0.478 | -0.164 | -0.493 |
| 22 | 4.842 | 4.854 | 4.824 | 4.889 | 4.903 | 4.887 | 4.887 | 4.895 | 4.885 | 4.856 | 4.842 | 4.830 | 4.803 | 5.014 | 5.000 |
| 23 | 1.314 | 1.320 | 1.318 | 1.320 | 1.314 | 1.312 | 1.312 | 1.310 | 1.308 | 1.306 | 1.304 | 1.300 | 1.300 | 1.306 | 1.263 |
| 24 | -0.768 | -0.729 | -0.695 | -0.693 | -0.658 | -0.619 | -0.596 | -0.578 | -0.559 | -0.536 | -0.518 | -0.497 | -0.475 | -0.756 | -0.491 |
| 27 | -0.772 | -0.731 | -0.697 | -0.694 | -0.662 | -0.621 | -0.600 | -0.582 | -0.561 | -0.540 | -0.522 | -0.499 | -0.479 | -0.753 | -0.489 |
| 28 | 2.368 | 2.323 | 2.347 | 2.341 | 2.362 | 2.388 | 2.409 | 2.421 | 2.435 | 2.456 | 2.470 | 2.476 | 2.493 | 2.288 | 2.464 |
| 29 | 2.421 | 2.370 | 2.392 | 2.384 | 2.405 | 2.431 | 2.451 | 2.464 | 2.476 | 2.496 | 2.509 | 2.515 | 2.531 | 2.341 | 2.511 |
| 30 | 4.507 | 4.458 | 4.472 | 4.468 | 4.484 | 4.503 | 4.525 | 4.537 | 4.543 | 4.554 | 4.564 | 4.558 | 4.566 | 4.452 | 4.572 |
| 31 | 3.700 | 3.645 | 3.663 | 3.653 | 3.669 | 3.688 | 3.704 | 3.714 | 3.722 | 3.739 | 3.747 | 3.747 | 3.759 | 3.612 | 3.736 |

MITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 13

| BELASTUNGSGRAD M/MU | | | | | | | | | | | | | | | |
|---------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| STELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.686 | 0.571 | 0.400 | 0.400 | 0.400 | 0.100 | 0.000 | 0.429 | 0.857 | 0.857 |
| | 2 | 3 | 4 | 5 | 6 | 1 | 1 | 1 | 2 | 3 | | 3 | | 7 | 8 |
| 1 | 0.016 | 0.016 | 0.018 | 0.018 | 0.018 | 0.014 | 0.010 | 0.006 | 0.012 | 0.012 | 0.004 | -0.025 | 0.000 | 0.012 | 0.018 |
| 2 | -0.011 | -0.013 | -0.011 | -0.011 | -0.013 | -0.017 | -0.021 | -0.026 | -0.019 | -0.017 | -0.024 | -0.046 | -0.028 | -0.013 | -0.009 |
| 3 | -0.015 | -0.017 | -0.015 | -0.013 | -0.013 | -0.017 | -0.023 | -0.028 | -0.023 | -0.023 | -0.034 | -0.042 | -0.030 | -0.015 | -0.011 |
| 4 | 0.018 | 0.018 | 0.016 | 0.012 | 0.008 | 0.008 | 0.005 | 0.001 | 0.005 | 0.005 | -0.003 | -0.011 | 0.001 | 0.010 | 0.012 |
| 7 | -0.004 | -0.004 | 0.004 | 0.012 | 0.025 | 0.025 | 0.018 | 0.014 | 0.018 | 0.018 | 0.006 | -0.014 | 0.002 | 0.018 | 0.027 |
| 8 | -0.010 | -0.010 | -0.008 | -0.006 | -0.006 | 0.000 | 0.002 | 0.010 | 0.012 | 0.012 | 0.020 | 0.014 | 0.002 | -0.010 | -0.006 |
| 9 | 0.013 | 0.013 | 0.017 | 0.031 | 0.043 | 0.053 | 0.055 | 0.061 | 0.068 | 0.070 | 0.080 | 0.133 | 0.051 | 0.045 | 0.051 |
| 11 | 0.096 | 0.094 | 0.098 | 0.094 | 0.088 | 0.084 | 0.080 | 0.076 | 0.080 | 0.078 | 0.096 | 0.082 | 0.098 | 0.125 | 0.127 |
| 12 | 0.016 | 0.039 | 0.100 | 0.156 | 0.207 | 0.207 | 0.195 | 0.176 | 0.187 | 0.195 | 0.166 | 0.065 | 0.100 | 0.166 | 0.199 |
| 13 | 0.002 | 0.002 | 0.004 | 0.006 | 0.006 | 0.010 | 0.012 | 0.016 | 0.020 | 0.022 | 0.032 | 0.016 | 0.010 | 0.004 | 0.010 |
| 14 | 0.004 | 0.014 | 0.090 | 0.223 | 0.312 | 0.312 | 0.295 | 0.269 | 0.279 | 0.293 | 0.254 | 0.133 | 0.158 | 0.256 | 0.299 |
| 15 | 0.501 | 0.501 | 0.451 | 0.460 | 0.468 | 0.488 | 0.488 | 0.495 | 0.495 | 0.665 | 0.714 | 0.474 | 0.801 | 0.788 | 0.794 |
| 16 | -0.514 | -0.518 | -0.532 | -0.538 | -0.551 | -0.497 | -0.454 | -0.386 | -0.380 | -0.382 | -0.255 | -0.197 | -0.366 | -0.544 | -0.548 |
| 19 | -0.507 | -0.507 | -0.505 | -0.495 | -0.483 | -0.427 | -0.390 | -0.329 | -0.320 | -0.316 | -0.201 | -0.185 | -0.339 | -0.495 | -0.489 |
| 22 | 5.045 | 5.039 | 5.059 | 5.059 | 5.059 | 5.067 | 5.084 | 5.090 | 5.082 | 5.076 | 5.074 | 5.336 | 5.394 | 5.340 | 5.358 |
| 23 | 1.279 | 1.277 | 1.265 | 1.263 | 1.259 | 1.261 | 1.261 | 1.265 | 1.273 | 1.271 | 1.283 | 1.267 | 1.257 | 1.240 | 1.244 |
| 24 | -0.487 | -0.487 | -0.483 | -0.479 | -0.475 | -0.520 | -0.553 | -0.606 | -0.602 | -0.604 | -0.697 | -0.762 | -0.633 | -0.495 | -0.485 |
| 27 | -0.483 | -0.481 | -0.458 | -0.450 | -0.444 | -0.493 | -0.530 | -0.590 | -0.588 | -0.586 | -0.684 | -0.776 | -0.621 | -0.464 | -0.440 |
| 28 | 2.474 | 2.476 | 2.472 | 2.482 | 2.487 | 2.462 | 2.439 | 2.402 | 2.419 | 2.427 | 2.380 | 2.319 | 2.274 | 2.372 | 2.304 |
| 29 | 2.515 | 2.513 | 2.501 | 2.509 | 2.513 | 2.482 | 2.455 | 2.419 | 2.425 | 2.421 | 2.370 | 2.335 | 2.304 | 2.409 | 2.335 |
| 30 | 4.587 | 4.595 | 4.580 | 4.591 | 4.591 | 4.566 | 4.566 | 4.546 | 4.554 | 4.562 | 4.535 | 4.525 | 4.478 | 4.537 | 4.468 |
| 31 | 3.736 | 3.741 | 3.728 | 3.767 | 3.794 | 3.765 | 3.743 | 3.704 | 3.714 | 3.720 | 3.669 | 3.597 | 3.552 | 3.655 | 3.593 |

VERSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

ERMITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT. 13

BELASTUNGSGRAD M/MU

| MESSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.943 | 1.000 |
|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | | |
| | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | | |
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- |
| 1 | 0.020 | 0.024 | 0.024 | 0.045 | 0.067 | 0.100 | 0.174 | 0.228 | 0.244 | 0.187 |
| 2 | -0.009 | -0.005 | -0.005 | 0.182 | 0.383 | 0.482 | 0.582 | 0.664 | 0.693 | 0.436 |
| 3 | -0.011 | -0.011 | -0.009 | 0.151 | 0.459 | 0.539 | 0.642 | 0.718 | 0.740 | 0.375 |
| 4 | 0.010 | 0.010 | 0.003 | 0.003 | 0.001 | 0.003 | 0.016 | 0.024 | 0.026 | 0.034 |
| 7 | 0.035 | 0.049 | 0.099 | 0.257 | 0.441 | 0.503 | 0.581 | 0.643 | 0.674 | 0.425 |
| 8 | -0.006 | -0.004 | -0.004 | -0.010 | 0.047 | 0.106 | 0.168 | 0.223 | 0.250 | 0.149 |
| 9 | 0.059 | 0.072 | 0.115 | 0.240 | 0.521 | 0.753 | 0.961 | 1.057 | 1.113 | 0.544 |
| 11 | 0.119 | 0.111 | 0.092 | 0.080 | 0.096 | 0.109 | 0.150 | 0.176 | 0.181 | 0.189 |
| 12 | 0.234 | 0.304 | 0.454 | 0.581 | 1.031 | 1.152 | 1.265 | 1.324 | 1.359 | 0.694 |
| 13 | 0.014 | 0.016 | 0.014 | 0.004 | 0.108 | 0.231 | 0.369 | 0.463 | 0.494 | 0.293 |
| 14 | 0.351 | 0.431 | 0.575 | 0.724 | 0.883 | 0.956 | 1.035 | 1.086 | 1.117 | 0.605 |
| 15 | 0.801 | 0.809 | 0.837 | 0.876 | 1.197 | 1.310 | 1.076 | 1.154 | 1.213 | 0.778 |
| 16 | -0.557 | -0.573 | -0.600 | -0.649 | -0.666 | -0.686 | -0.672 | -0.680 | -0.746 | -0.567 |
| 19 | -0.481 | -0.462 | -0.419 | -0.359 | -0.292 | -0.181 | -0.083 | -0.031 | -0.035 | -0.214 |
| 22 | 5.330 | 5.349 | 5.402 | 5.363 | 5.332 | 5.260 | 5.279 | 5.236 | 5.172 | 5.158 |
| 23 | 1.246 | 1.244 | 1.242 | 1.271 | 1.424 | 1.482 | 1.550 | 1.593 | 1.603 | 1.240 |
| 24 | -0.483 | -0.471 | -0.467 | -0.460 | -0.463 | -0.465 | -0.448 | -0.450 | -0.432 | -0.460 |
| 27 | -0.430 | -0.419 | -0.405 | -0.384 | -0.204 | -0.070 | 0.127 | 0.217 | 0.318 | -0.386 |
| 28 | 2.317 | 2.325 | 2.339 | 2.360 | 2.419 | 2.443 | 2.487 | 2.503 | 2.515 | 2.306 |
| 29 | 2.341 | 2.335 | 2.347 | 2.349 | 2.449 | 2.486 | 2.546 | 2.572 | 2.583 | 2.343 |
| 30 | 4.476 | 4.472 | 4.486 | 4.476 | 4.642 | 4.895 | 5.051 | 5.098 | 5.090 | 4.923 |
| 31 | 3.614 | 3.626 | 3.686 | 3.763 | 3.841 | 3.886 | 3.954 | 3.977 | 3.977 | 3.569 |

UCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

MITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 15

BELASTUNGSGRAD M/MU

| STELLE | 0.000 | 0.114 | 0.229 | 0.229 | 0.343 | 0.457 | 0.514 | 0.571 | 0.629 | 0.686 | 0.743 | 0.800 | 0.857 | 0.000 | 0.85 |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | | | ----- | | | | | | | | | | ----- | ----- |
| | | | | 1 | | | | | | | | | | 1 | 1 |
| 1 | 0.053 | -0.015 | -0.011 | -0.019 | -0.019 | -0.017 | -0.007 | -0.004 | -0.004 | 0.004 | 0.004 | -0.002 | 0.000 | -0.013 | -0.017 |
| 2 | 0.062 | -0.006 | 0.000 | -0.010 | -0.010 | -0.006 | 0.005 | 0.007 | 0.007 | 0.017 | 0.015 | 0.009 | 0.011 | -0.008 | -0.004 |
| 3 | 0.158 | 0.090 | 0.094 | 0.078 | 0.076 | 0.078 | 0.088 | 0.090 | 0.092 | 0.098 | 0.098 | 0.092 | 0.094 | 0.076 | 0.131 |
| 4 | 0.000 | -0.064 | -0.057 | -0.068 | -0.068 | -0.064 | -0.053 | -0.051 | -0.049 | -0.043 | -0.043 | -0.045 | -0.041 | -0.051 | -0.049 |
| 7 | 0.014 | -0.054 | -0.050 | -0.058 | -0.060 | -0.056 | -0.046 | -0.043 | -0.041 | -0.035 | -0.035 | -0.041 | -0.039 | -0.052 | -0.056 |
| 8 | 0.021 | 0.027 | 0.029 | 0.031 | 0.027 | 0.029 | 0.031 | 0.031 | 0.031 | 0.031 | 0.029 | 0.029 | 0.029 | 0.039 | 0.021 |
| 9 | -0.029 | 0.016 | 0.014 | 0.022 | 0.026 | 0.022 | 0.022 | 0.020 | 0.030 | 0.022 | 0.020 | 0.024 | 0.020 | 0.020 | 0.026 |
| 11 | -0.097 | -0.065 | -0.063 | -0.034 | -0.024 | -0.036 | -0.011 | -0.007 | 0.011 | 0.013 | 0.026 | 0.042 | 0.063 | 0.007 | 0.063 |
| 12 | -0.064 | -0.013 | -0.025 | -0.017 | -0.009 | -0.003 | 0.003 | 0.005 | 0.026 | 0.028 | 0.034 | 0.063 | 0.071 | 0.020 | 0.092 |
| 13 | -0.084 | -0.050 | -0.066 | -0.035 | -0.029 | -0.027 | -0.023 | -0.025 | -0.013 | -0.019 | -0.019 | -0.011 | -0.013 | -0.035 | -0.019 |
| 14 | -0.080 | -0.068 | -0.041 | -0.035 | -0.027 | -0.027 | -0.023 | -0.025 | -0.013 | -0.029 | -0.017 | -0.025 | -0.009 | -0.031 | -0.033 |
| 15 | 0.002 | 0.026 | 0.018 | 0.026 | 0.024 | 0.016 | 0.012 | 0.008 | 0.014 | 0.002 | -0.002 | 0.000 | -0.006 | 0.036 | 0.000 |
| 16 | -0.199 | -0.191 | -0.193 | -0.193 | -0.203 | -0.222 | -0.215 | -0.228 | -0.234 | -0.238 | -0.244 | -0.248 | -0.250 | -0.160 | -0.263 |
| 19 | -0.197 | -0.191 | -0.195 | -0.197 | -0.209 | -0.228 | -0.222 | -0.236 | -0.242 | -0.248 | -0.254 | -0.259 | -0.265 | -0.167 | -0.277 |
| 22 | 2.411 | 2.417 | 2.425 | 2.425 | 2.423 | 2.433 | 2.435 | 2.437 | 2.439 | 2.439 | 2.441 | 2.441 | 2.445 | 2.437 | 2.427 |
| 23 | 2.489 | 2.491 | 2.501 | 2.499 | 2.499 | 2.507 | 2.509 | 2.509 | 2.511 | 2.513 | 2.513 | 2.517 | 2.521 | 2.497 | 2.495 |
| 24 | -0.735 | -0.717 | -0.699 | -0.699 | -0.684 | -0.666 | -0.653 | -0.647 | -0.639 | -0.629 | -0.623 | -0.612 | -0.604 | -0.727 | -0.616 |
| 27 | -0.713 | -0.697 | -0.683 | -0.683 | -0.670 | -0.656 | -0.648 | -0.642 | -0.635 | -0.629 | -0.623 | -0.615 | -0.607 | -0.707 | -0.619 |
| 29 | 2.361 | 2.373 | 2.381 | 2.383 | 2.387 | 2.395 | 2.402 | 2.406 | 2.408 | 2.412 | 2.416 | 2.420 | 2.424 | 2.369 | 2.418 |
| 30 | 3.819 | 3.831 | 3.835 | 3.835 | 3.837 | 3.843 | 3.847 | 3.851 | 3.853 | 3.855 | 3.858 | 3.862 | 3.864 | 3.823 | 3.845 |
| 31 | 3.832 | 3.844 | 3.850 | 3.848 | 3.850 | 3.856 | 3.860 | 3.862 | 3.866 | 3.868 | 3.871 | 3.875 | 3.877 | 3.838 | 3.862 |

SUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978.

MITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 15

| STELLE | BELASTUNGSGRAD M/MU | | | | | | | | | | | | | | |
|--------|---------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|
| | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.686 | 0.571 | 0.400 | 0.400 | 0.400 | 0.100 | 0.000 | 0.429 | 0.857 | 0.857 |
| | 2 | 3 | 4 | 5 | 6 | 1 | 1 | 1 | 2 | 3 | | 3 | | 7 | 8 |
| 1 | -0.017 | -0.017 | -0.039 | -0.039 | -0.039 | -0.041 | -0.037 | -0.035 | -0.023 | -0.021 | -0.002 | -0.004 | -0.124 | -0.122 | -0.19 |
| 2 | -0.004 | -0.004 | -0.024 | -0.020 | -0.020 | -0.022 | -0.020 | -0.018 | -0.008 | -0.004 | 0.011 | 0.007 | -0.106 | -0.100 | -0.17 |
| 3 | 0.123 | 0.127 | 0.297 | 0.303 | 0.303 | 0.307 | 0.307 | 0.305 | 0.320 | 0.334 | 0.295 | 0.361 | 0.221 | 0.225 | 0.25 |
| 4 | -0.049 | -0.051 | -0.076 | -0.078 | -0.080 | -0.082 | -0.080 | -0.078 | -0.068 | -0.064 | -0.045 | -0.041 | -0.158 | -0.150 | -0.22 |
| 7 | -0.054 | -0.050 | -0.050 | -0.023 | 0.044 | 0.055 | 0.055 | 0.050 | 0.061 | 0.071 | 0.077 | 0.040 | -0.068 | -0.041 | -0.09 |
| 8 | 0.021 | 0.023 | 0.027 | 0.031 | 0.033 | 0.037 | 0.039 | 0.041 | 0.045 | 0.045 | 0.051 | 0.037 | 0.031 | 0.025 | 0.03 |
| 9 | 0.028 | 0.014 | 0.030 | 0.028 | 0.016 | 0.016 | 0.024 | 0.018 | 0.028 | 0.032 | 0.051 | 0.030 | 0.032 | -0.009 | 0.00 |
| 11 | 0.067 | 0.069 | 0.059 | 0.057 | 0.044 | 0.032 | 0.032 | 0.013 | 0.042 | 0.048 | 0.063 | 0.028 | 0.057 | 0.067 | 0.06 |
| 12 | 0.120 | 0.118 | 0.188 | 0.213 | 0.225 | 0.200 | 0.213 | 0.186 | 0.184 | 0.196 | 0.178 | 0.077 | 0.129 | 0.157 | 0.20 |
| 13 | -0.011 | -0.019 | 0.004 | 0.014 | 0.008 | 0.014 | -0.004 | -0.013 | -0.002 | 0.000 | 0.012 | -0.025 | -0.011 | -0.029 | -0.01 |
| 14 | -0.025 | -0.011 | 0.012 | 0.039 | 0.063 | 0.067 | 0.051 | 0.039 | 0.065 | 0.067 | 0.080 | 0.020 | 0.028 | 0.024 | 0.03 |
| 15 | 0.006 | -0.000 | -0.025 | -0.021 | -0.025 | -0.019 | 0.012 | 0.014 | 0.022 | 0.024 | 0.051 | 0.057 | 0.041 | -0.012 | 0.00 |
| 16 | -0.263 | -0.263 | -0.265 | -0.273 | -0.269 | -0.269 | -0.234 | -0.207 | -0.203 | -0.203 | -0.156 | -0.150 | -0.205 | -0.250 | -0.24 |
| 19 | -0.277 | -0.277 | -0.269 | -0.263 | -0.246 | -0.228 | -0.211 | -0.191 | -0.179 | -0.173 | -0.136 | -0.154 | -0.211 | -0.246 | -0.24 |
| 22 | 2.429 | 2.429 | 2.433 | 2.433 | 2.433 | 2.433 | 2.437 | 2.443 | 2.450 | 2.450 | 2.458 | 2.431 | 2.423 | 2.421 | 2.43 |
| 23 | 2.497 | 2.501 | 2.507 | 2.507 | 2.509 | 2.507 | 2.509 | 2.511 | 2.515 | 2.517 | 2.517 | 2.475 | 2.475 | 2.481 | 2.49 |
| 24 | -0.618 | -0.618 | -0.623 | -0.625 | -0.627 | -0.645 | -0.657 | -0.678 | -0.676 | -0.676 | -0.713 | -0.741 | -0.688 | -0.637 | -0.63 |
| 27 | -0.617 | -0.615 | -0.609 | -0.603 | -0.596 | -0.611 | -0.621 | -0.640 | -0.638 | -0.640 | -0.672 | -0.715 | -0.658 | -0.609 | -0.60 |
| 29 | 2.418 | 2.418 | 2.420 | 2.426 | 2.428 | 2.420 | 2.416 | 2.404 | 2.404 | 2.402 | 2.383 | 2.363 | 2.379 | 2.410 | 2.41 |
| 30 | 3.845 | 3.843 | 3.843 | 3.845 | 3.845 | 3.839 | 3.837 | 3.833 | 3.839 | 3.839 | 3.833 | 3.803 | 3.813 | 3.823 | 3.82 |
| 31 | 3.864 | 3.800 | 3.871 | 3.873 | 3.875 | 3.871 | 3.864 | 3.858 | 3.864 | 3.864 | 3.854 | 3.820 | 3.834 | 3.848 | 3.85 |

VERSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

ERMITTELTE STAHLDEHNUNGEN IN PROMILLE IM SCHNITT 15

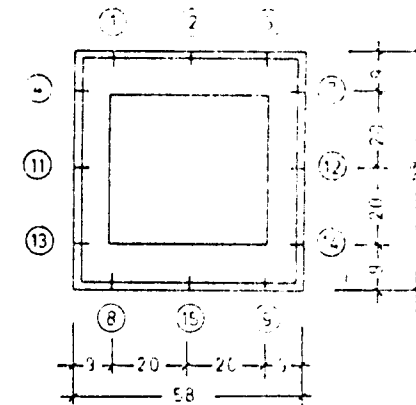
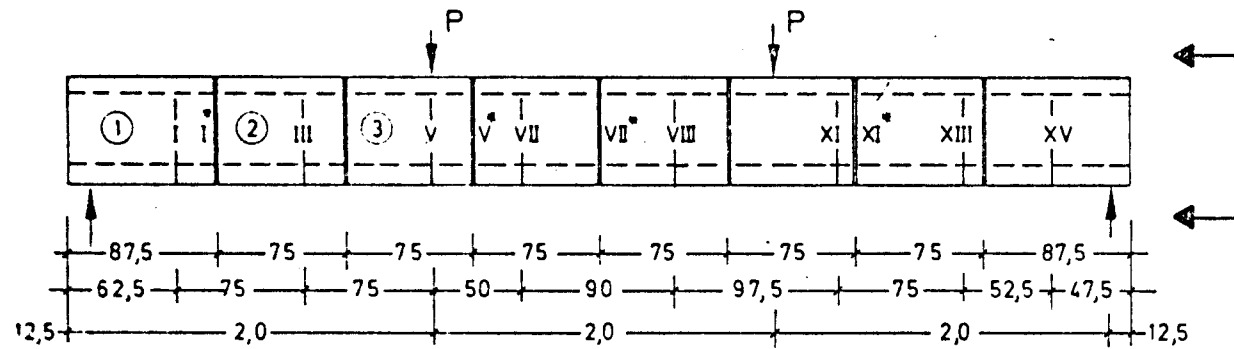
BELASTUNGSGRAD M/MU

| MESSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.943 | 1.000 |
|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | | |
| 1 | -0.191 | -0.202 | -0.206 | -0.230 | -0.234 | -0.245 | -0.220 | -0.210 | -0.237 | -0.214 |
| 2 | -0.168 | -0.178 | -0.180 | -0.191 | 0.015 | 0.172 | 0.287 | 0.382 | 0.372 | -0.032 |
| 3 | 0.266 | 0.258 | 0.318 | 0.580 | 0.732 | 0.767 | 0.870 | 0.905 | 0.913 | 0.521 |
| 4 | -0.228 | -0.242 | -0.246 | -0.267 | -0.267 | -0.275 | -0.253 | -0.238 | -0.261 | -0.228 |
| 7 | -0.072 | -0.017 | 0.106 | 0.213 | 0.297 | 0.377 | 0.476 | 0.541 | 0.529 | 0.022 |
| 8 | 0.035 | 0.039 | 0.043 | 0.041 | 0.041 | 0.047 | 0.068 | 0.084 | 0.082 | 0.099 |
| 9 | 0.014 | -0.007 | 0.007 | 0.081 | 0.311 | 0.422 | 0.537 | 0.601 | 0.652 | 0.675 |
| 11 | 0.083 | 0.059 | 0.063 | 0.046 | 0.040 | 0.048 | 0.079 | 0.077 | 0.069 | 0.116 |
| 12 | 0.225 | 0.239 | 0.315 | 0.467 | 0.554 | 0.632 | 0.699 | 0.726 | 0.740 | 0.736 |
| 13 | 0.006 | -0.011 | 0.004 | 0.006 | 0.000 | 0.016 | 0.055 | 0.065 | 0.065 | 0.092 |
| 14 | 0.086 | 0.094 | 0.174 | 0.264 | 0.334 | 0.359 | 0.421 | 0.484 | 0.511 | 0.533 |
| 15 | 0.010 | -0.006 | 0.016 | 0.034 | 0.061 | 0.100 | 0.139 | 0.188 | 0.223 | 0.258 |
| 16 | -0.248 | -0.254 | -0.265 | -0.252 | -0.244 | -0.238 | -0.201 | -0.191 | -0.207 | -0.163 |
| 19 | -0.226 | -0.207 | -0.163 | 0.082 | 0.221 | 0.357 | 0.511 | 0.612 | 0.653 | 0.207 |
| 22 | 2.435 | 2.437 | 2.435 | 2.435 | 2.431 | 2.423 | 2.458 | 2.458 | 2.447 | 2.460 |
| 23 | 2.503 | 2.509 | 2.525 | 2.587 | 2.663 | 2.708 | 2.780 | 2.809 | 2.815 | 2.624 |
| 24 | -0.639 | -0.637 | -0.643 | -0.651 | -0.666 | -0.680 | -0.682 | -0.694 | -0.696 | -0.709 |
| 27 | -0.596 | -0.588 | -0.572 | -0.539 | -0.537 | -0.537 | -0.525 | -0.512 | -0.508 | -0.508 |
| 29 | 2.416 | 2.418 | 2.426 | 2.439 | 2.455 | 2.465 | 2.496 | 2.508 | 2.515 | 2.517 |
| 30 | 3.831 | 3.833 | 3.833 | 3.833 | 3.835 | 3.833 | 3.853 | 3.855 | 3.853 | 3.845 |
| 31 | 3.862 | 3.873 | 3.893 | 3.916 | 3.983 | 4.008 | 4.053 | 4.084 | 4.100 | 3.983 |

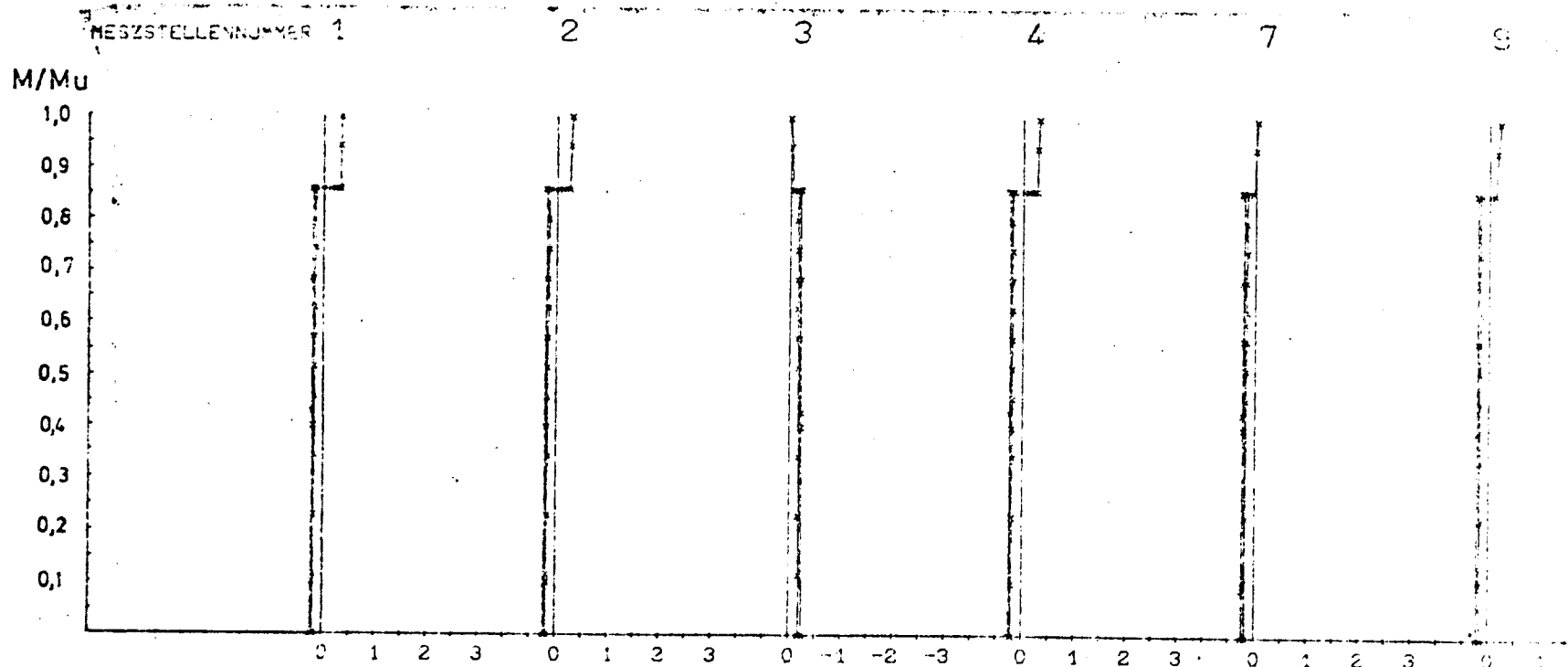
D Dehnungen der Bewehrung (graphische Form)

Bügeldehnungen des Balkens SETMQ 1

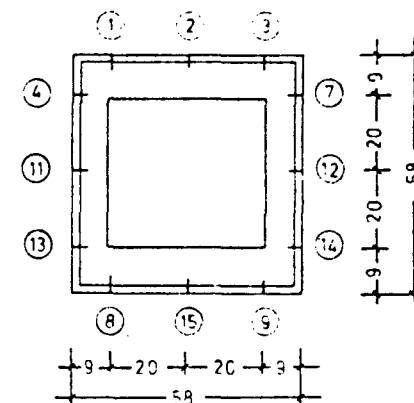
Schnitt I



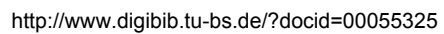
Meßquerschnitt
Meßstellen für
Bügel



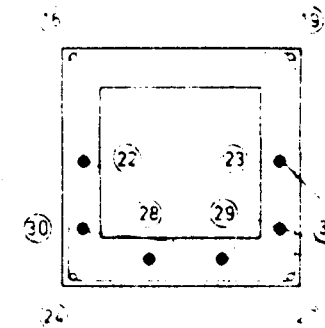
Schnitt I



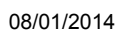
Meßquerschnitt
Meßstellen für
Bugel



Schnitt I

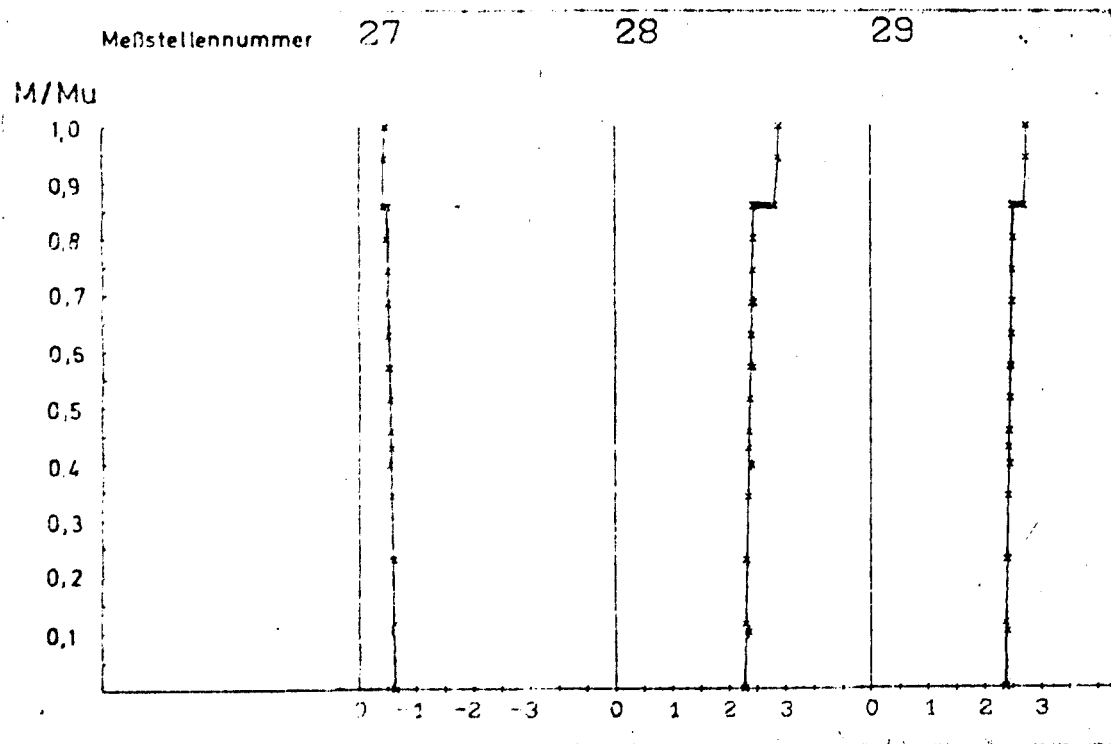
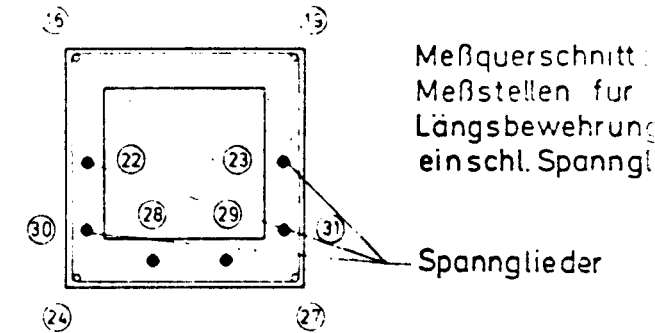
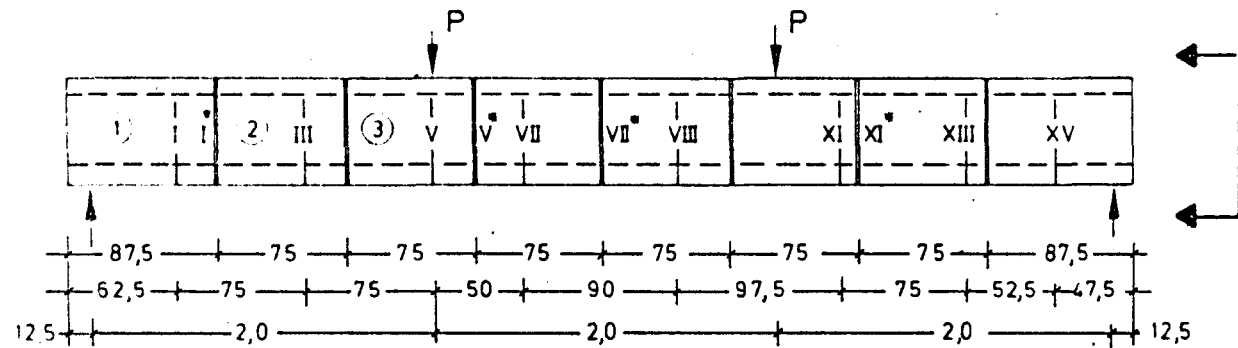


Spannglieder



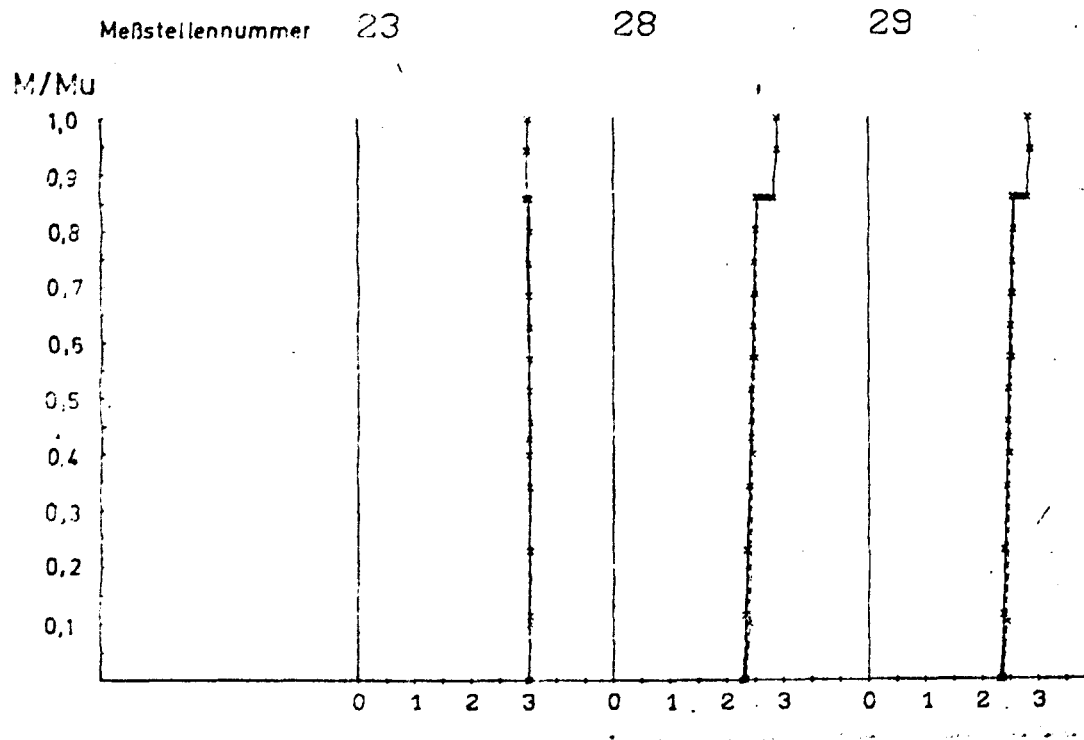
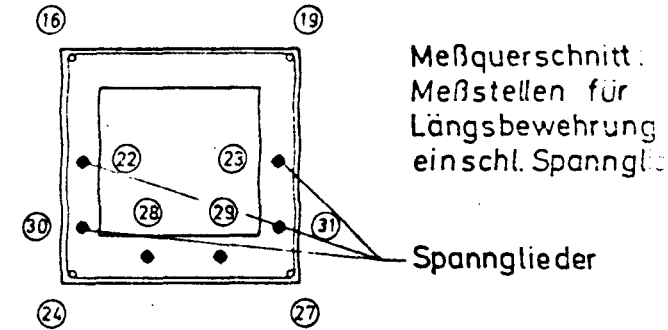
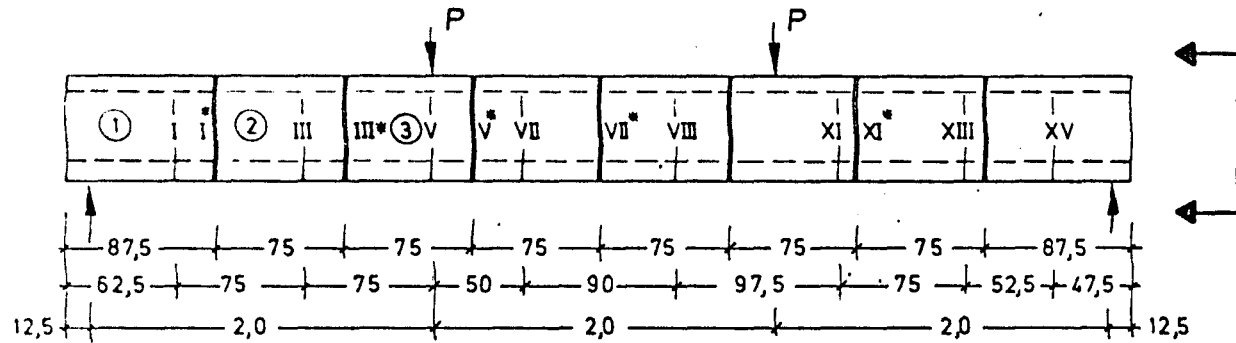
Längsstahldehnungen des Balkens SETMQ 1

Schnitt I



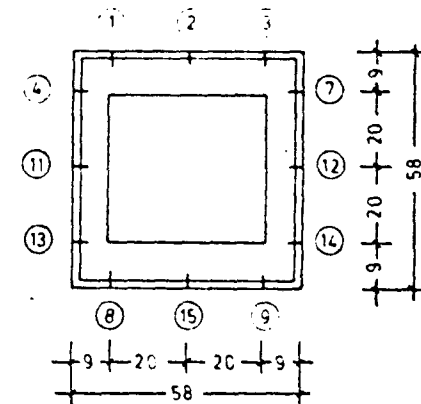
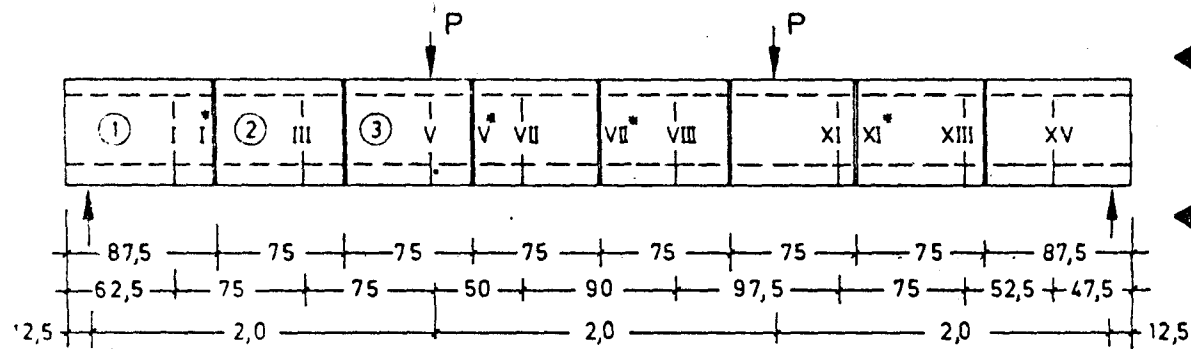
Längsstahldehnungen des Balkens SETMQ 1

Schnitt I *

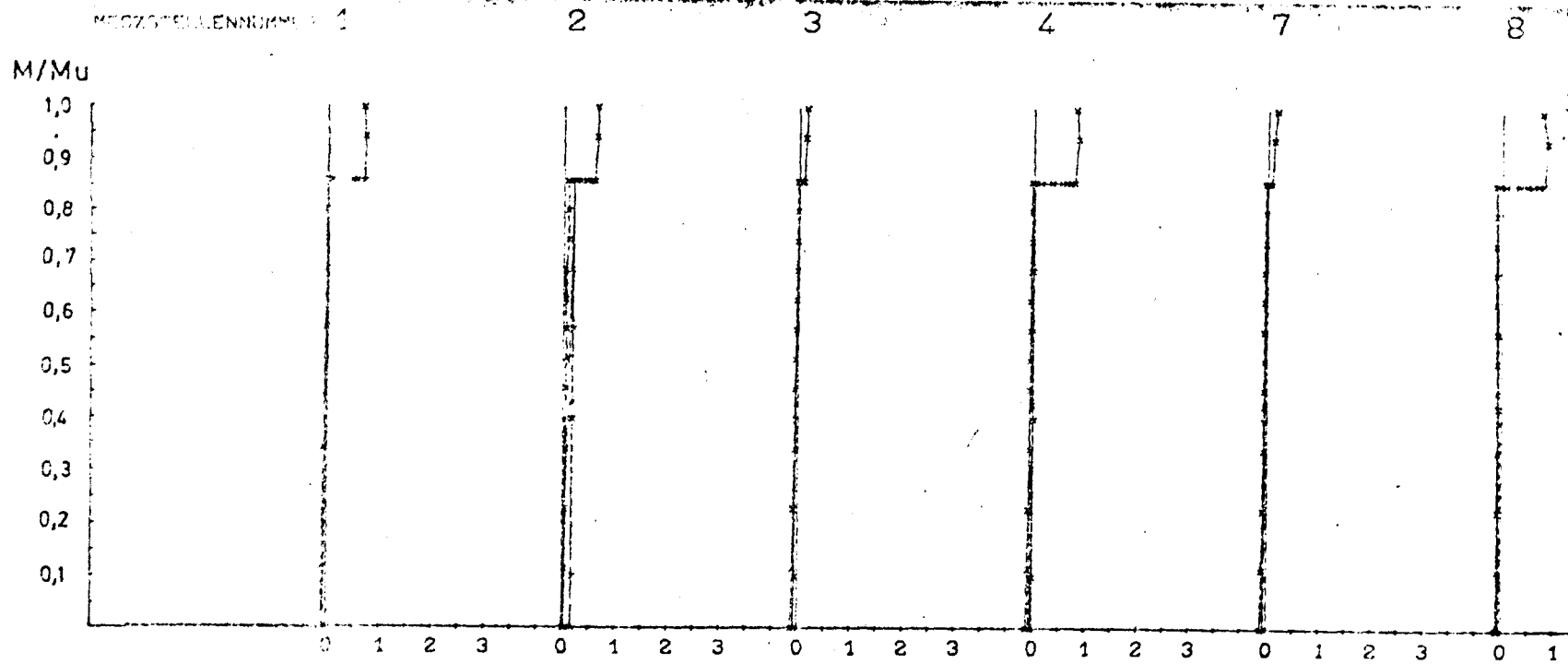


Bügeldehnungen des Balkens SETMQ 1

Schnitt III

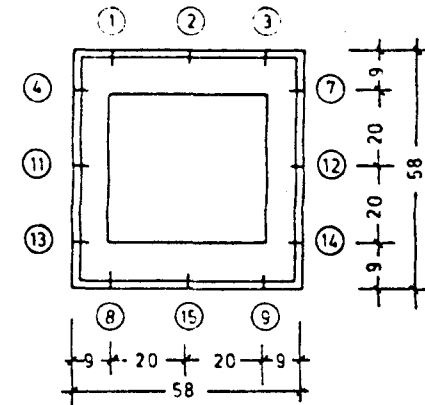
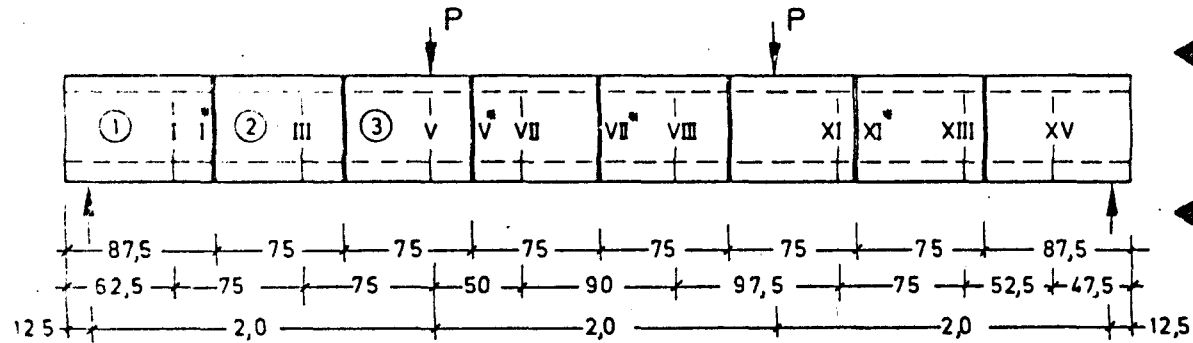


Meßquerschnitt
Meßstellen für
Bügel

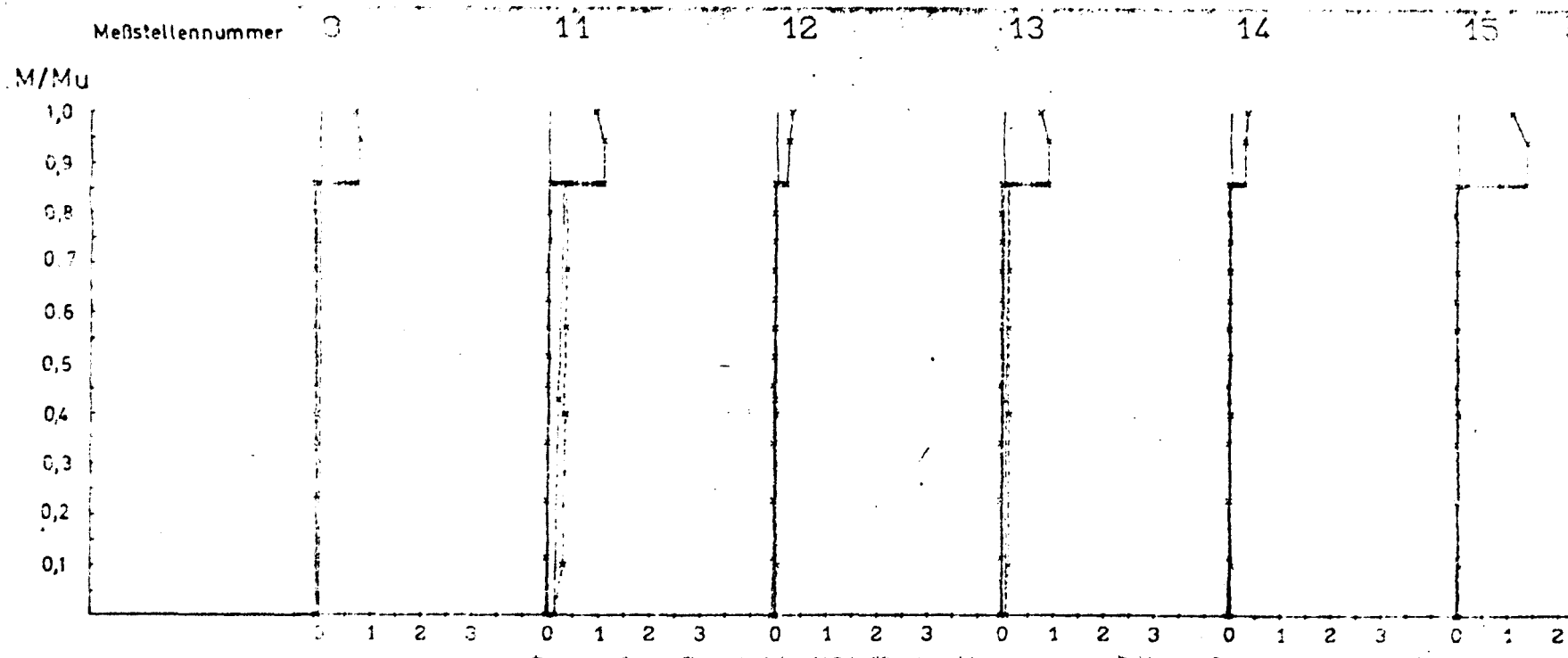


Bügeldehnungen des Balkens SETMQ 1

Schnitt III

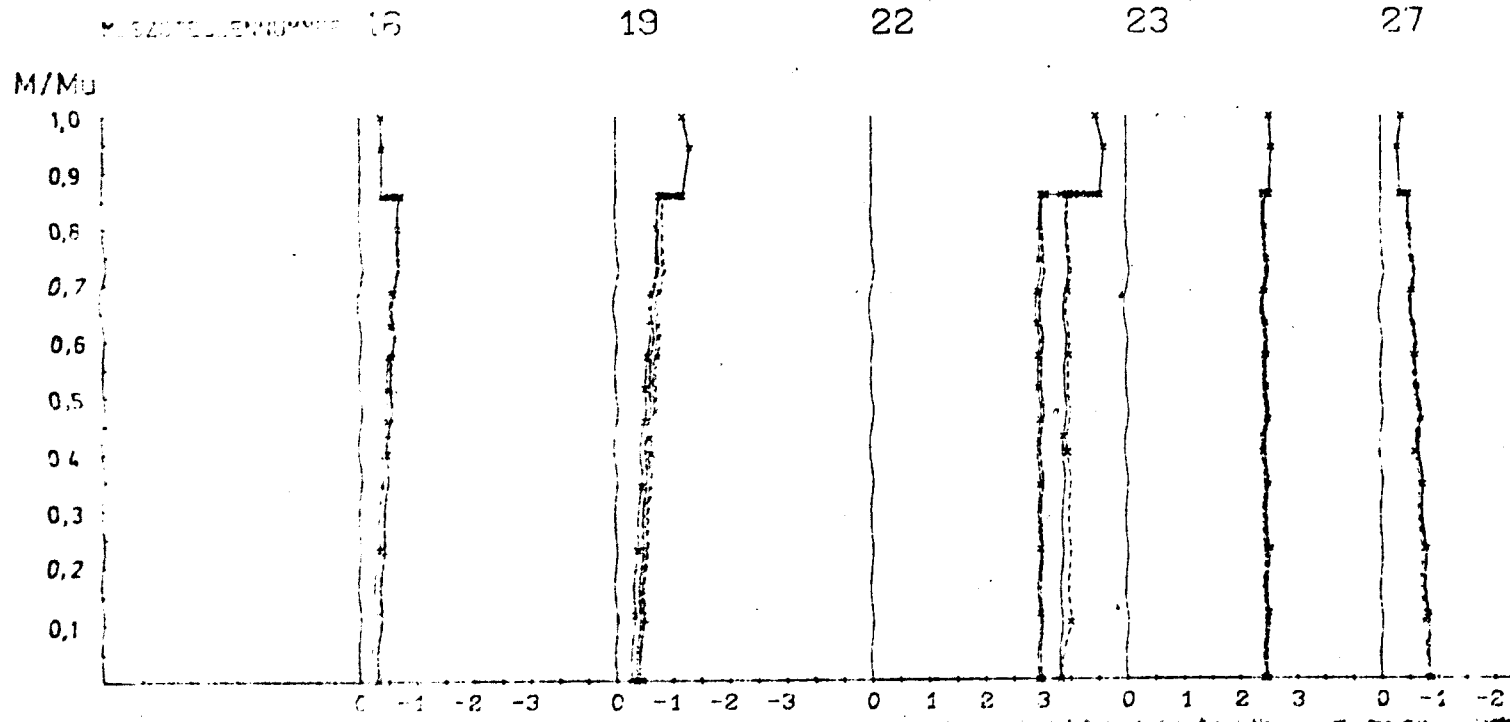
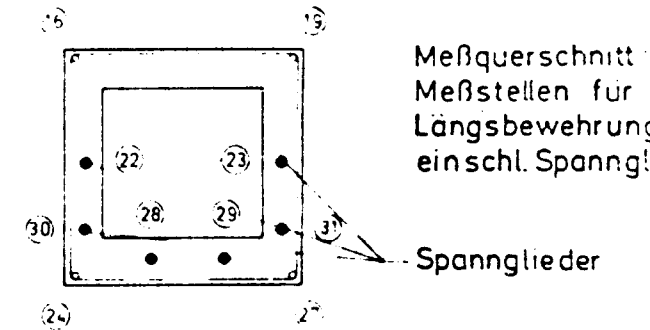
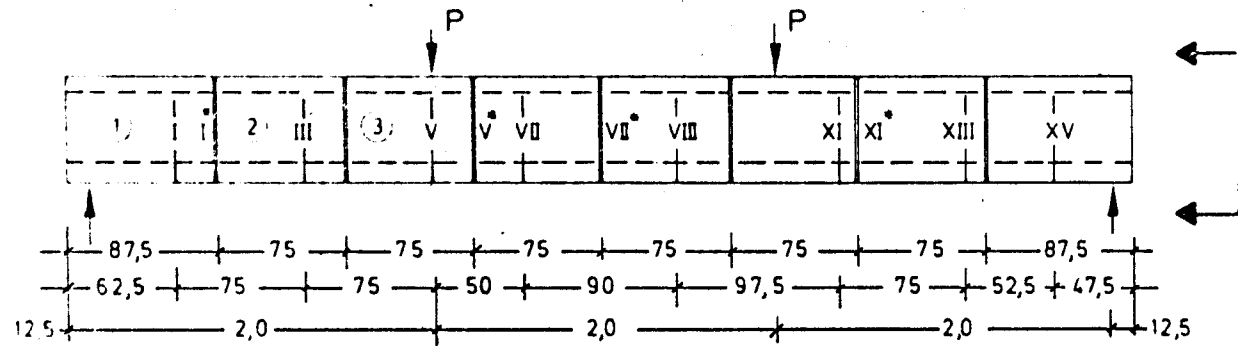


Meßquerschnitt
Meßstellen für
Bügel



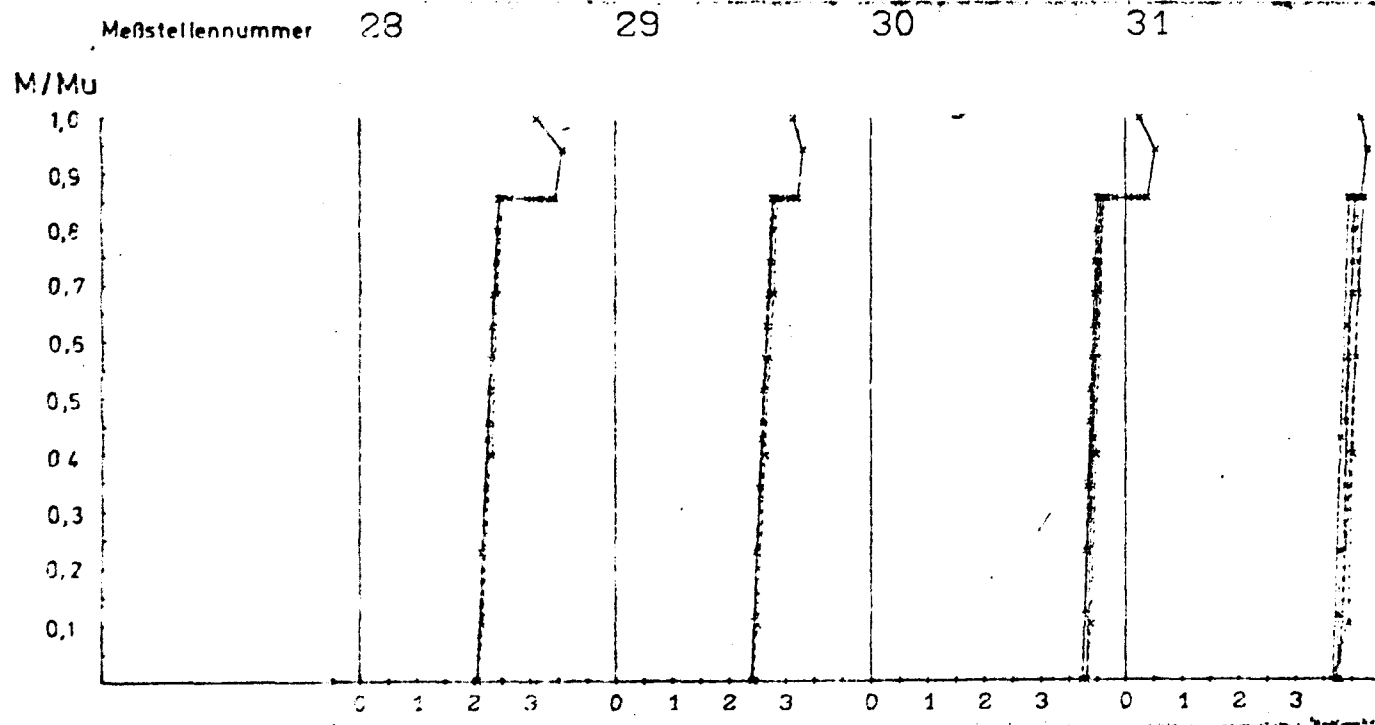
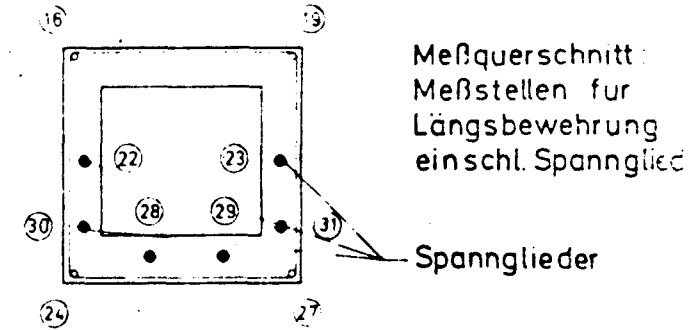
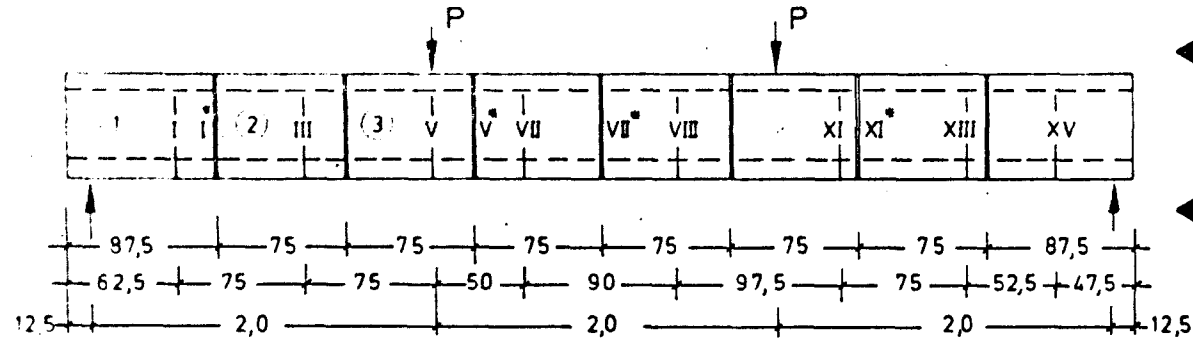
Längsstahldehnungen des Balkens SETMQ 1

Schnitt III



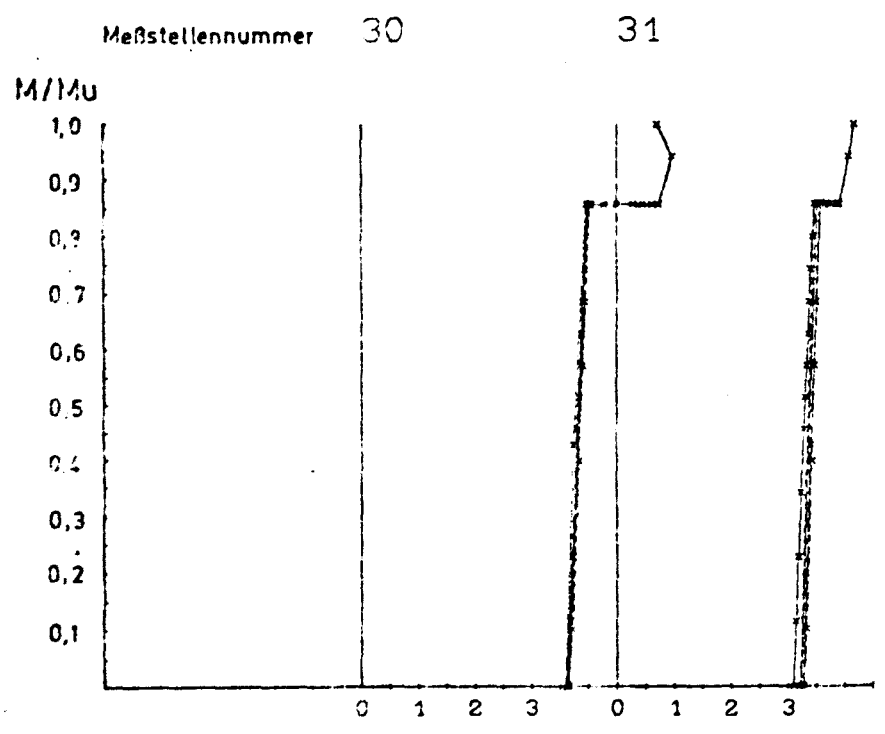
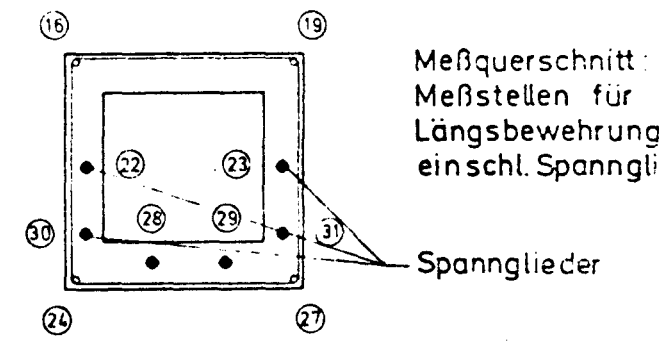
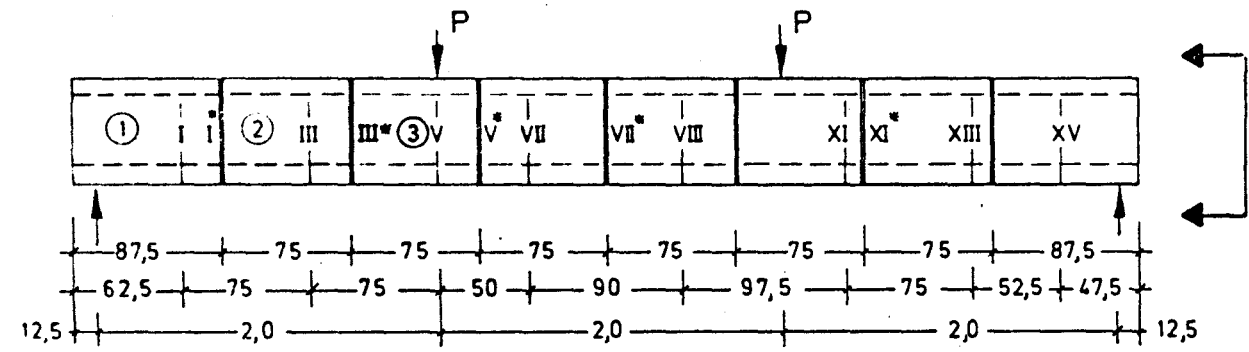
Längsstahldehnungen des Balkens SETMQ 1

Schnitt III



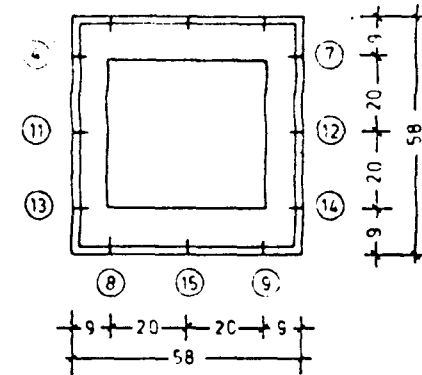
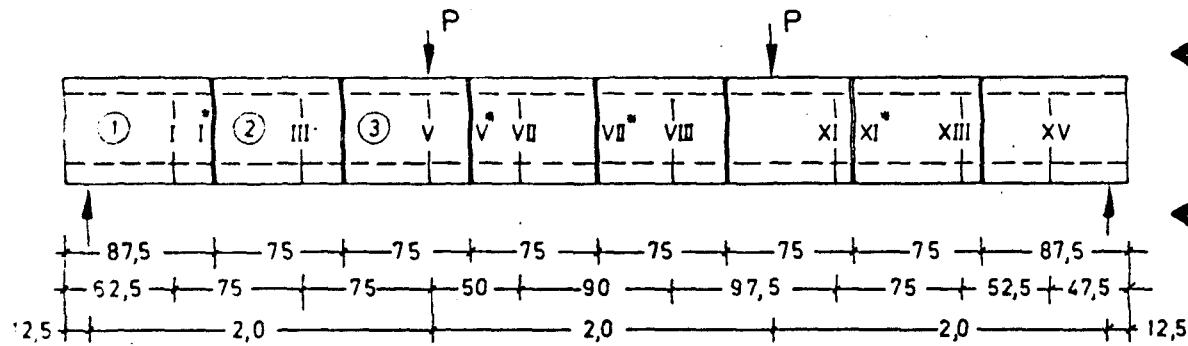
Längsstahldehnungen des Balkens SETMQ 1

Schnitt III *

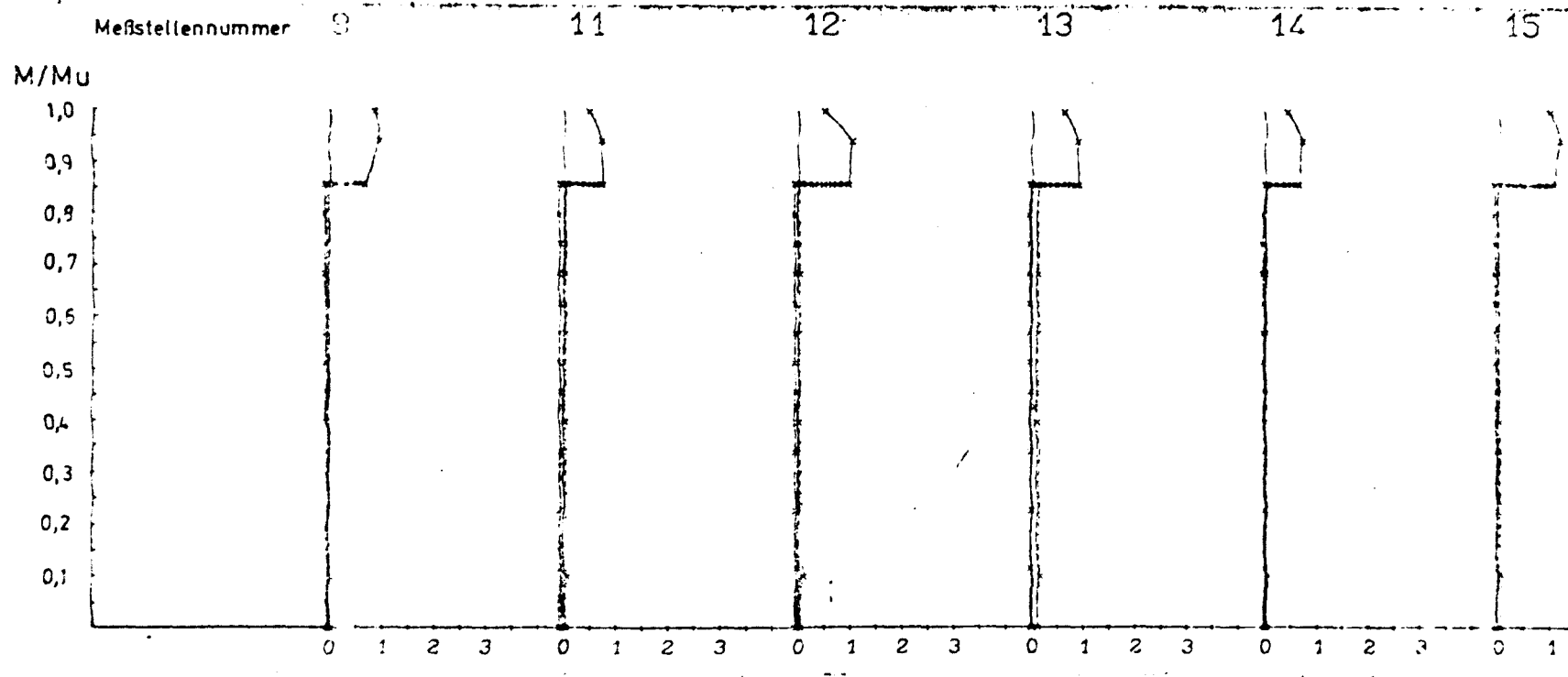


Bügeldehnungen des Balkens SETMQ 1

Schnitt V

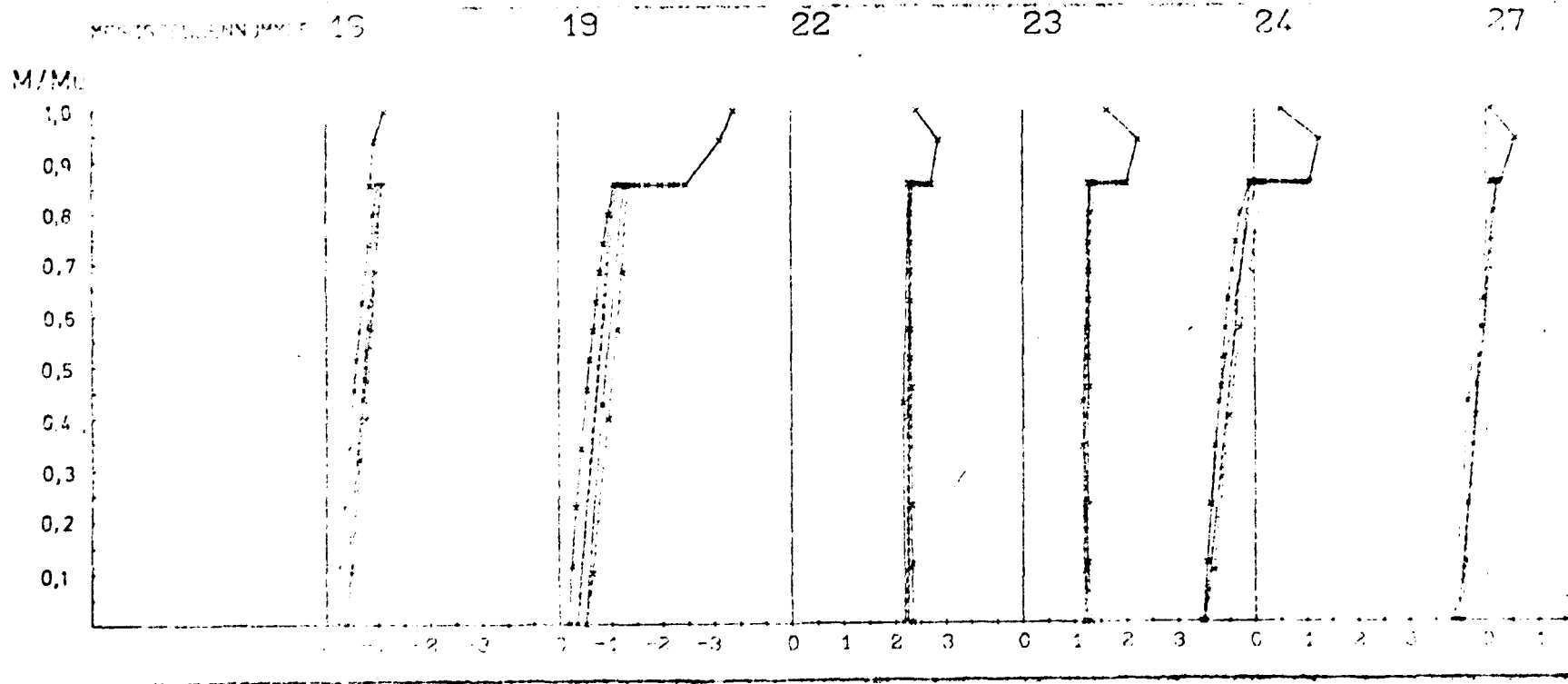
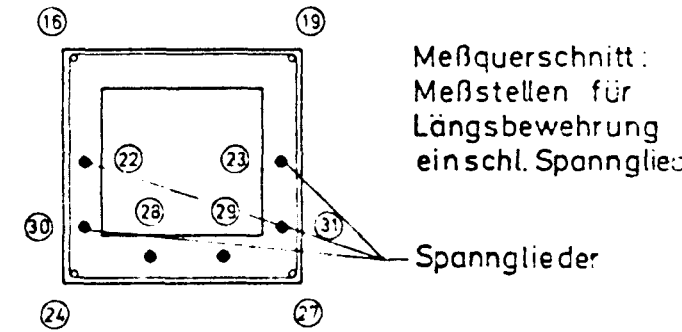
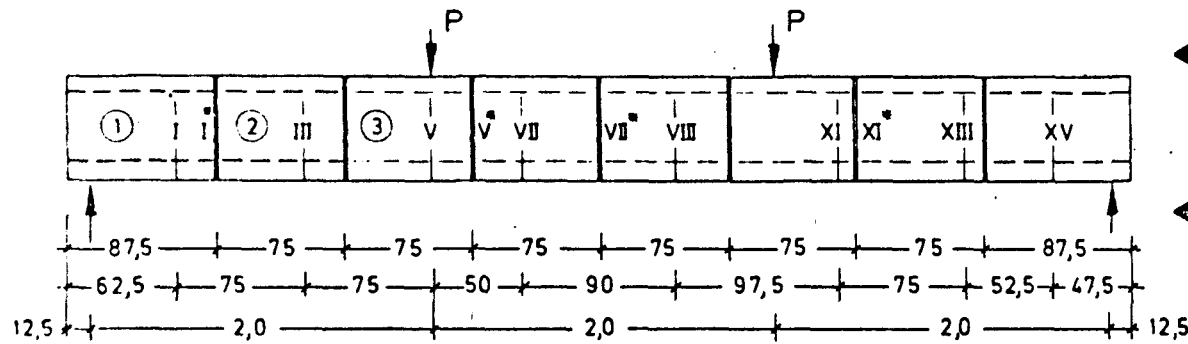


Meßquerschnitt
Meßstellen für
Bugel



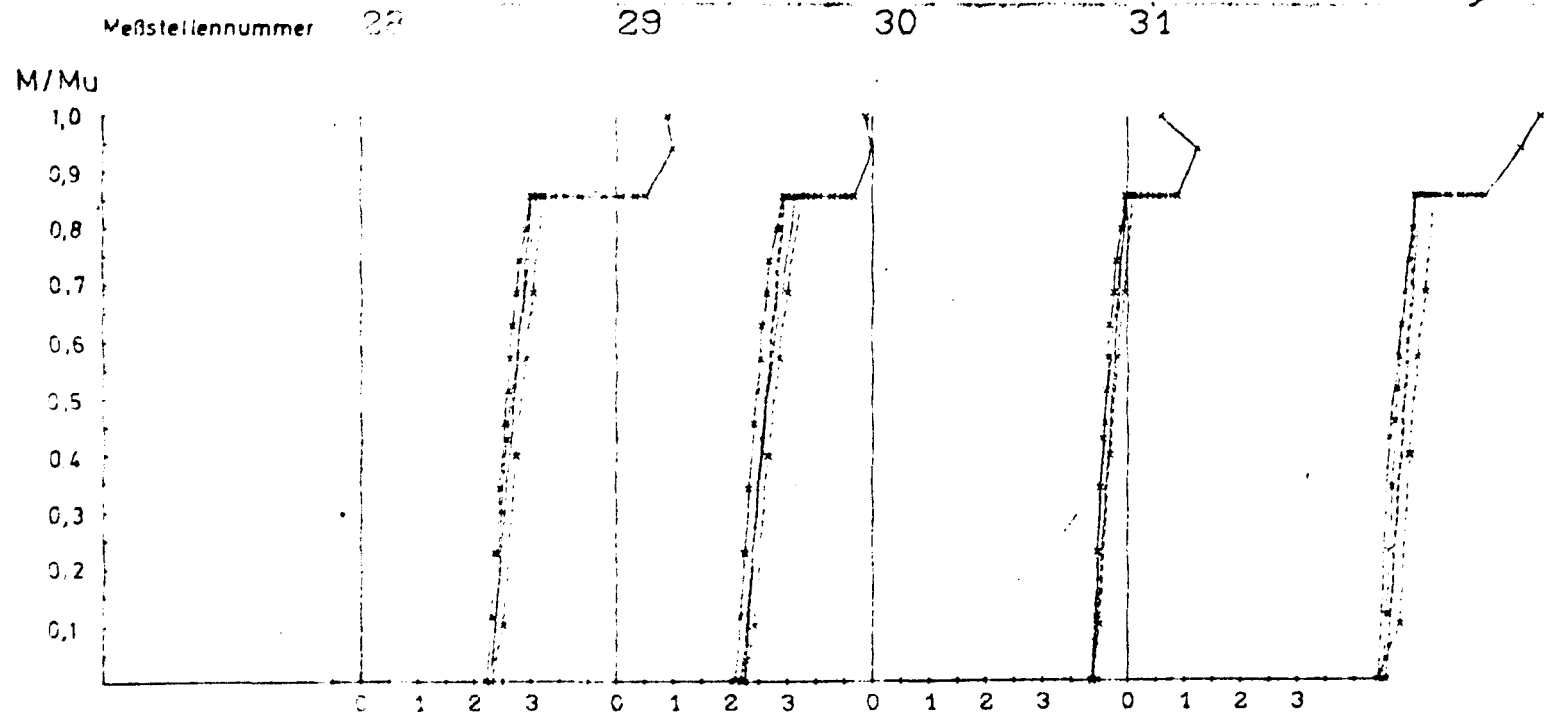
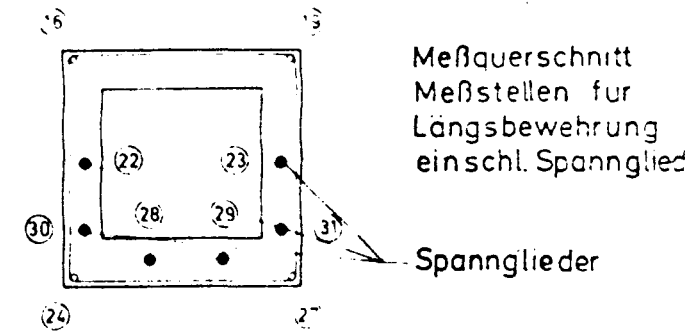
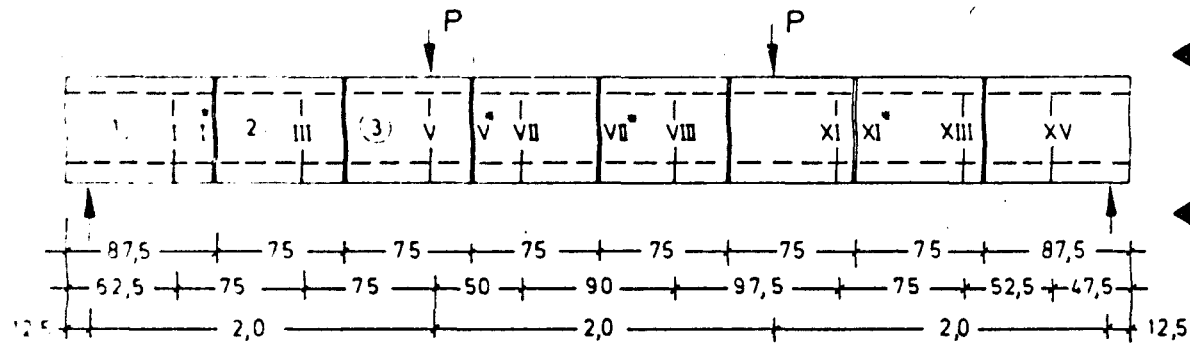
Längsstahldehnungen des Balkens SETMQ 1

Schnitt V



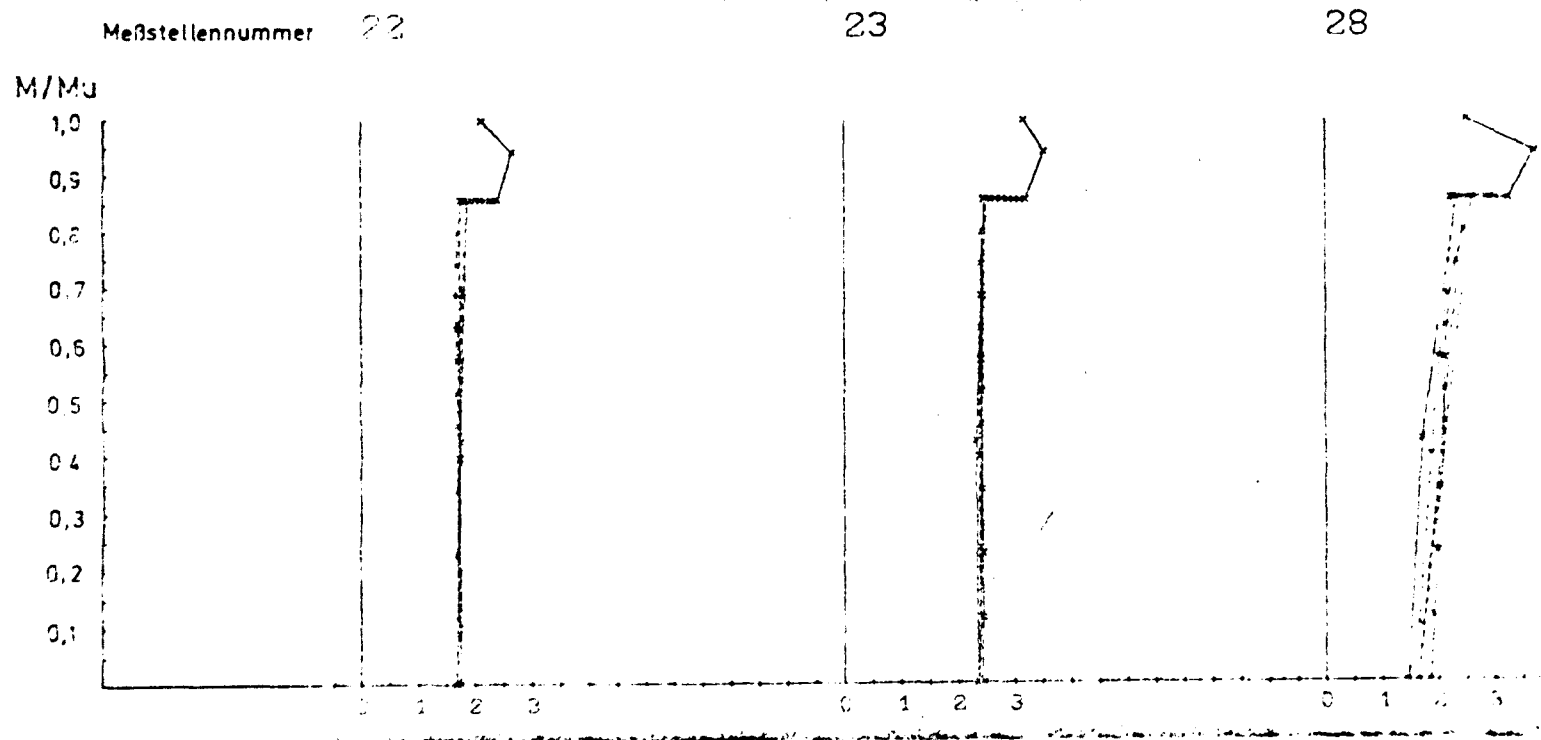
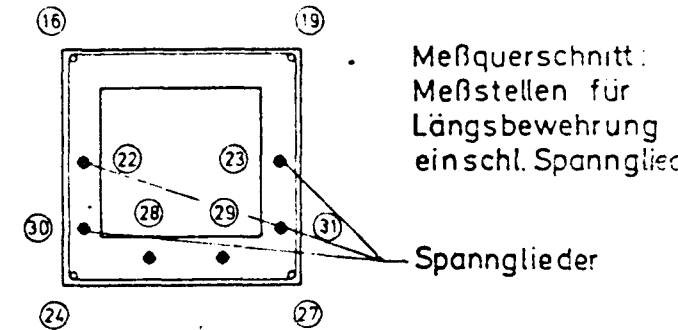
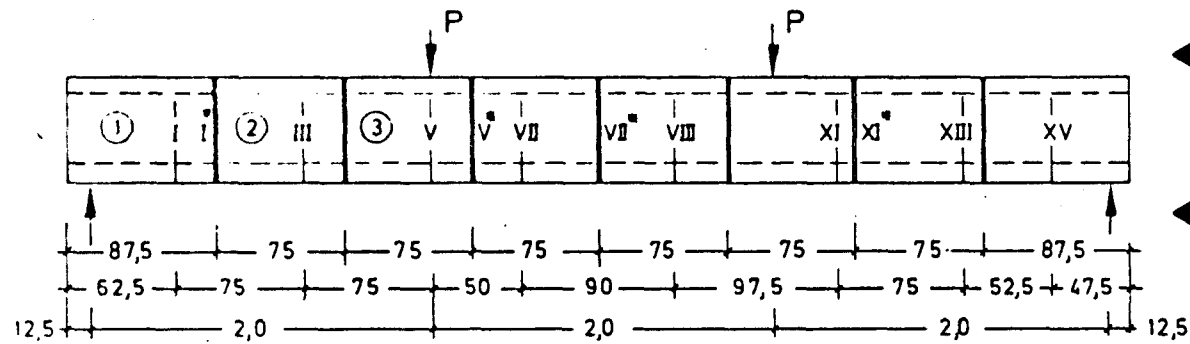
Längsstahldehnungen des Balkens SETMQ 1

Schnitt V



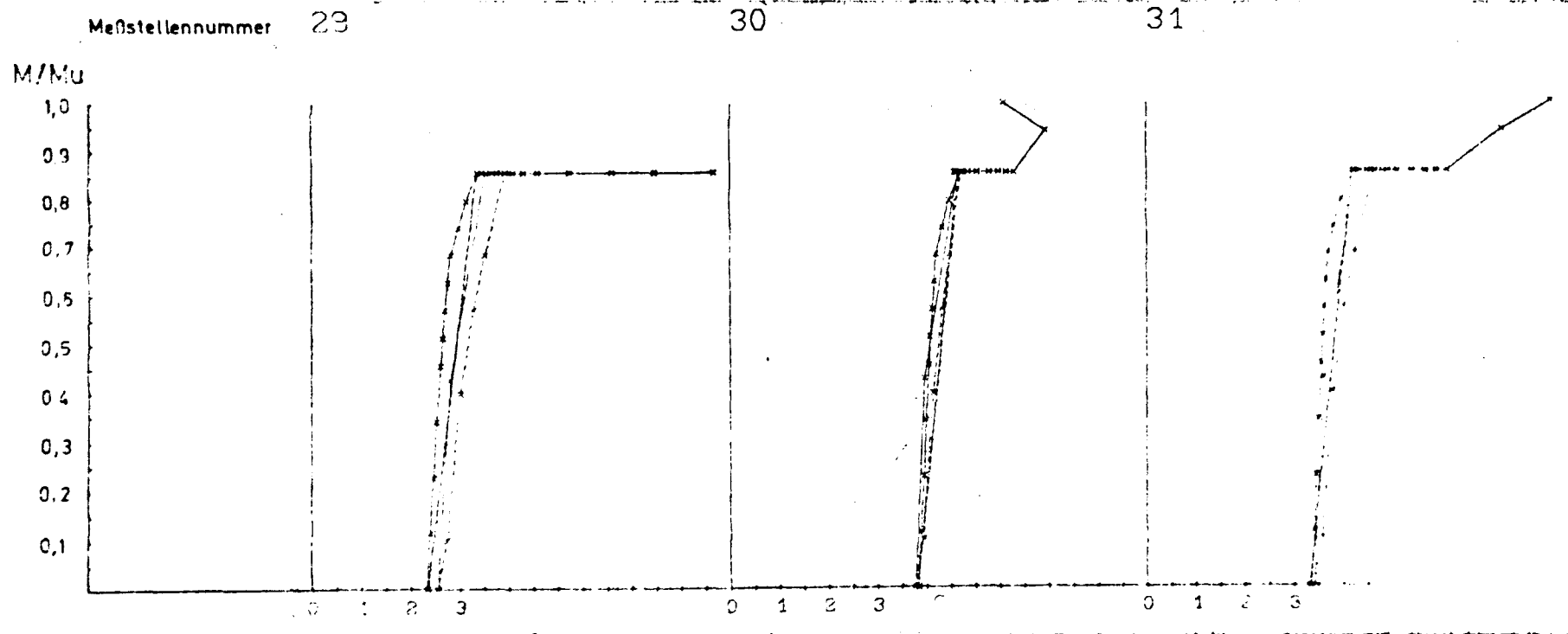
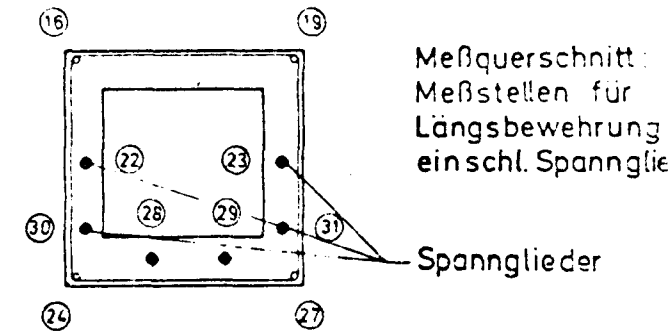
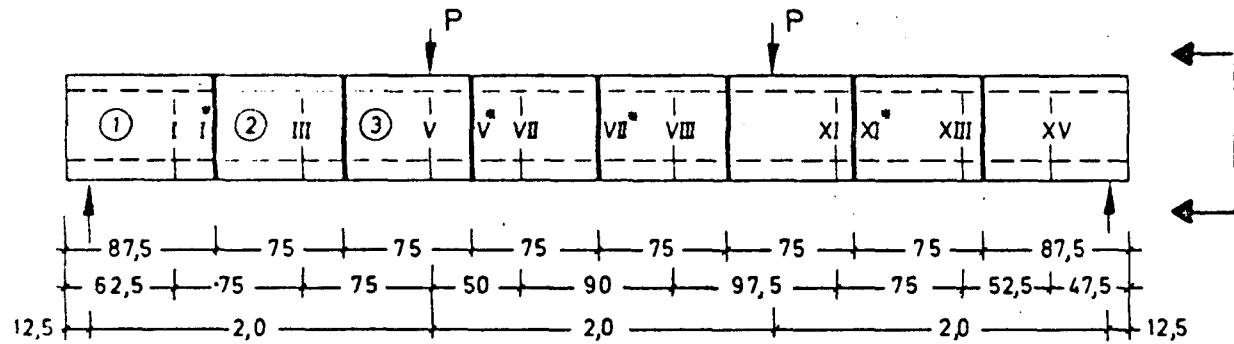
Längsstahldehnungen des Balkens SETMQ 1

Schnitt V*



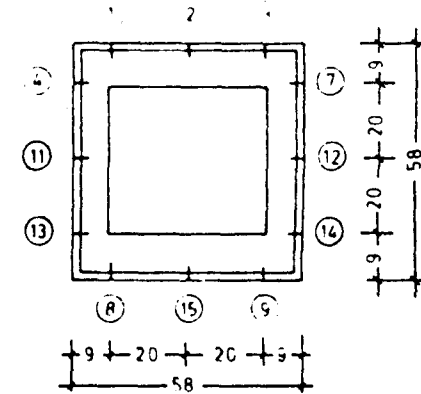
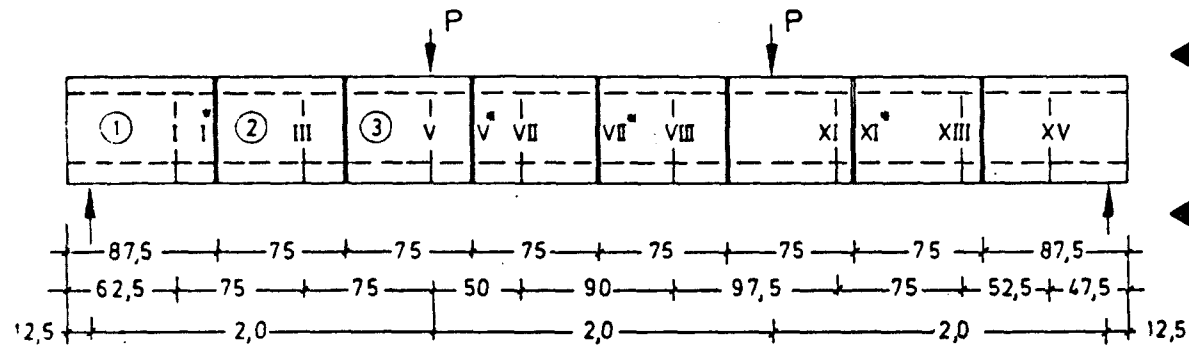
Längsstahldehnungen des Balkens SETMQ 1

Schnitt V*

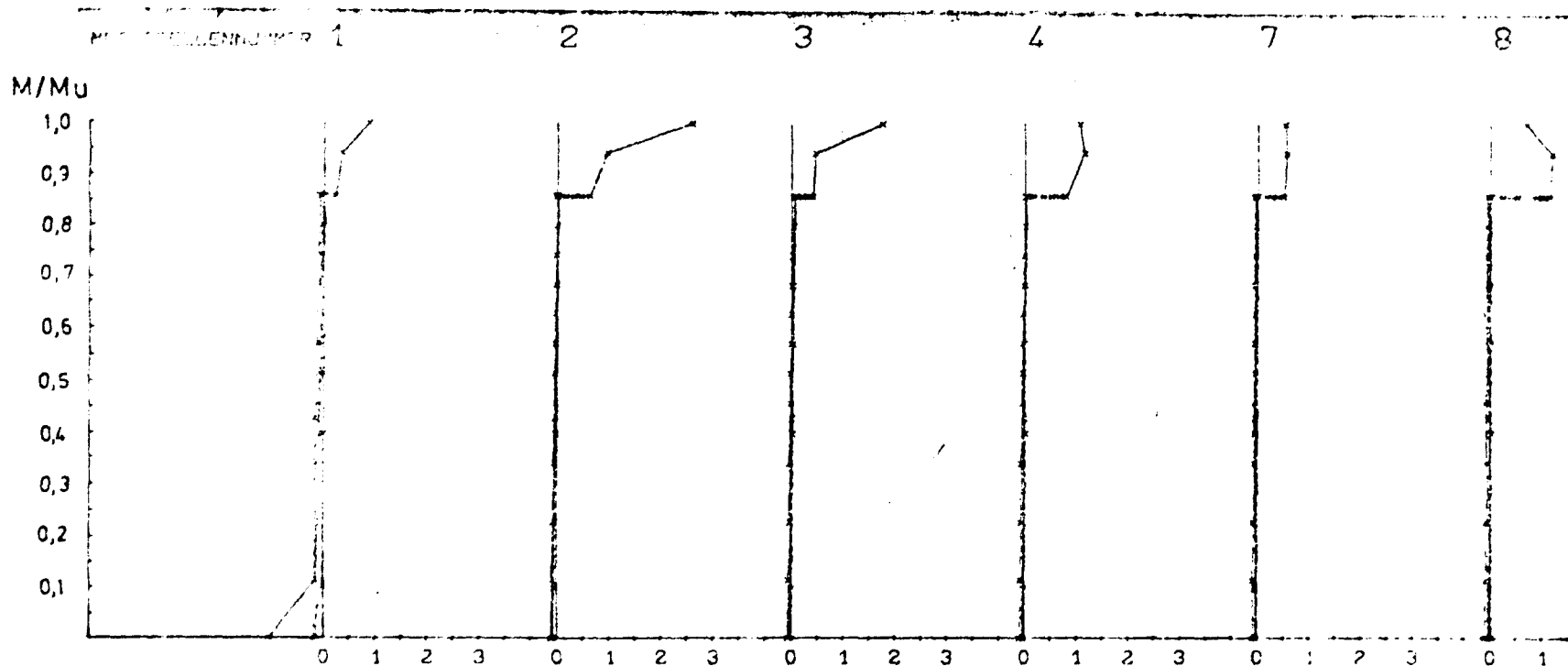


Bügeldehnungen des Balkens SETMQ 1

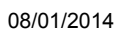
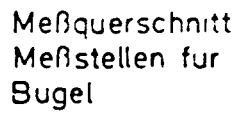
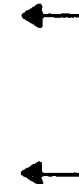
Schnitt VII



Meßquerschnitt
Meßstellen für
Bügel

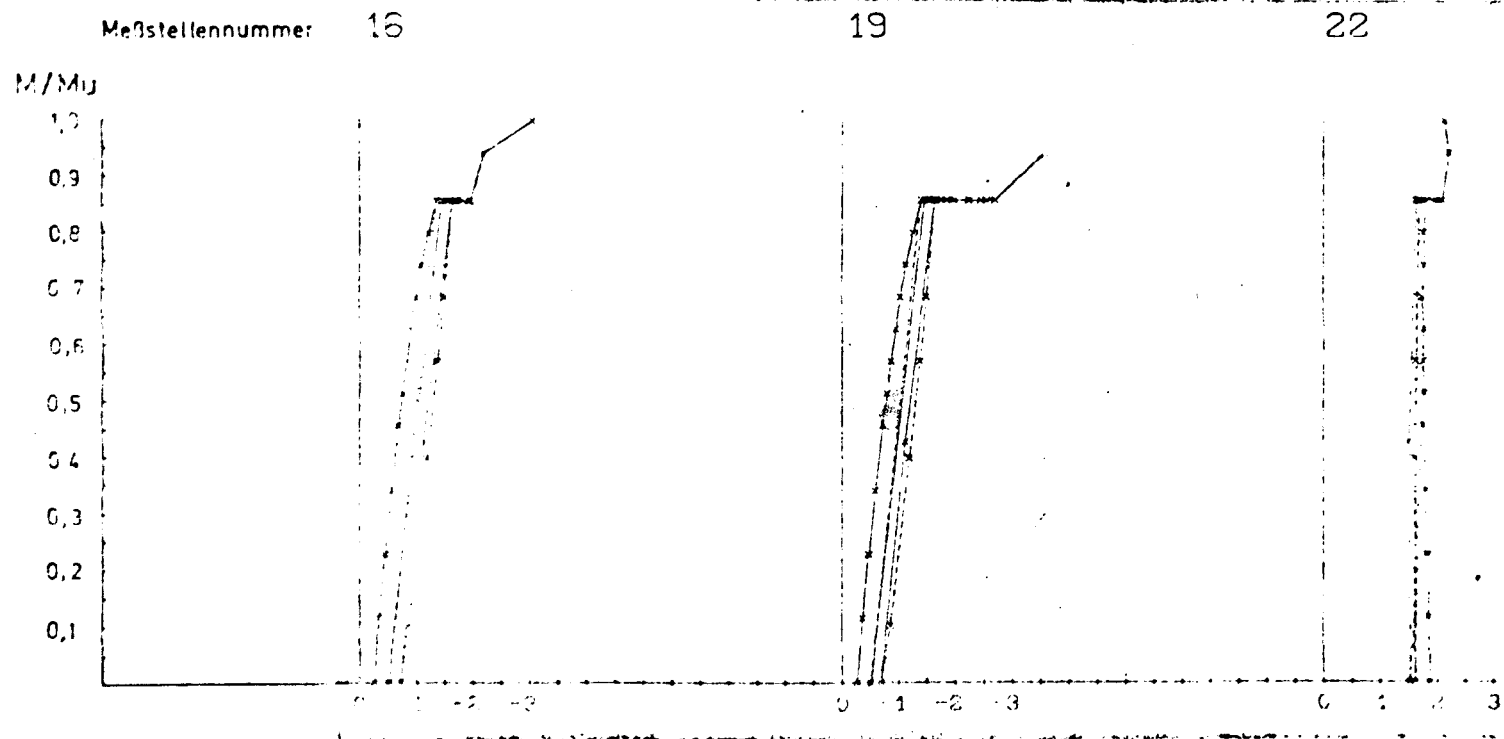
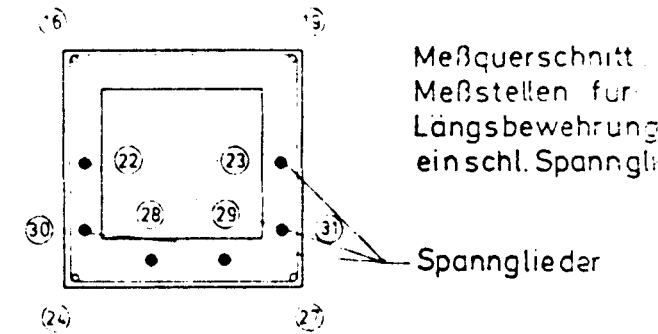
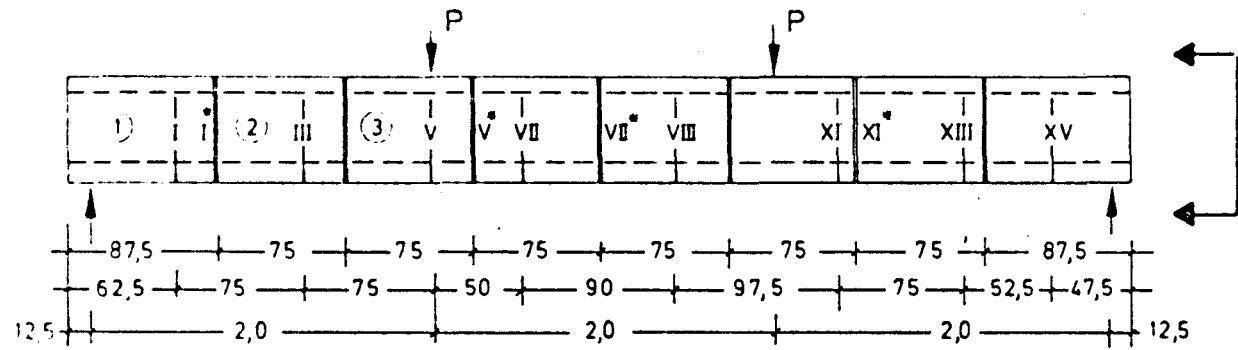


Schnitt VII



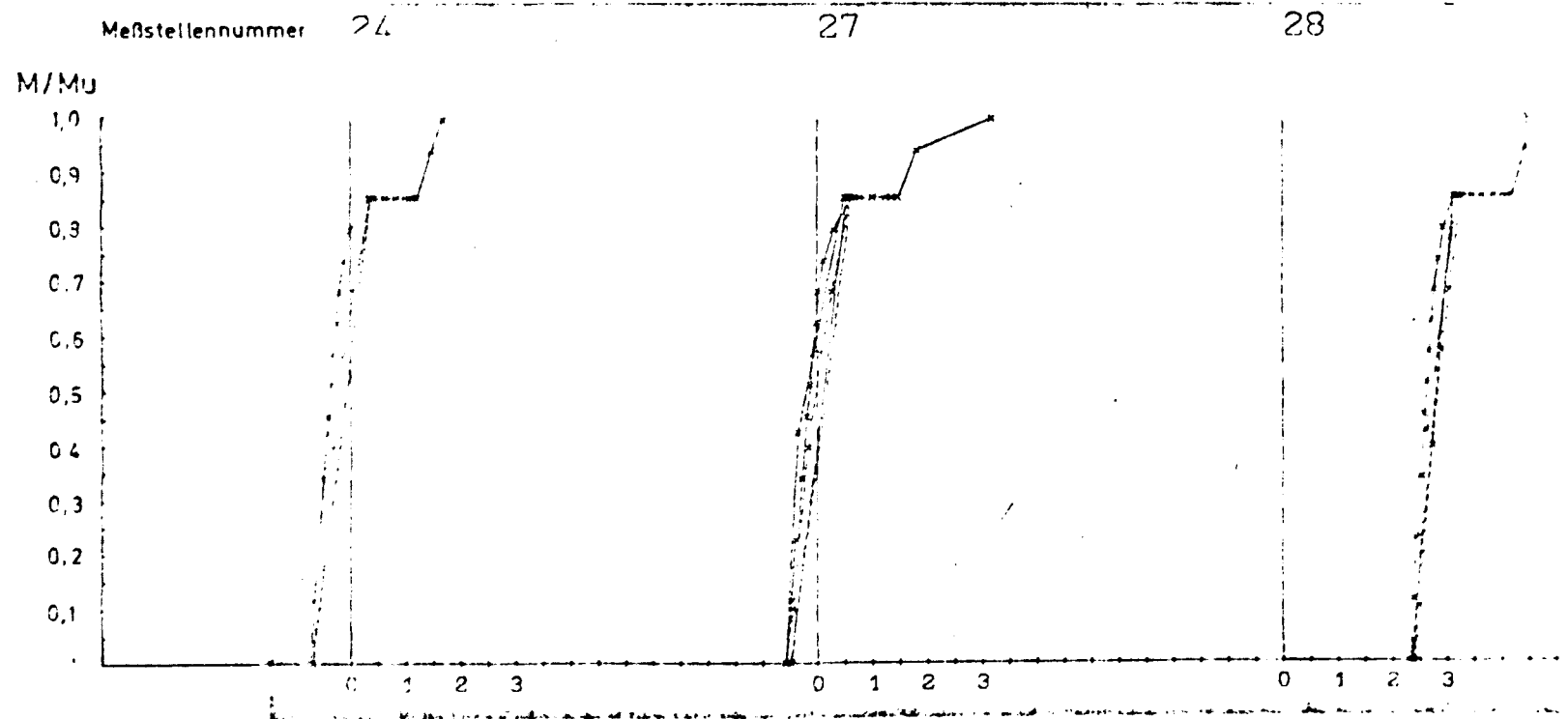
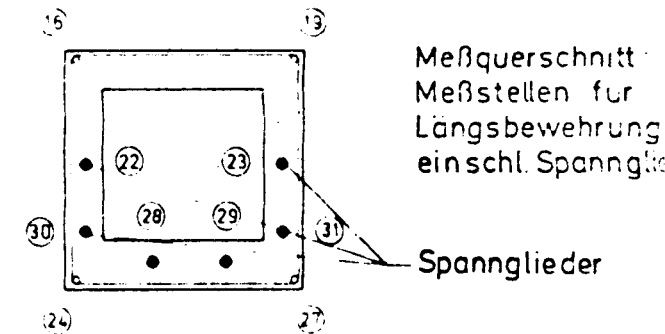
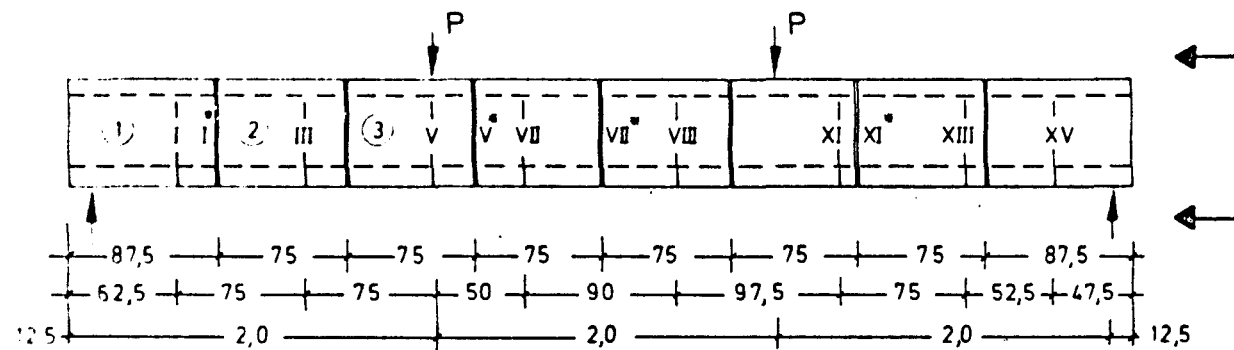
Längsstahldehnungen des Balkens SETMQ 1

Schnitt VII



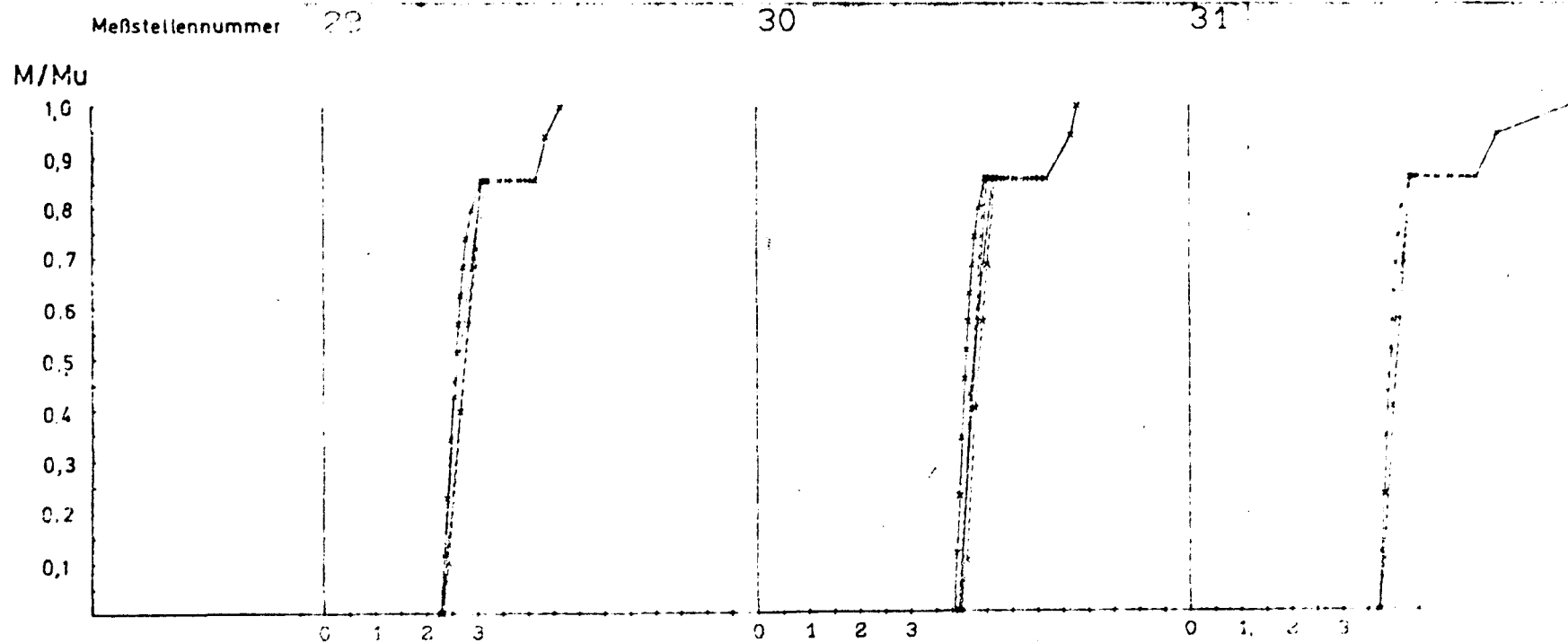
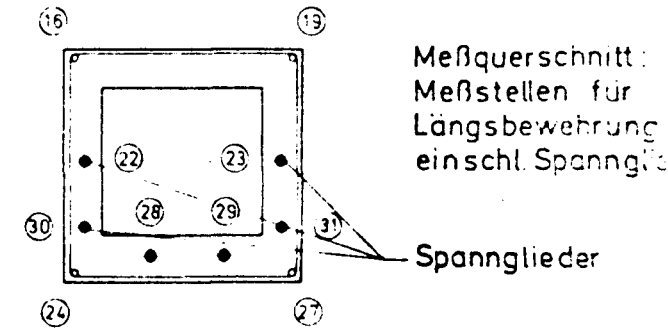
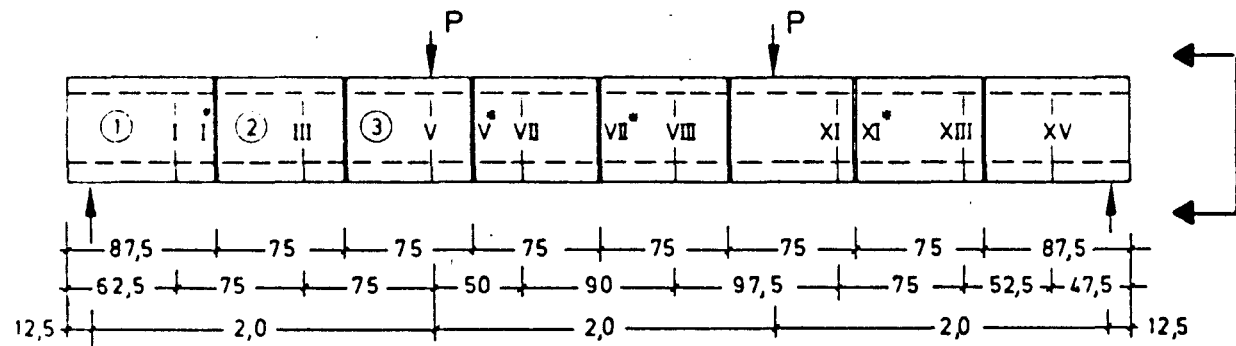
Längsstahldehnungen des Balkens SETMQ 1

Schnitt VII



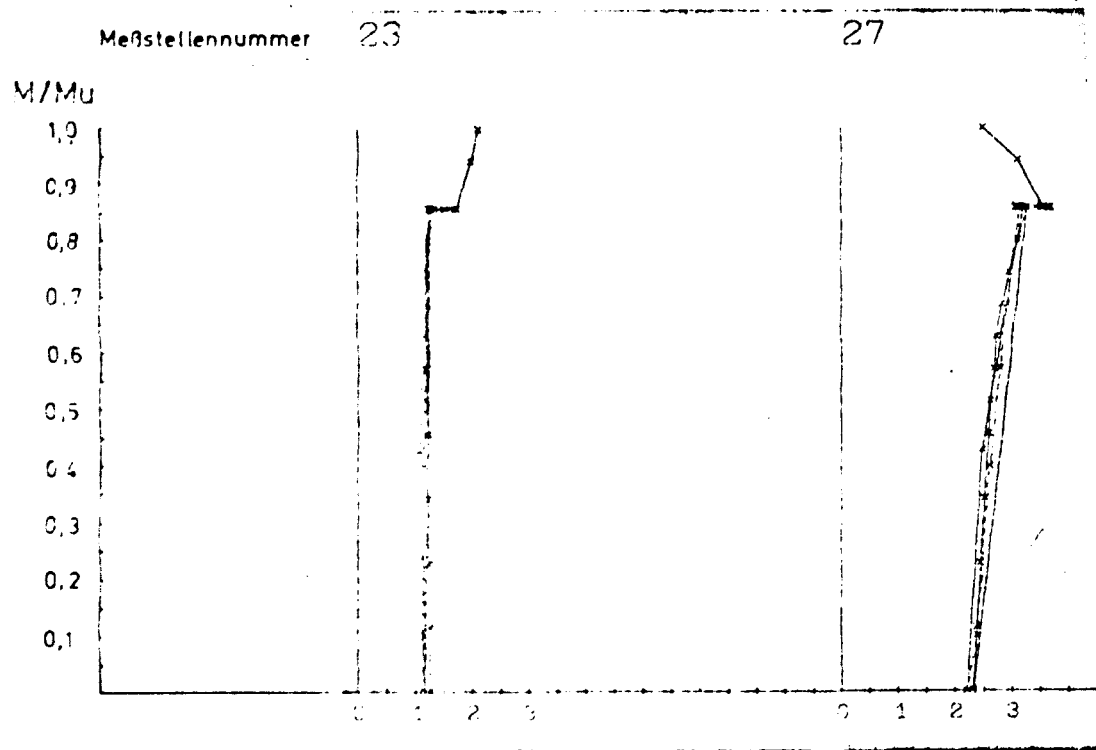
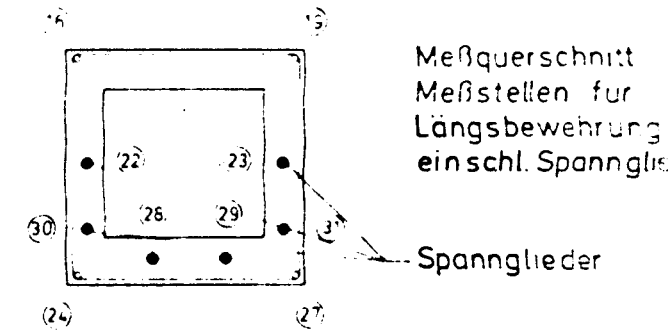
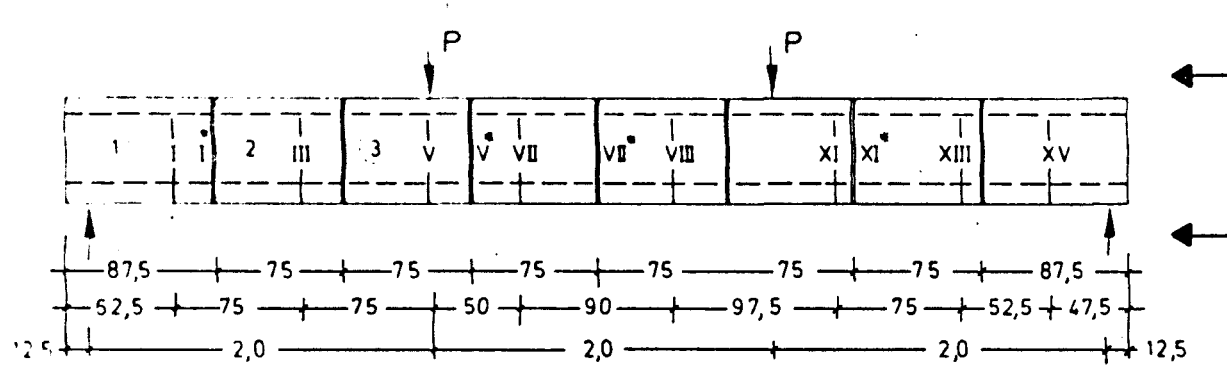
Längsstahldehnungen des Balkens SETMQ 1

Schnitt VII



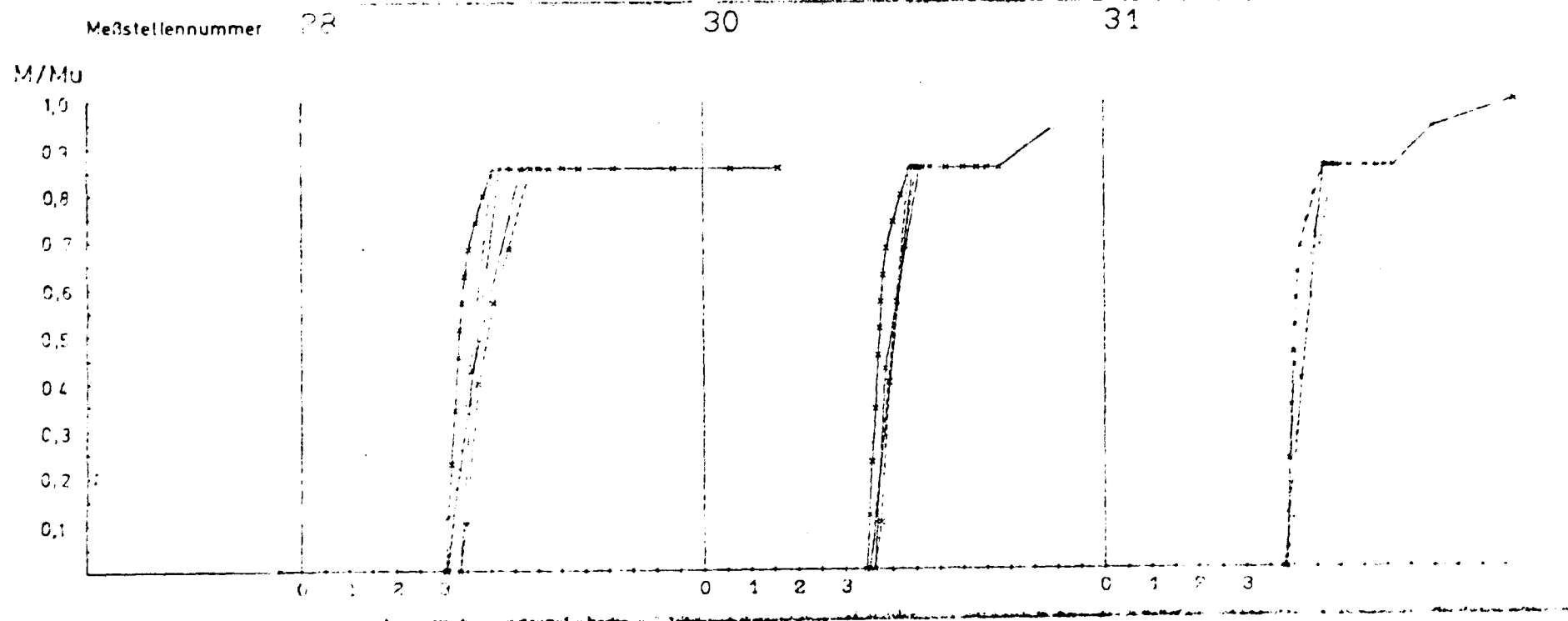
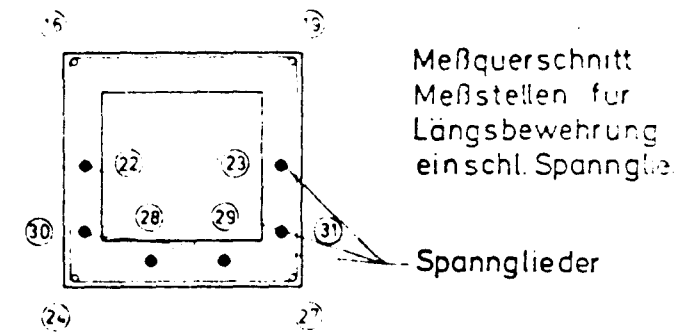
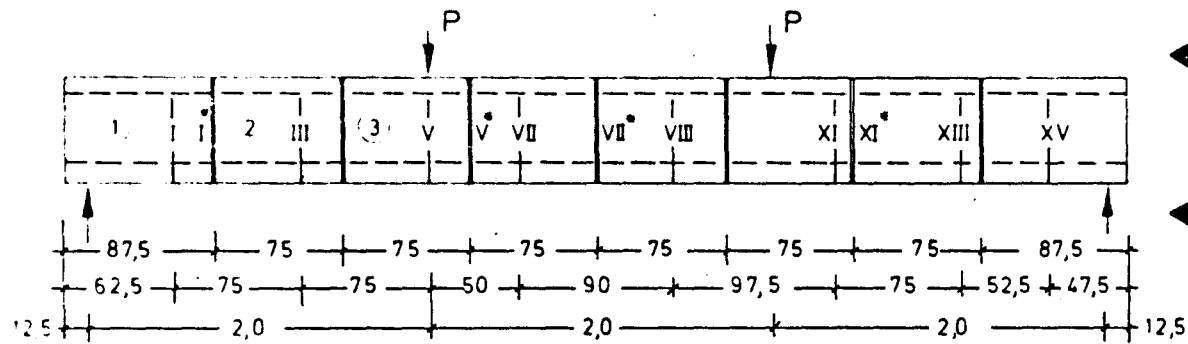
Längsstahldehnungen des Balkens SETMQ 1

Schnitt VII*



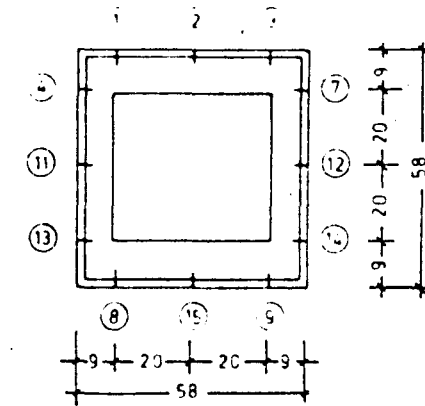
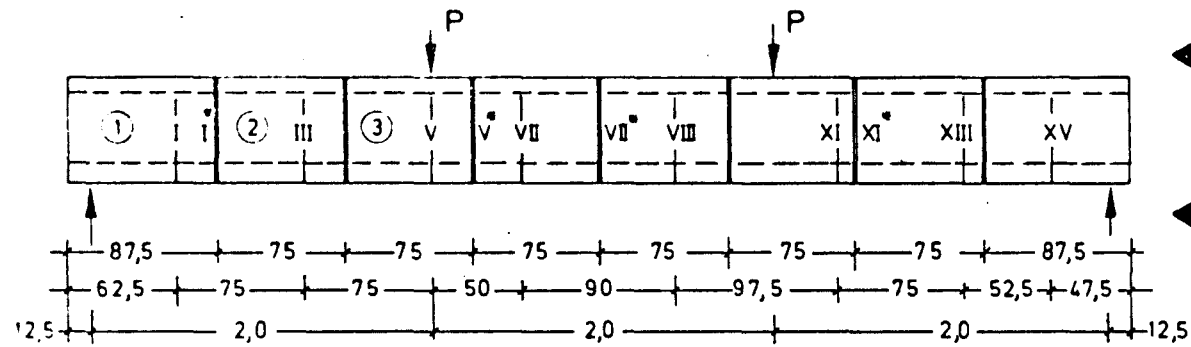
Längsstahldehnungen des Balkens SETMQ 1

Schnitt VII*

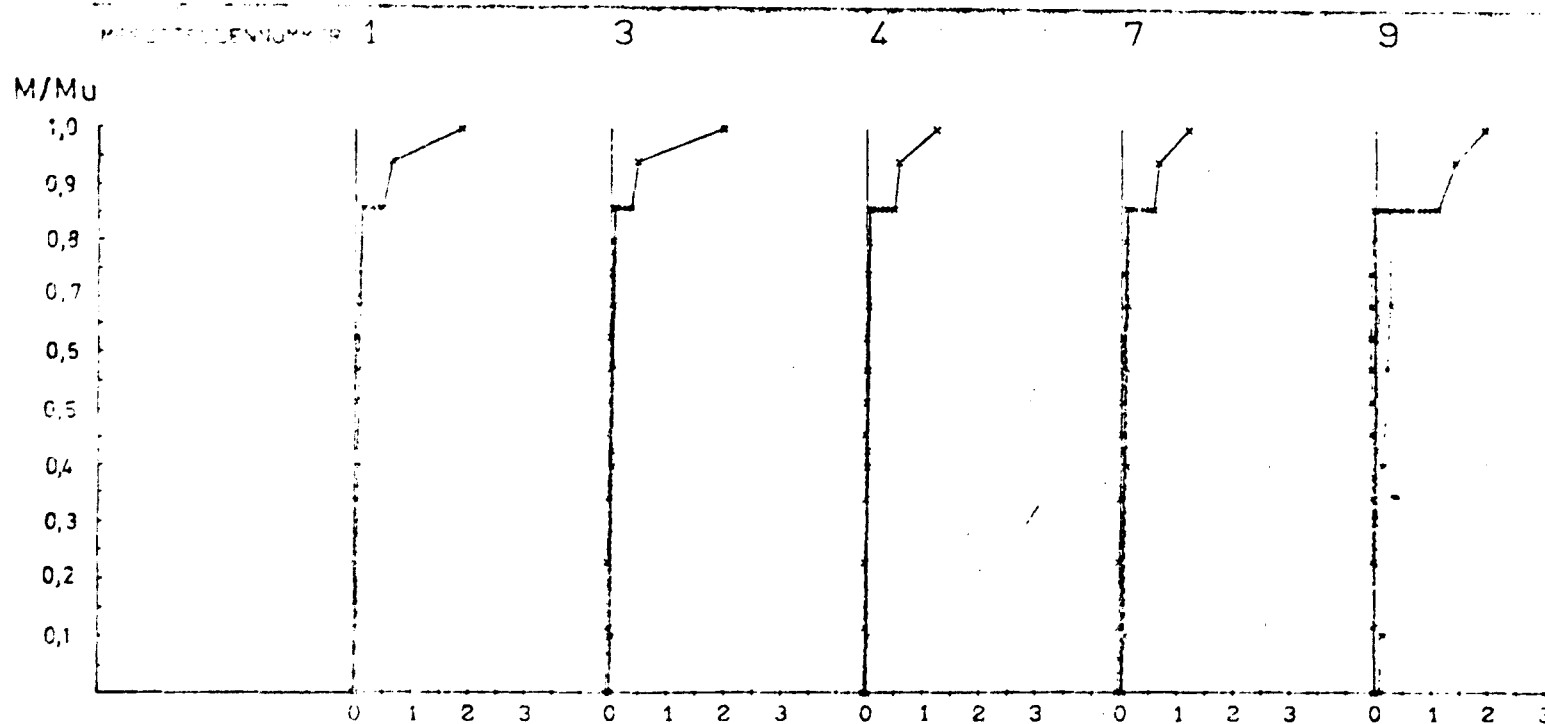


Bügeldehnungen des Balkens SETMQ 1

Schnitt VIII

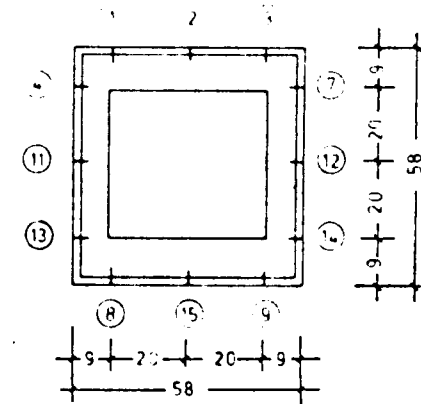
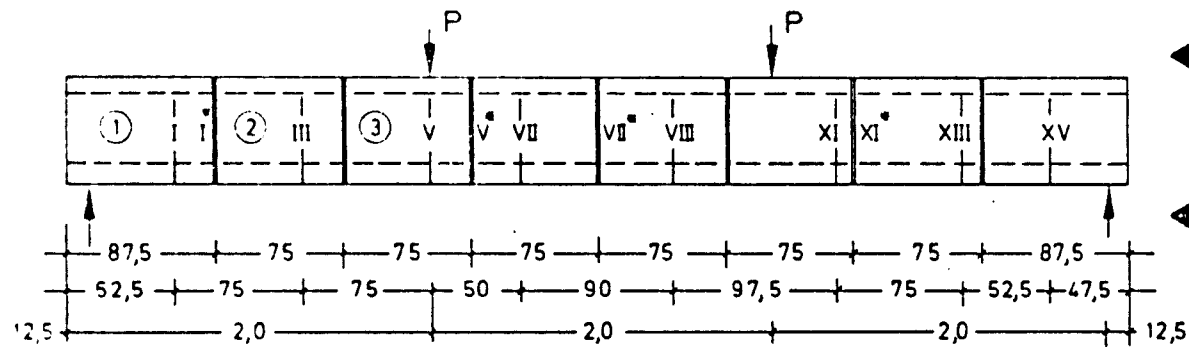


Meßquerschnitt
Meßstellen für
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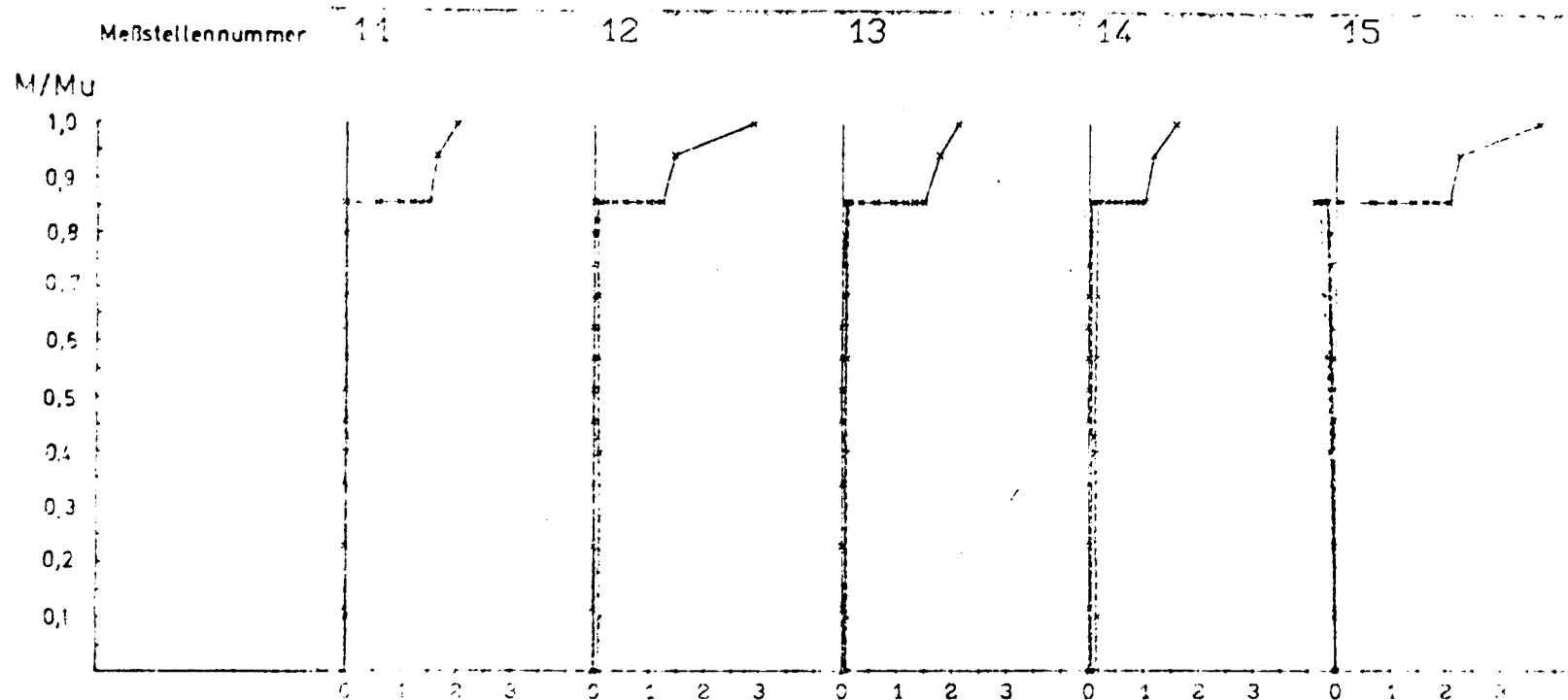


Bügeldehnungen des Balkens SETMQ 1

Schnitt VIII

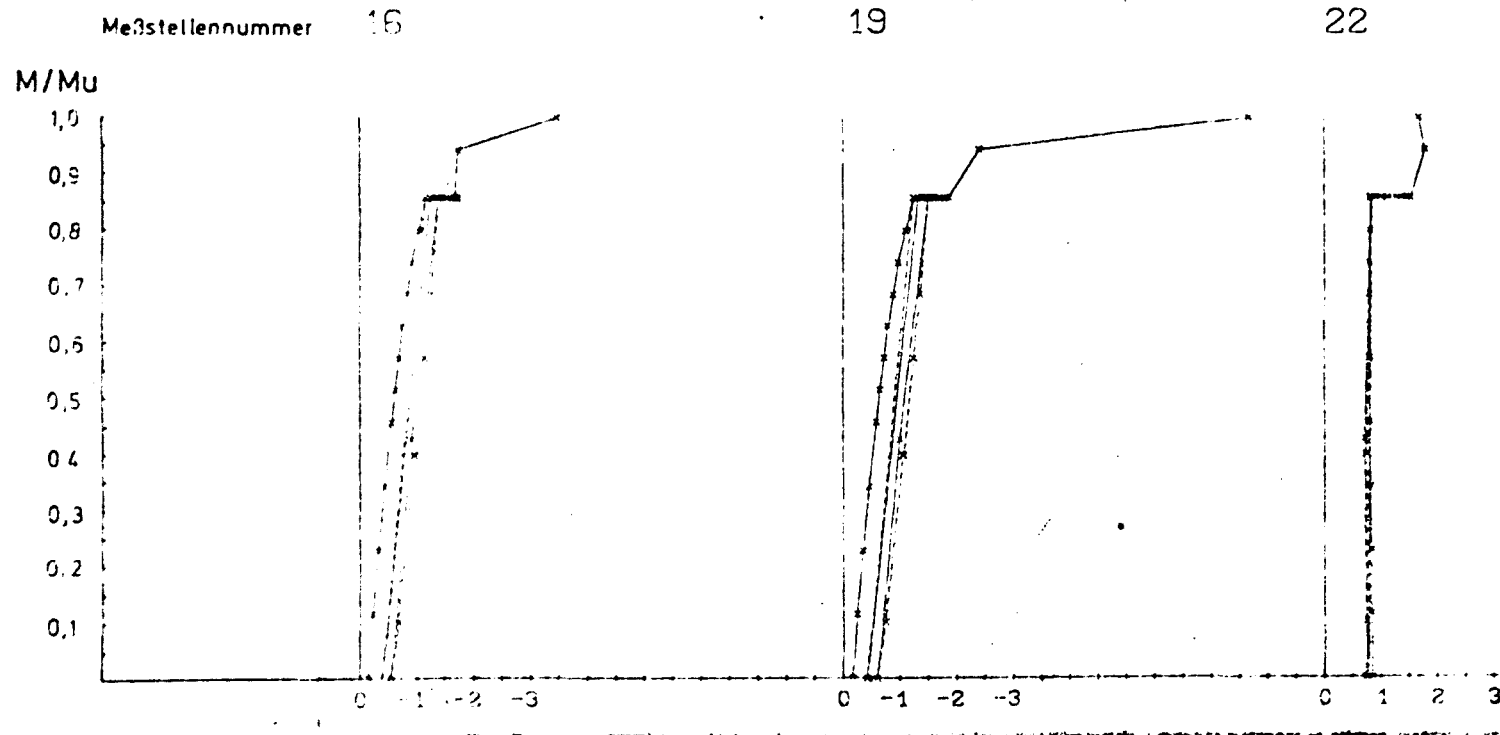
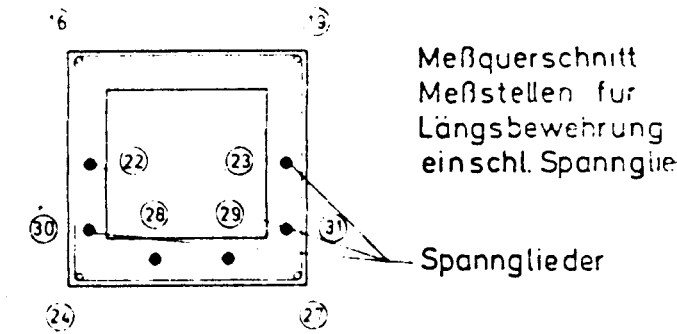
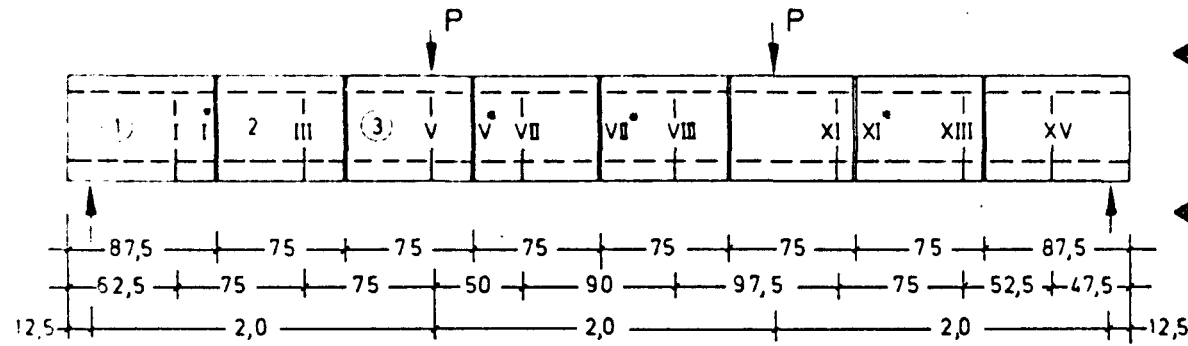


Meßquerschnitt
Meßstellen für
Bügel



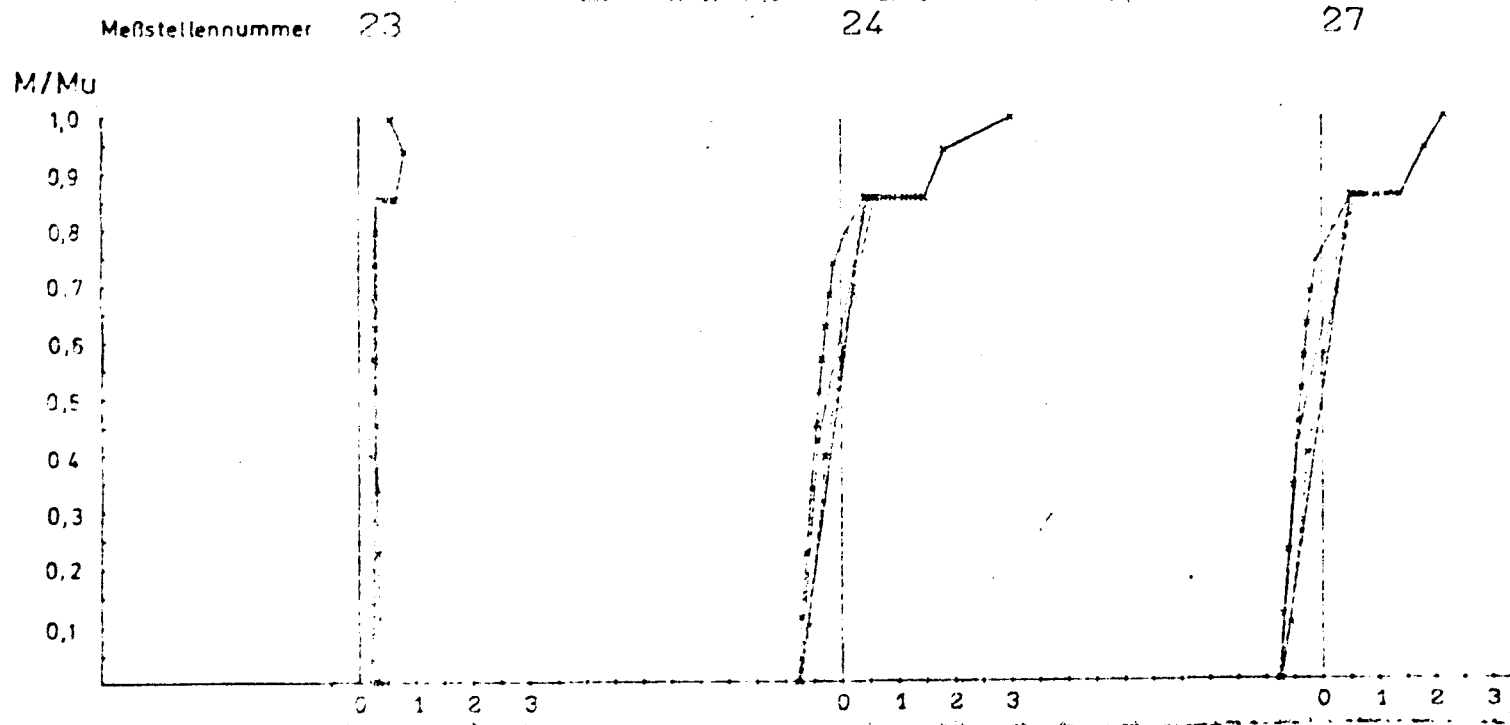
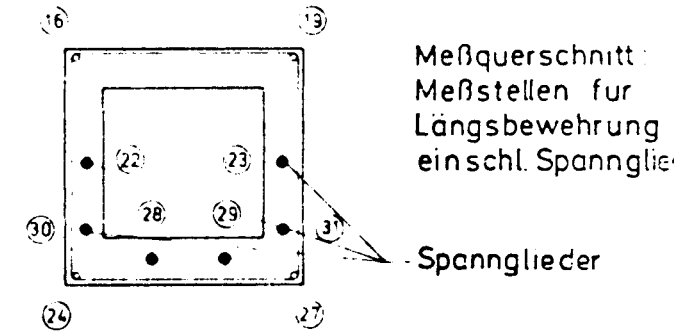
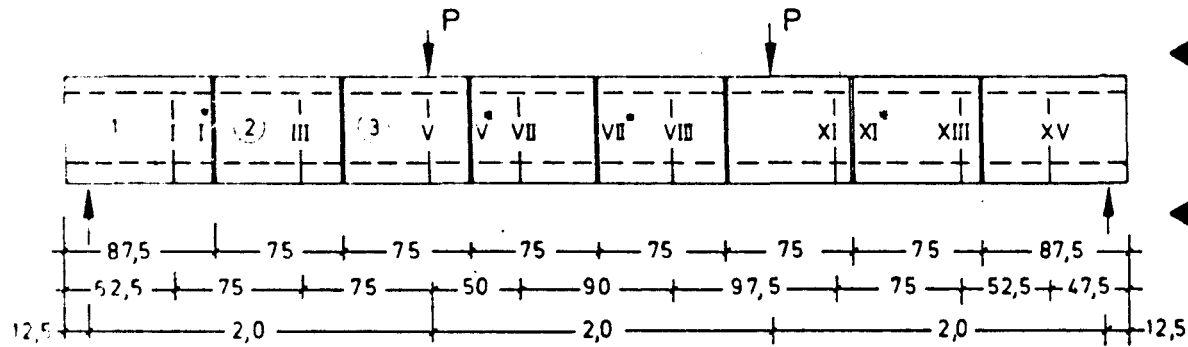
Längsstahldehnungen des Balkens SETMQ 1

Schnitt VIII

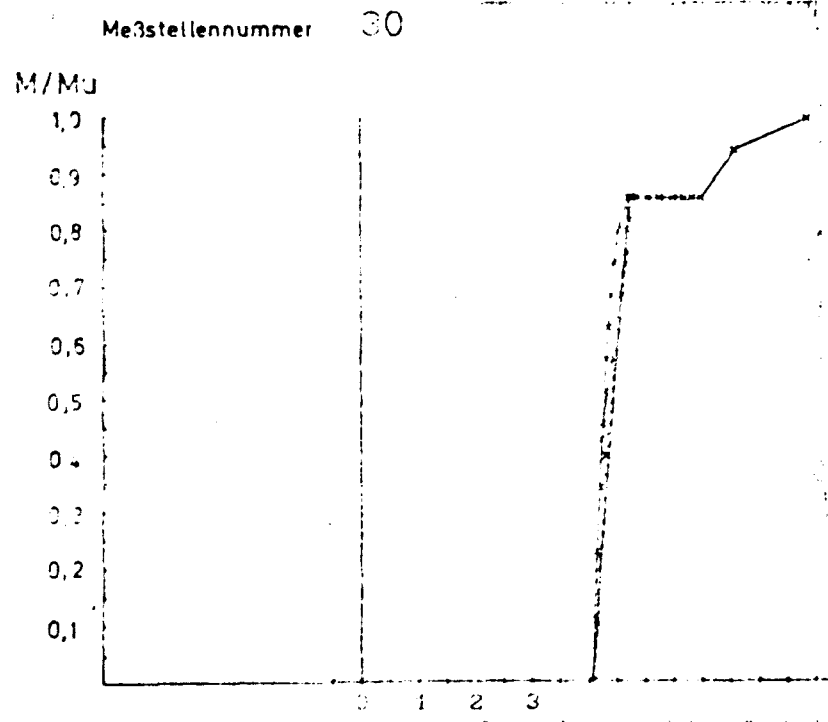
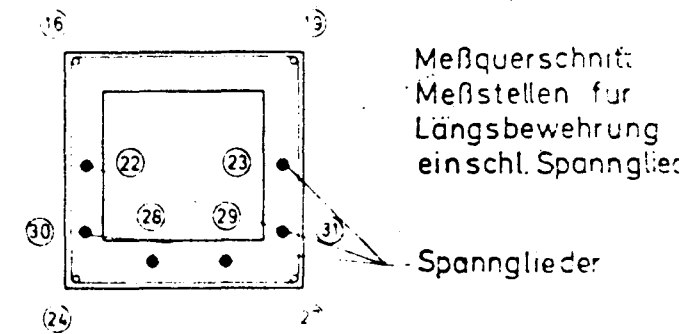
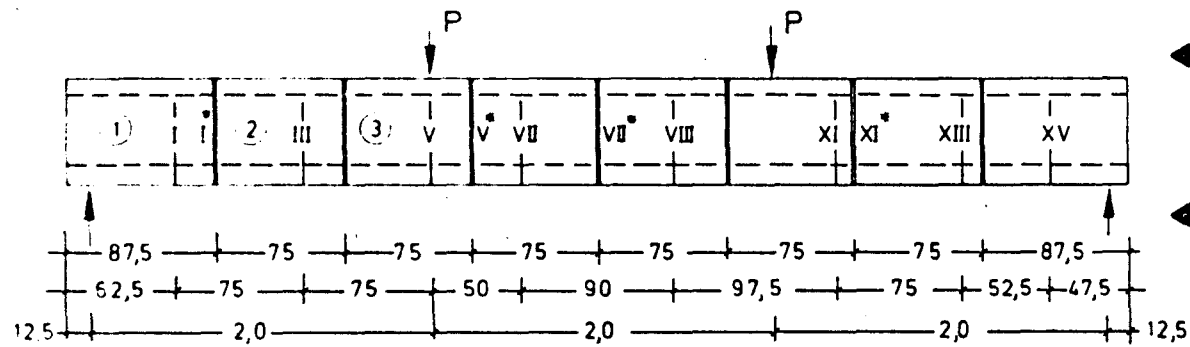


Längsstahldehnungen des Balkens SETMQ 1

Schnitt VIII

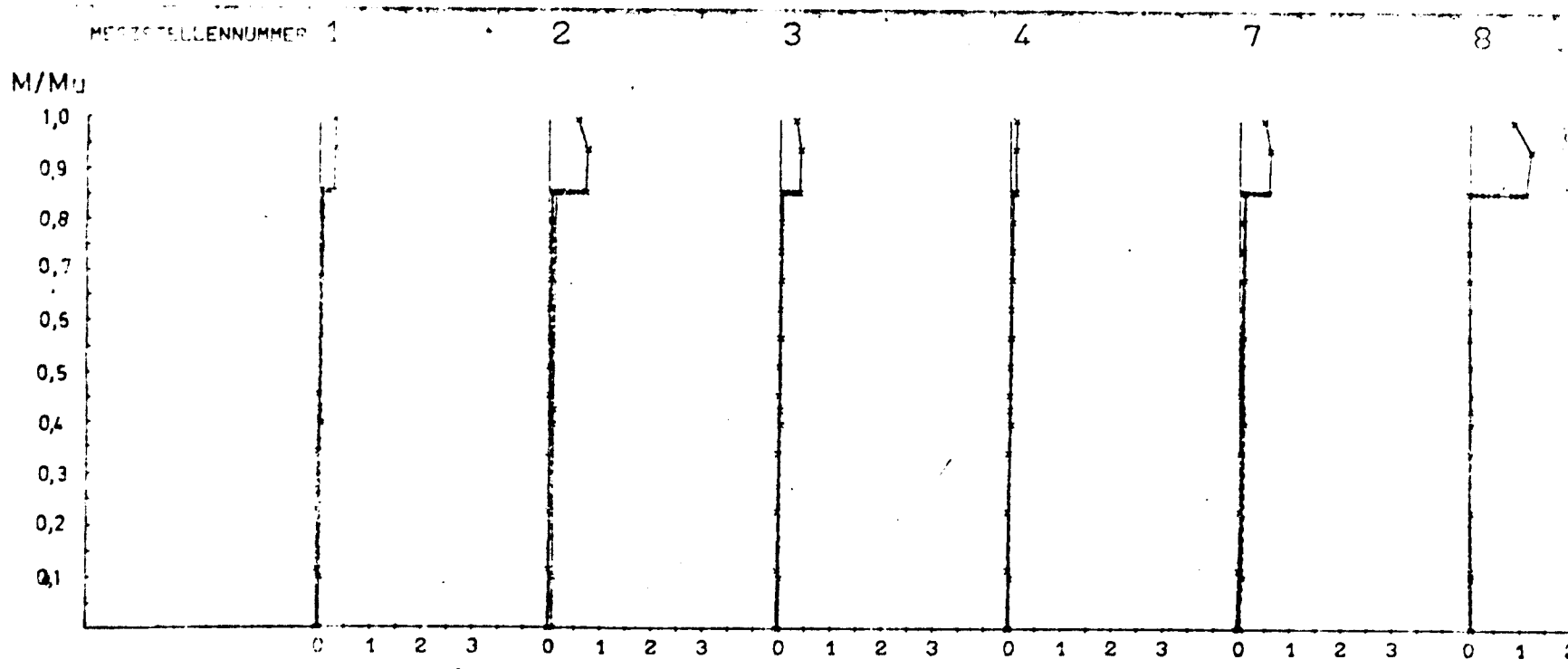
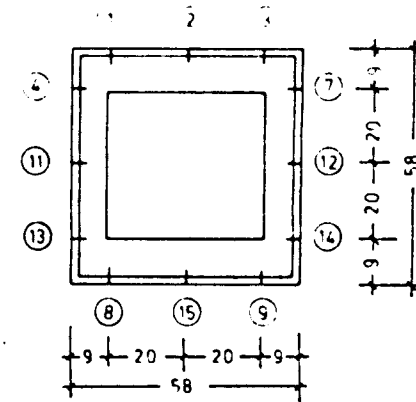
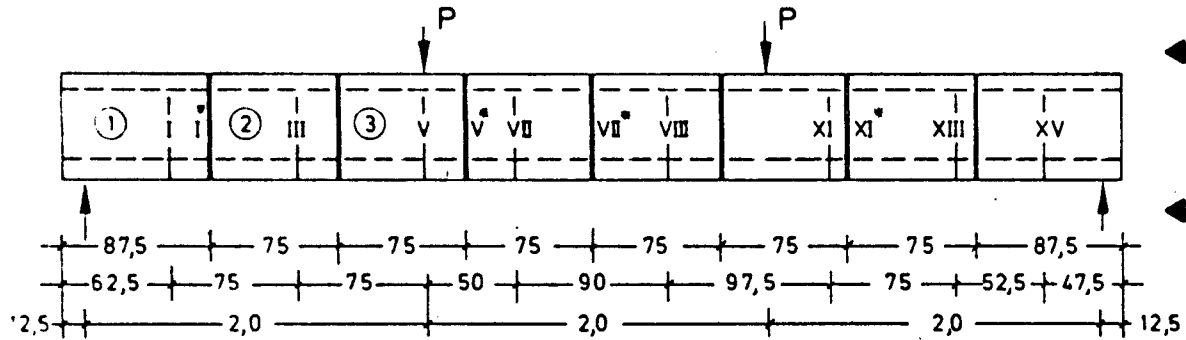


Schnitt VIII



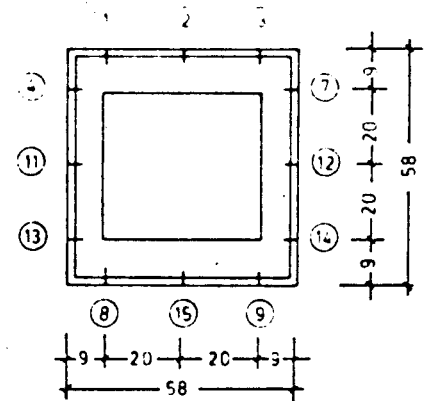
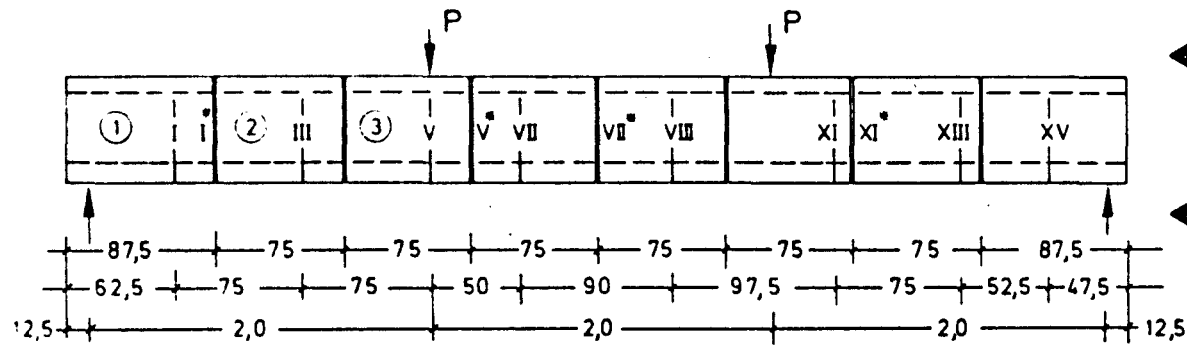
Bügeldehnungen des Balkens SETMQ 1

Schnitt XI

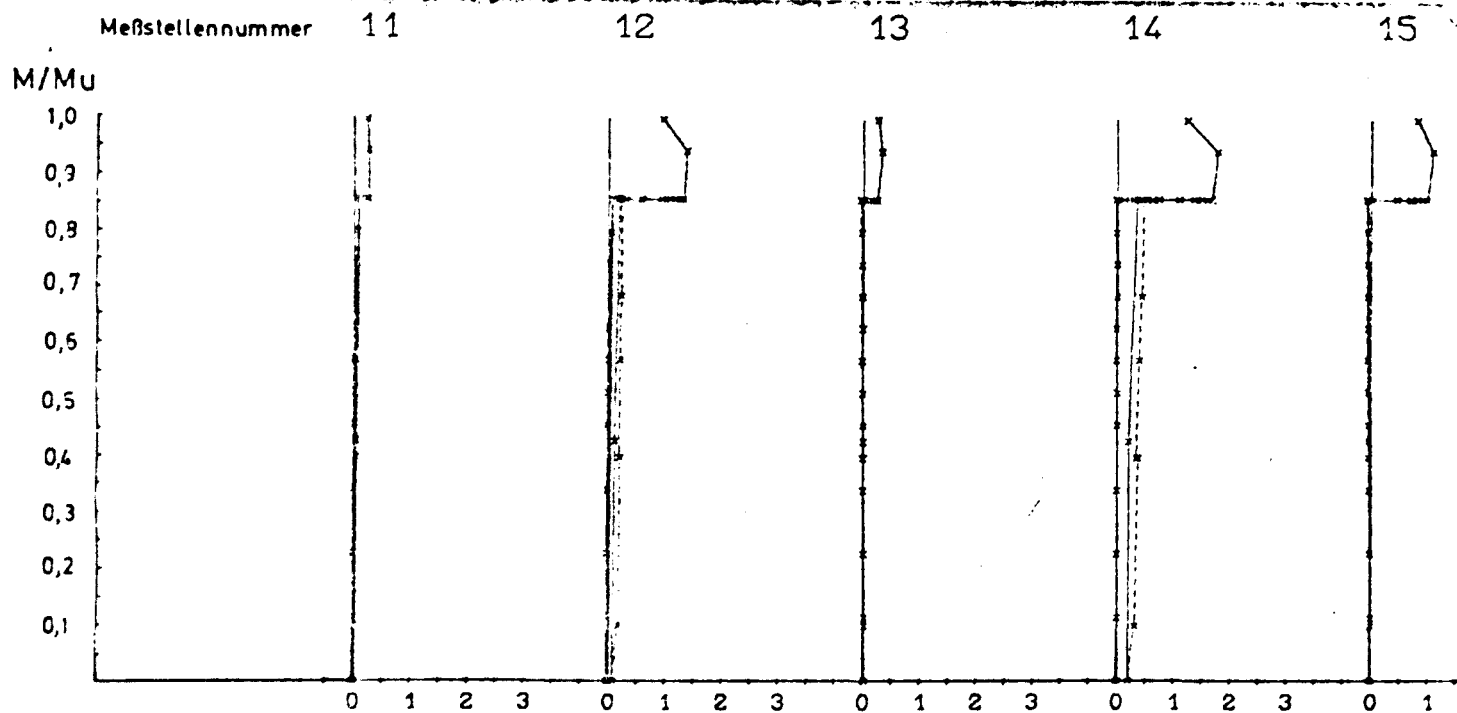


Bügeldehnungen des Balkens SETMQ 1

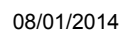
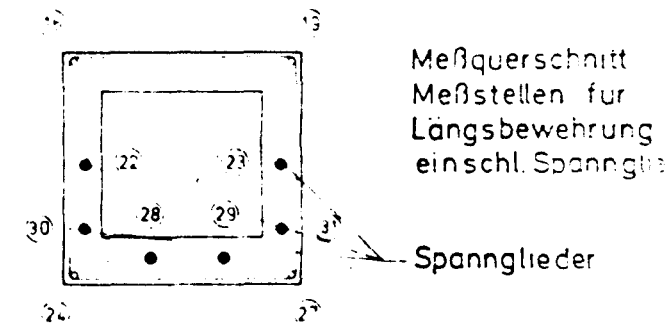
Schnitt XI



Meßquerschnitt
Meßstellen für
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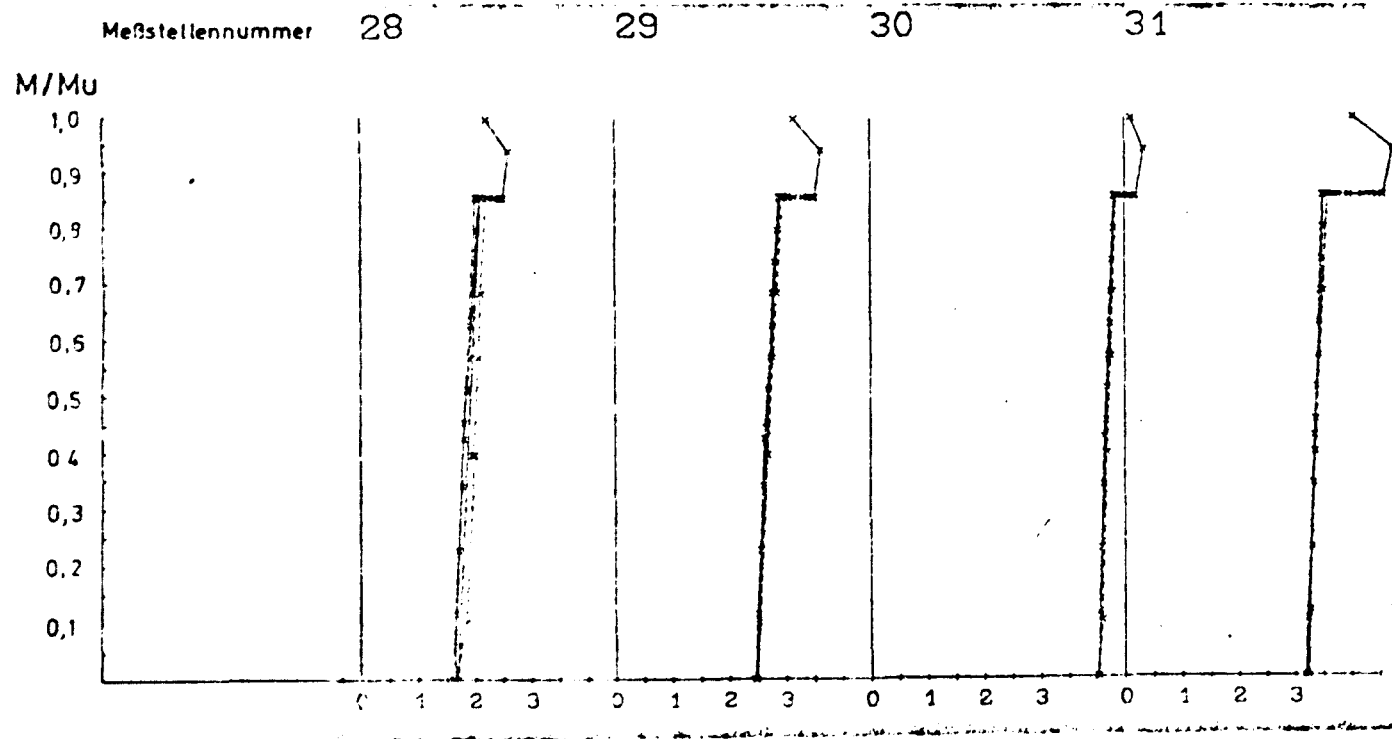
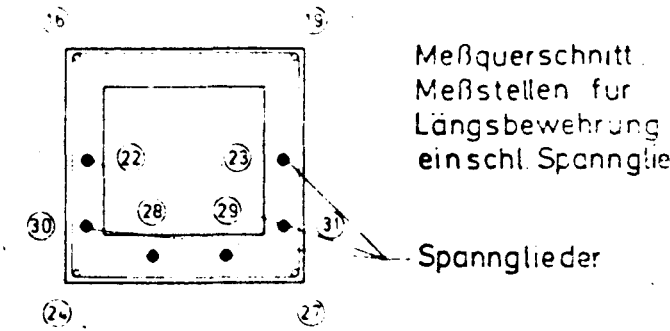
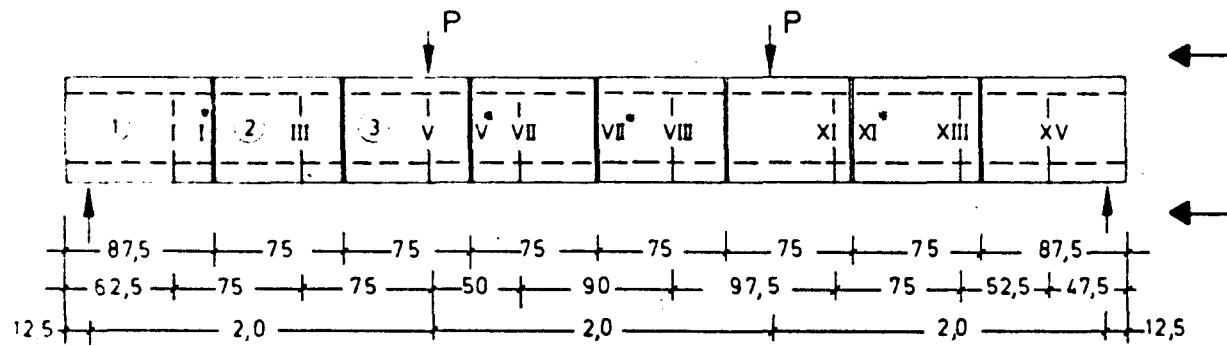


Schnitt XI



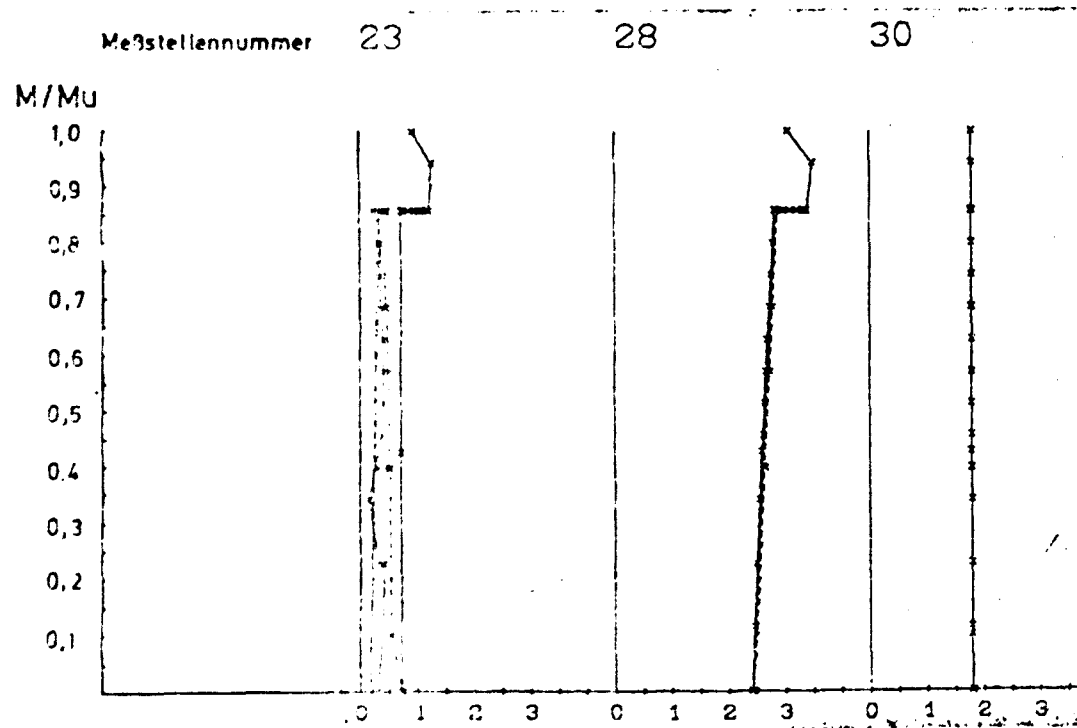
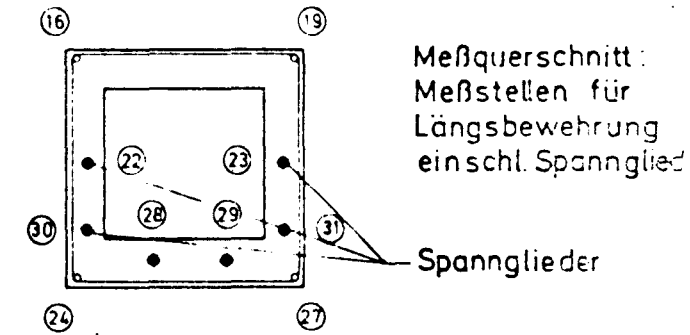
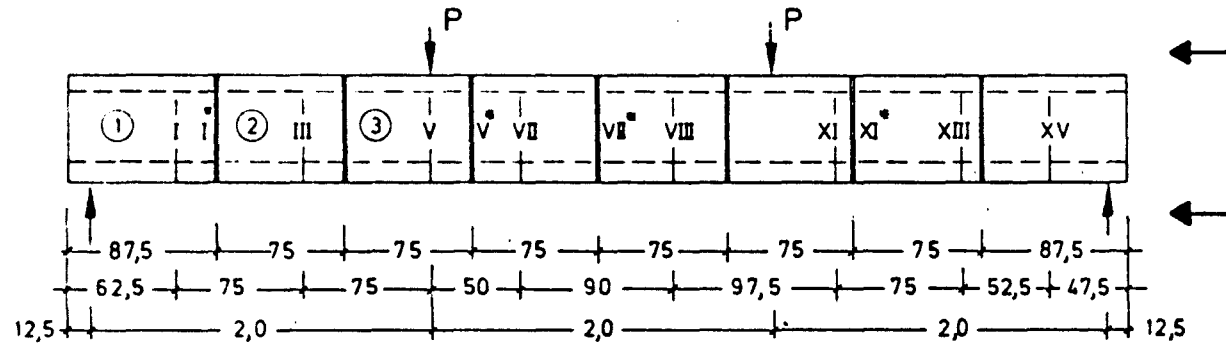
Längsstahldehnungen des Balkens SETMQ 1

Schnitt XI



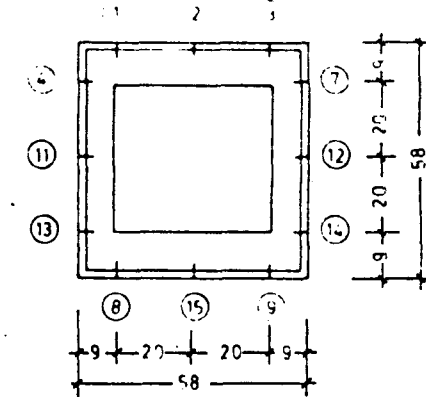
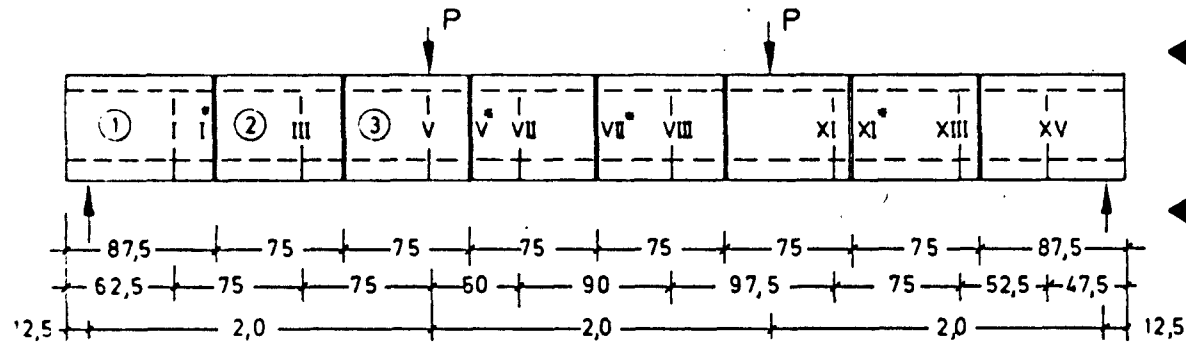
Längsstahldehnungen des Balkens SETMQ 1

Schnitt XI *

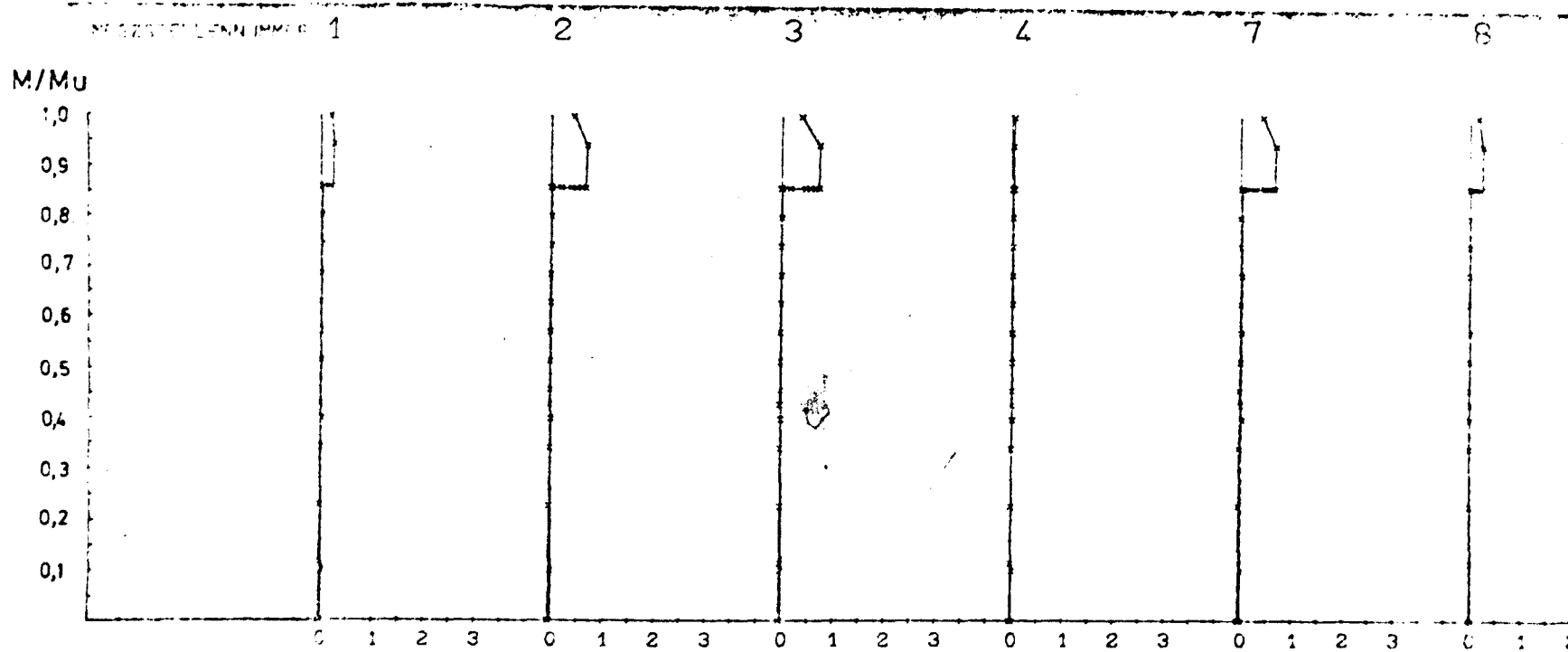


Bügeldehnungen des Balkens SETMQ 1

Schnitt XIII

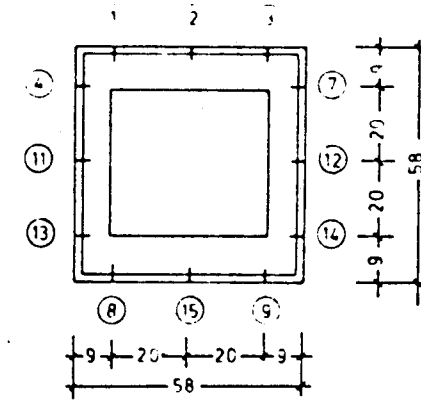
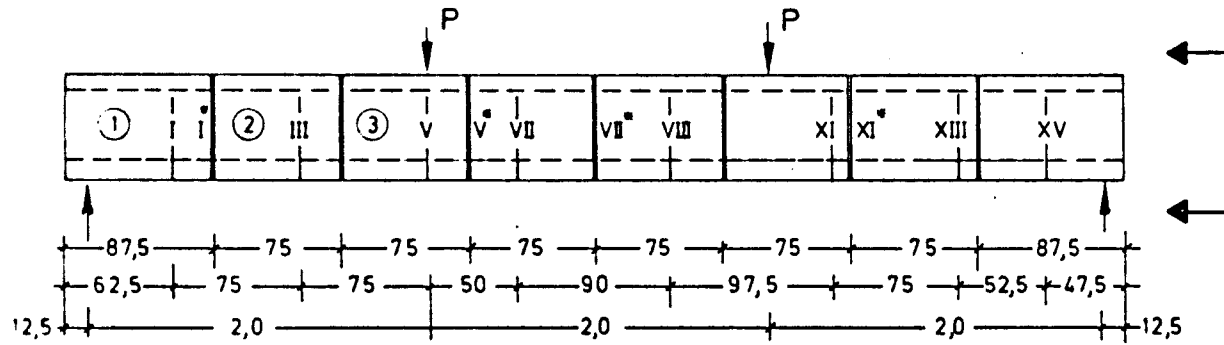


Meßquerschnitt
Meßstellen für
Bugel

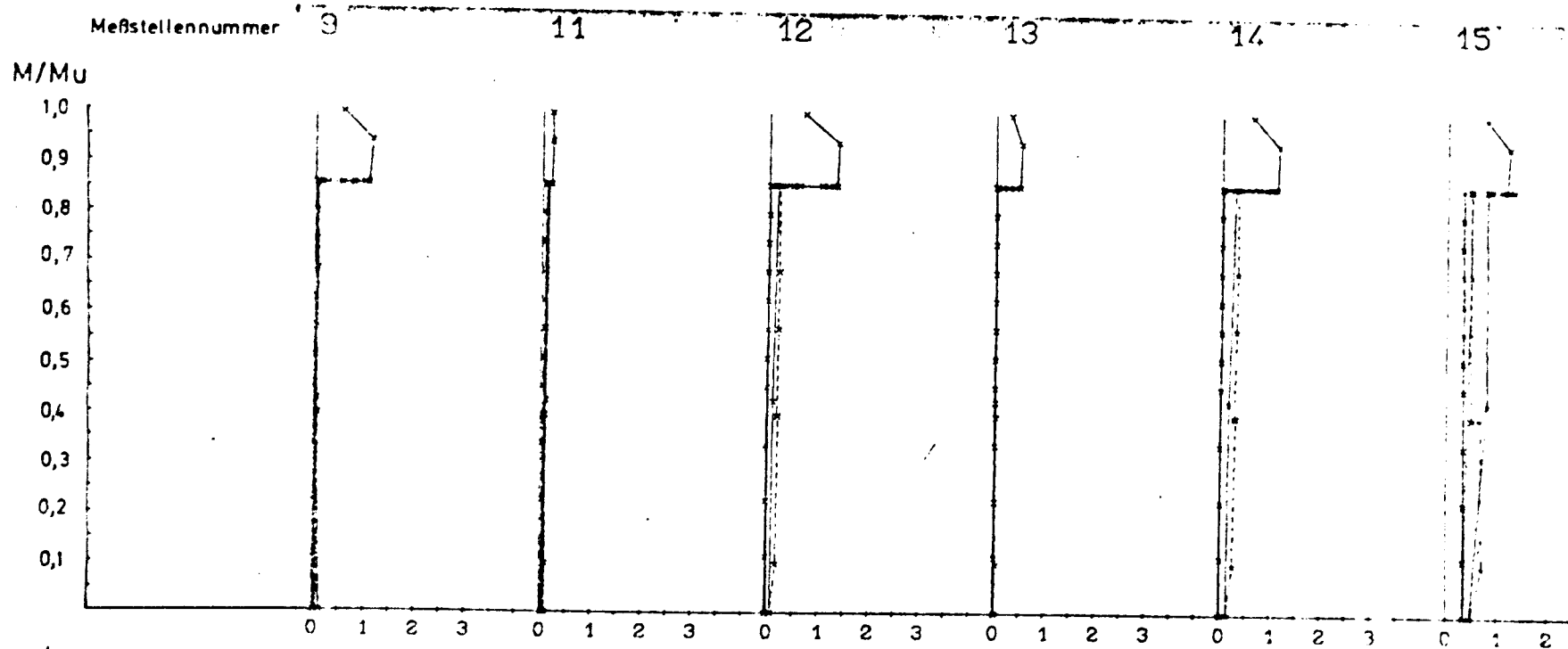


Bügeldehnungen des Balkens SETMQ 1

Schnitt XIII

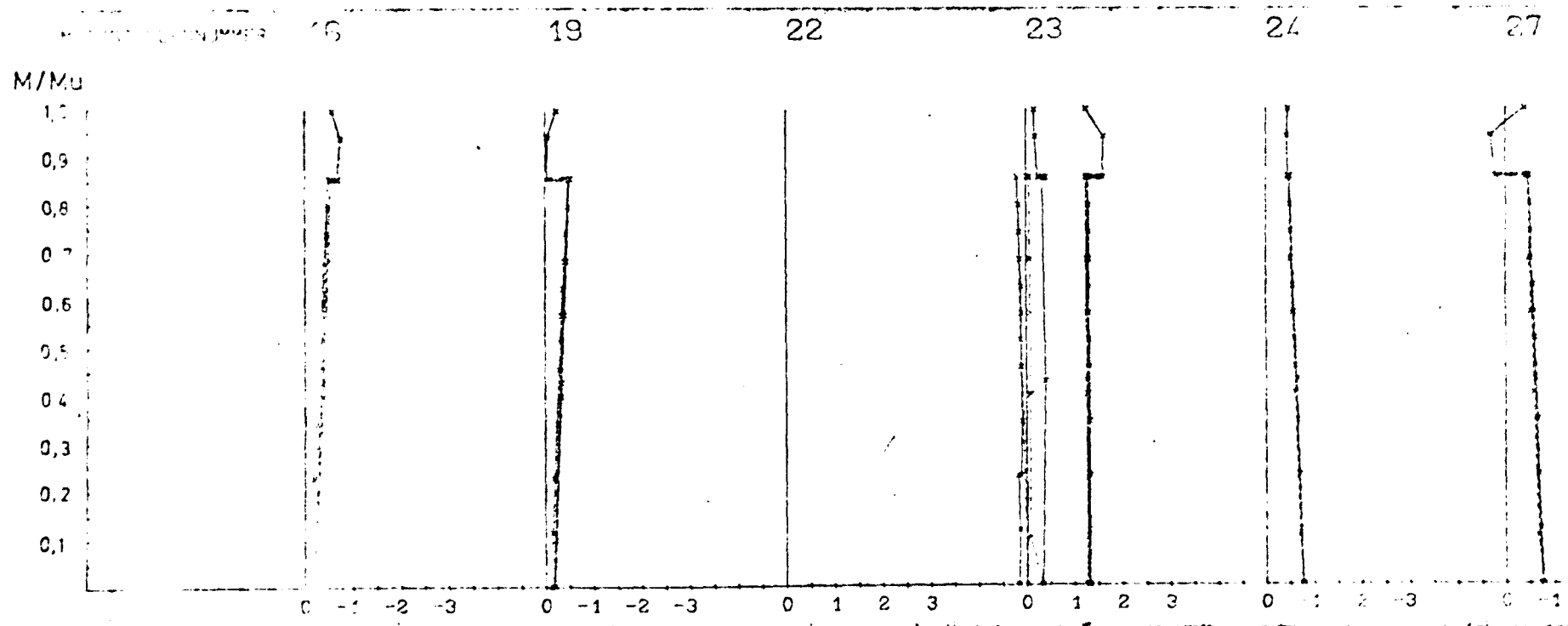
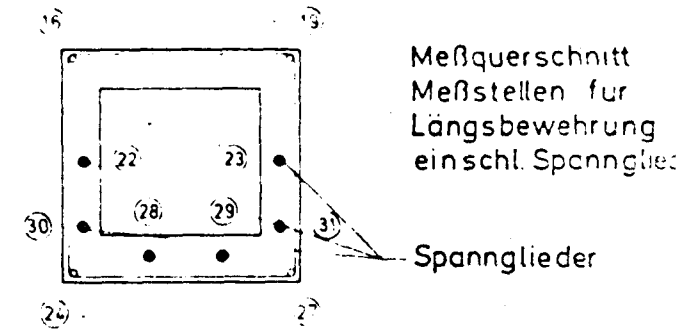
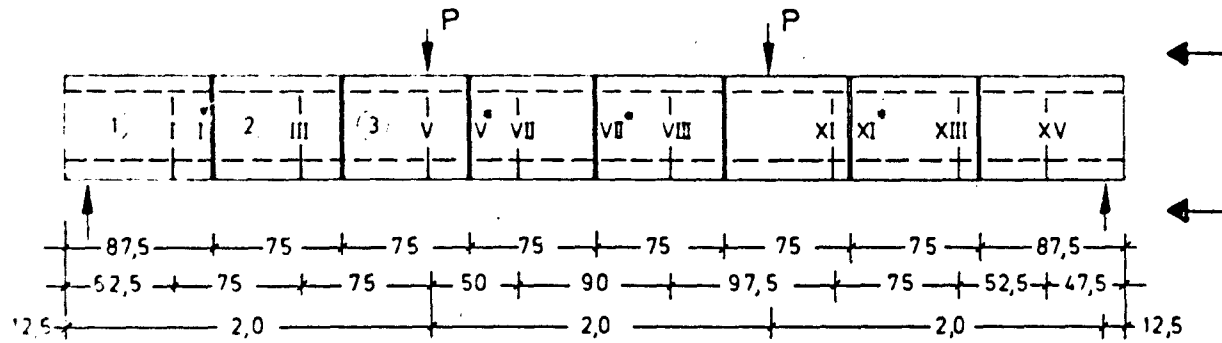


Meßquerschnitt
Meßstellen für
Bugel



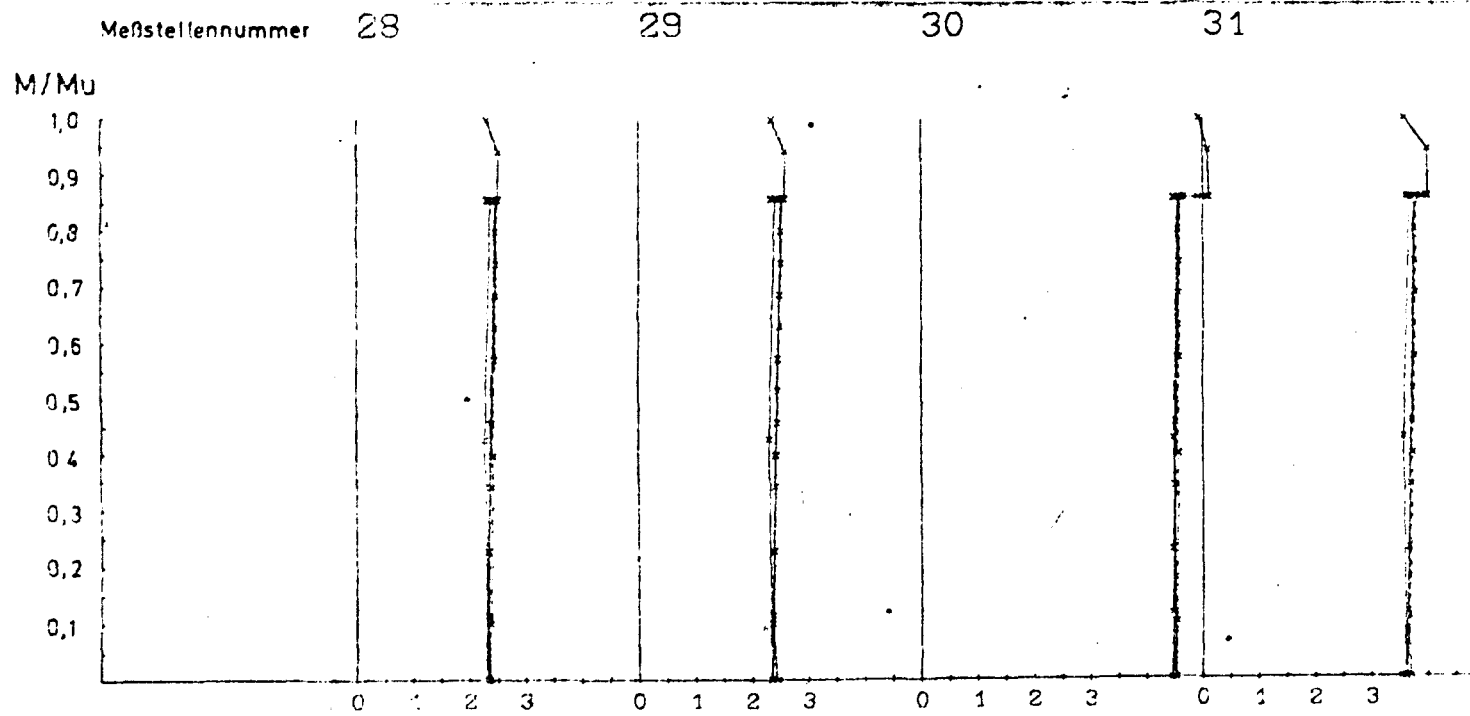
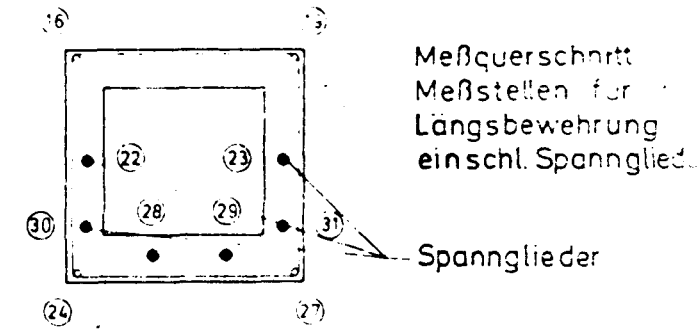
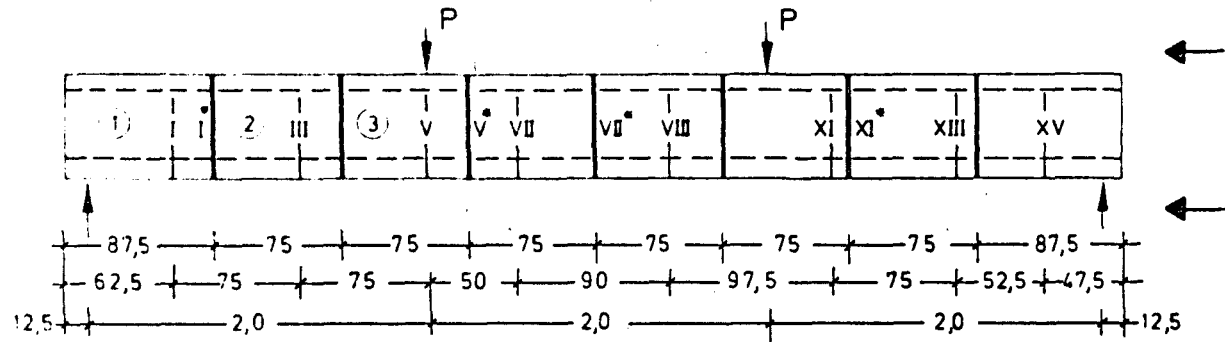
Längsstahldehnungen des Balkens SETMQ 1

Schnitt XIII



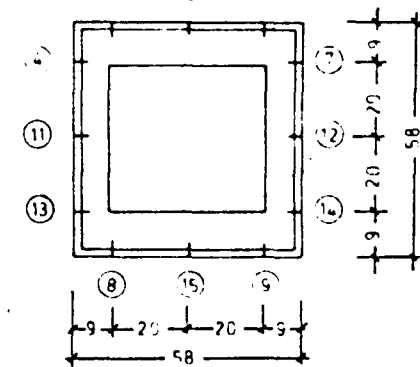
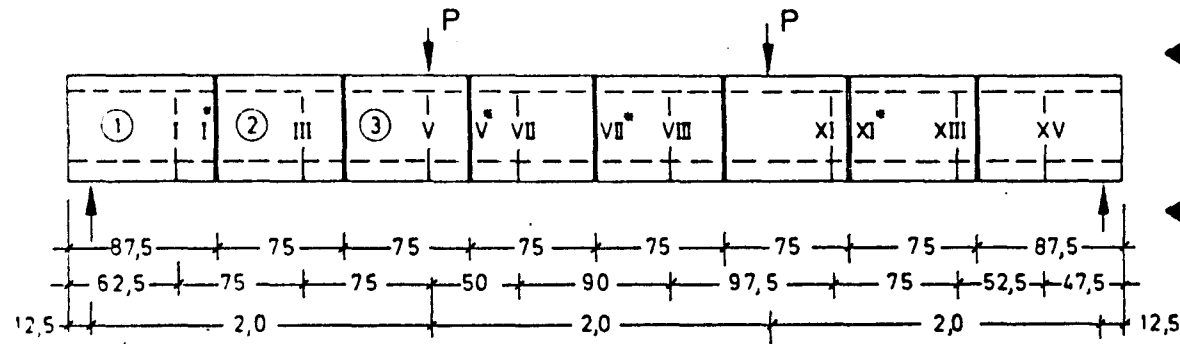
Längsstahldehnungen des Balkens SETMQ 1

Schnitt X III

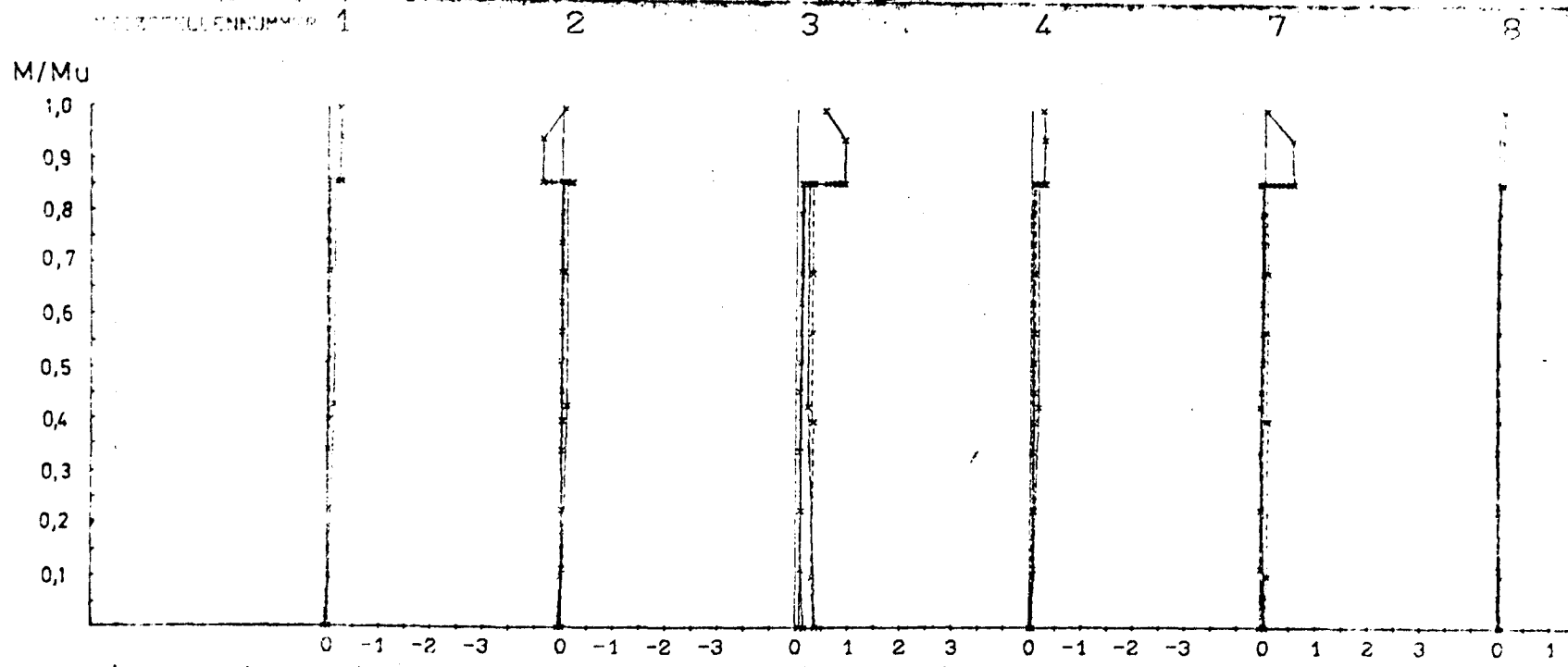


Bügeldehnungen des Balkens SETMQ 1

Schnitt XV

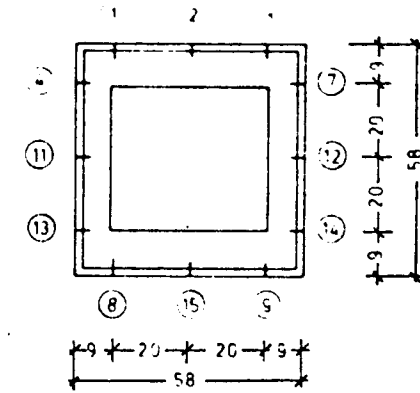
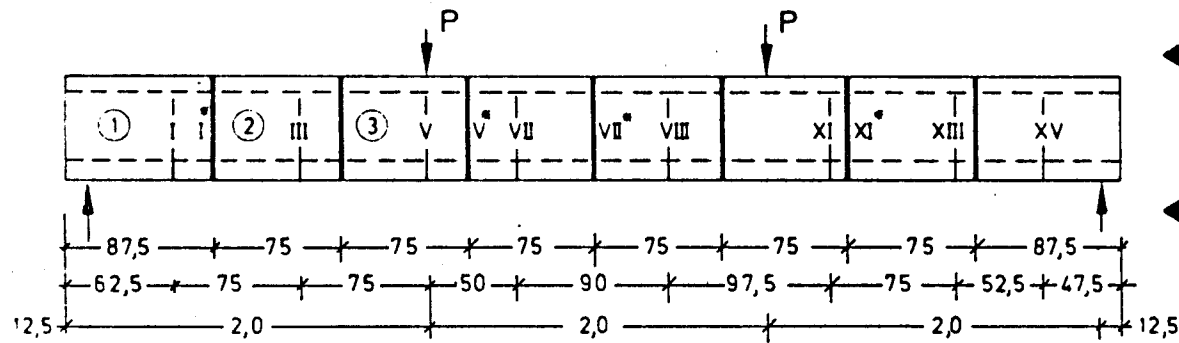


Meßquerschnitt
Meßstellen für
Bügel

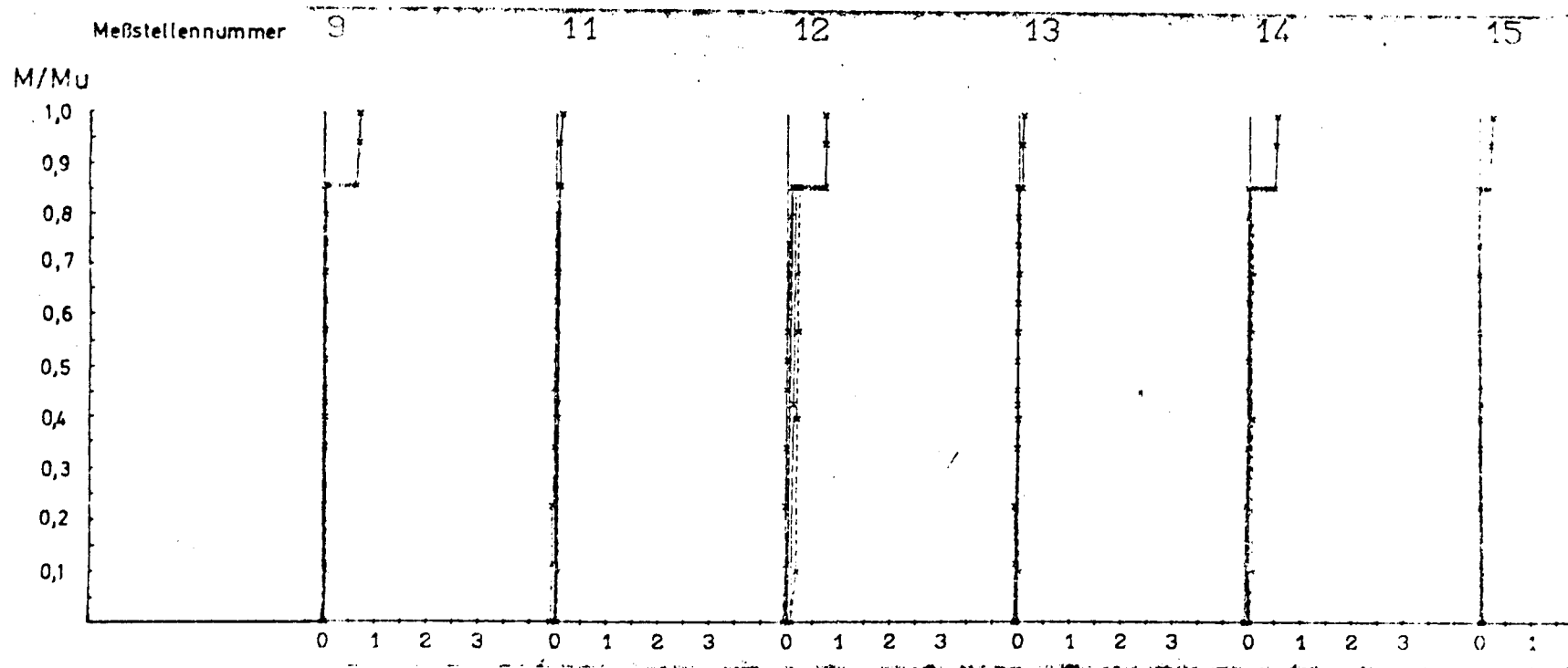


Bügeldehnungen des Balkens SETMQ 1

Schnitt XV

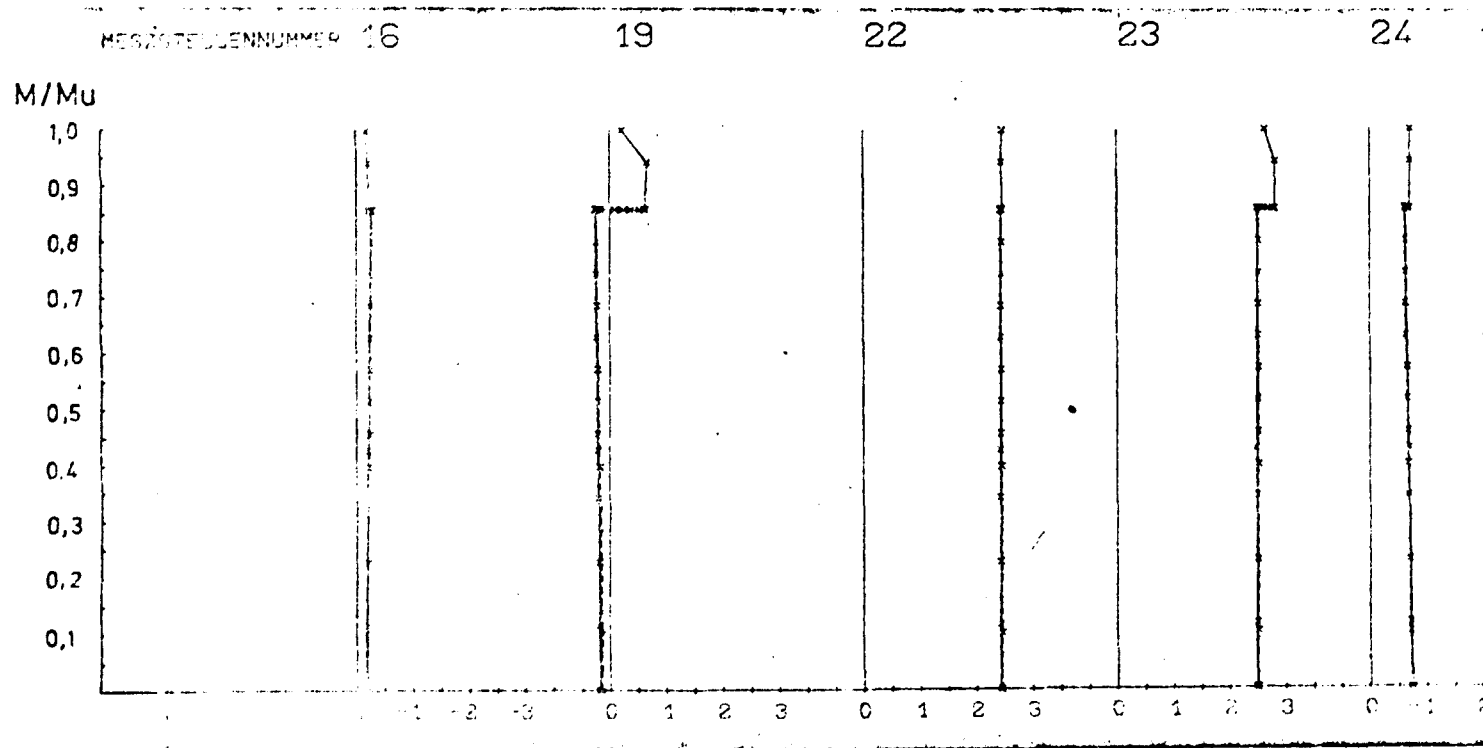
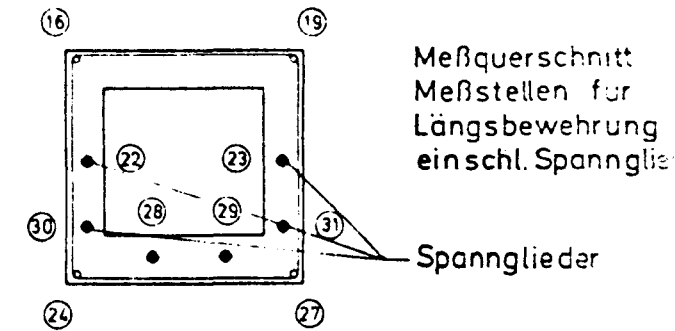
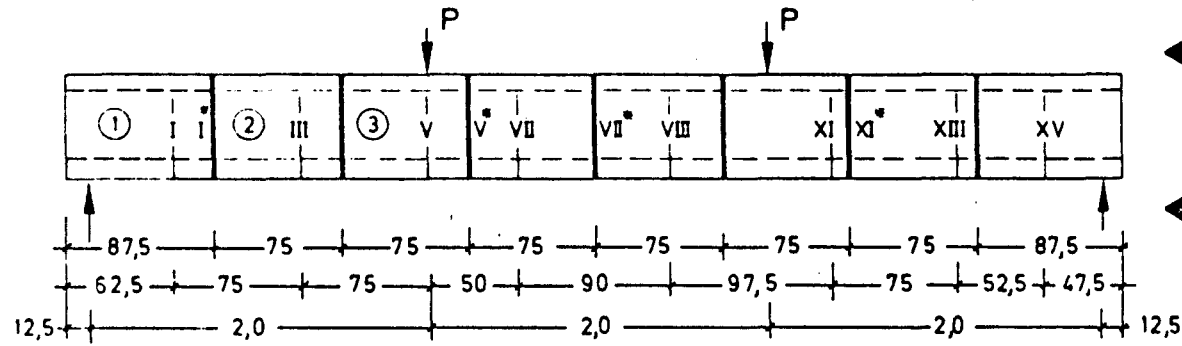


Meßquerschnitt
Meßstellen für
Bugel



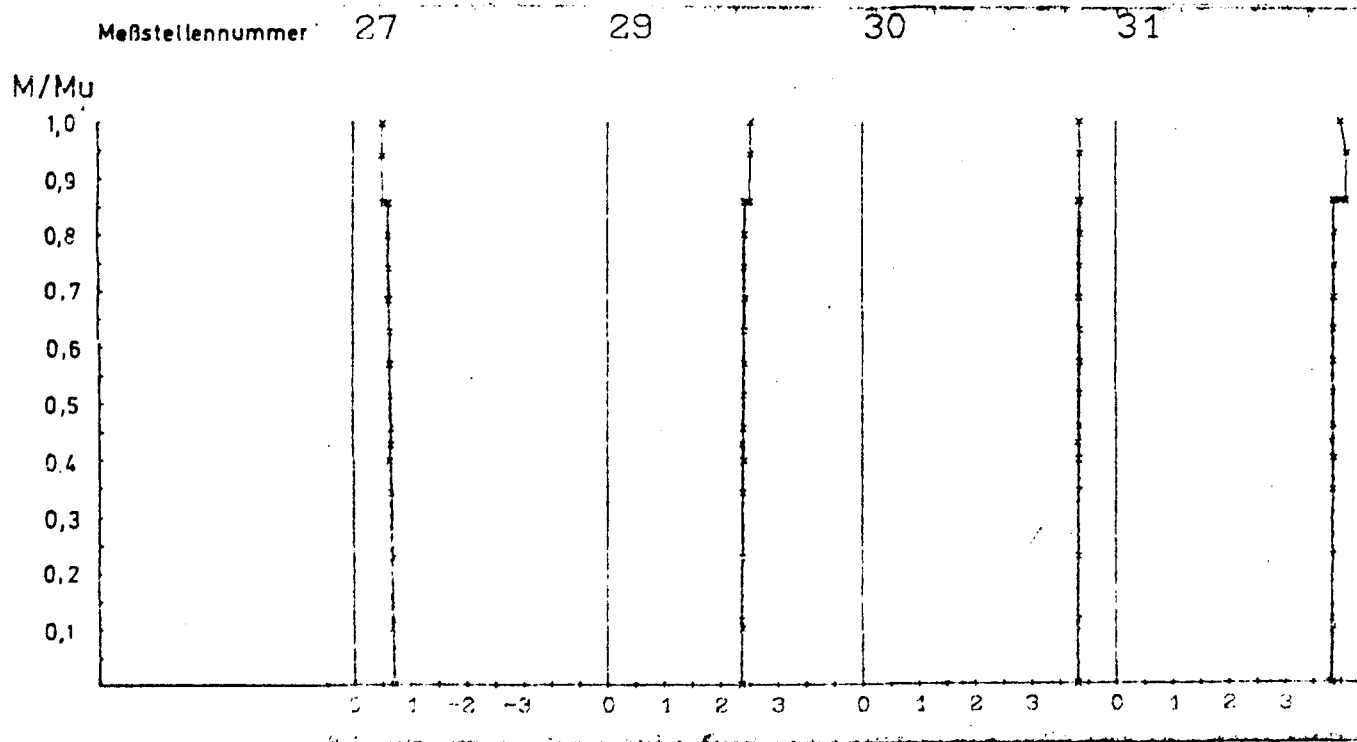
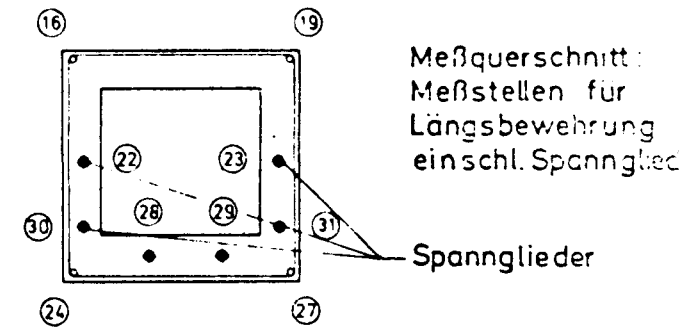
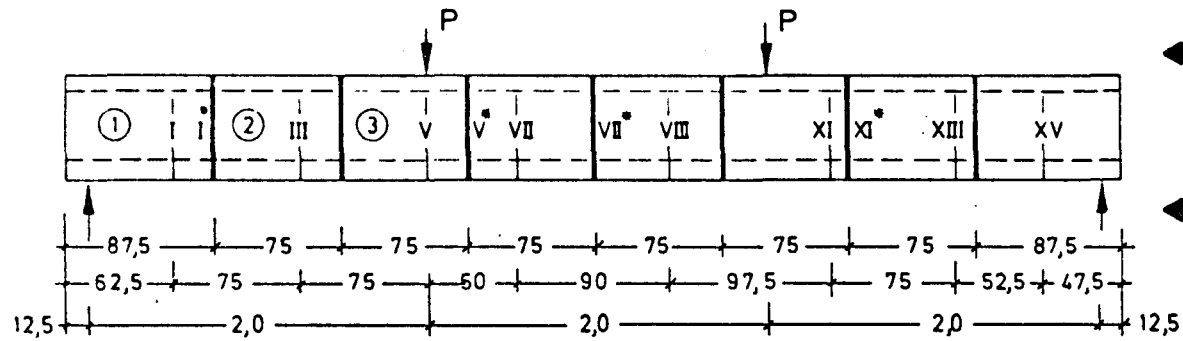
Längsstahldehnungen des Balkens SETMQ 1

Schnitt XV



Längsstahldehnungen des Balkens SETMQ 1

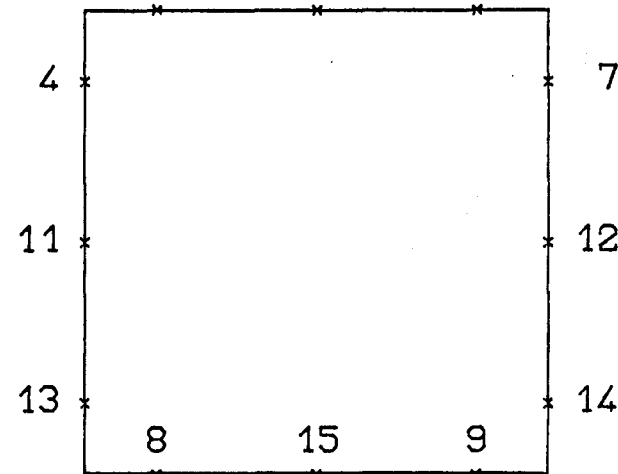
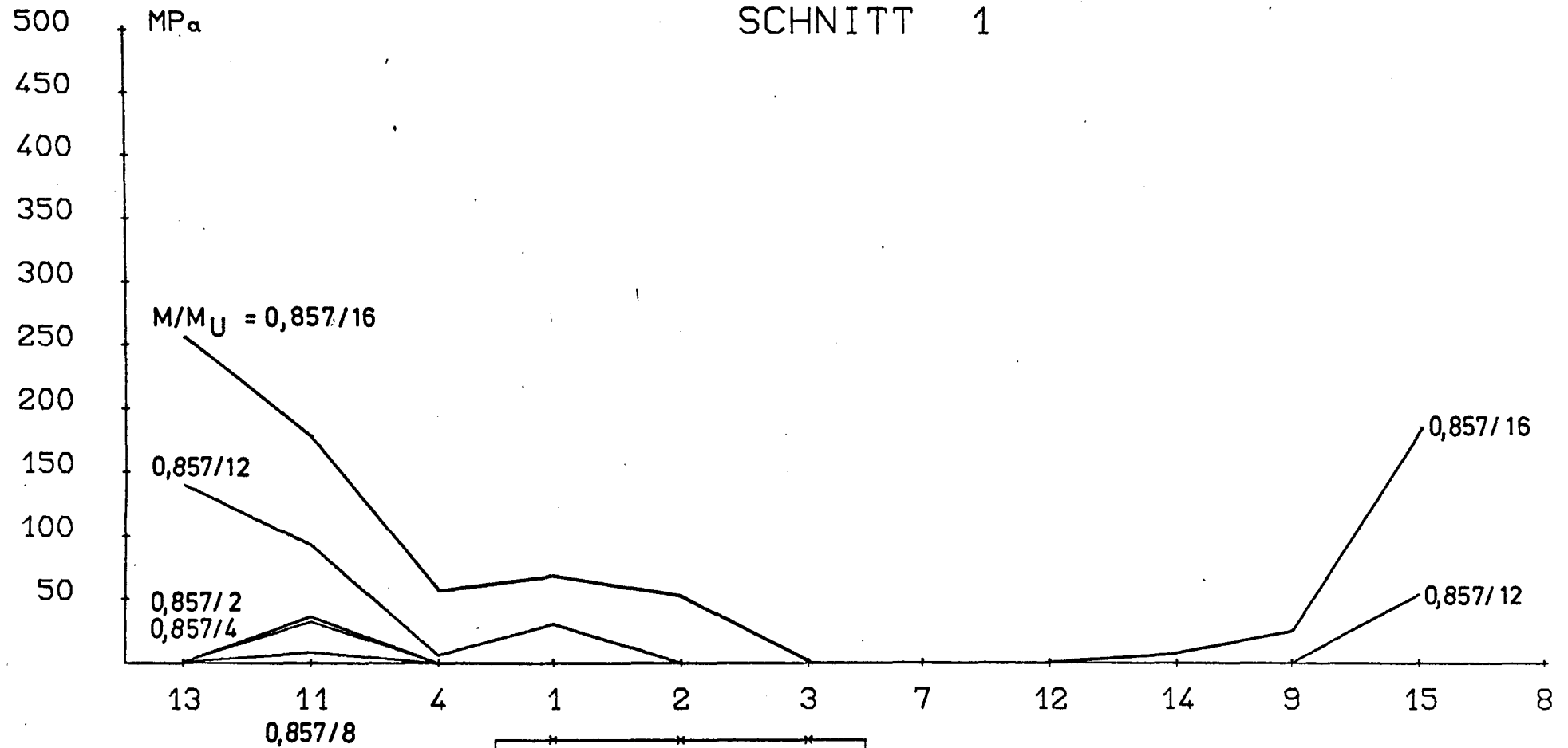
Schnitt XV



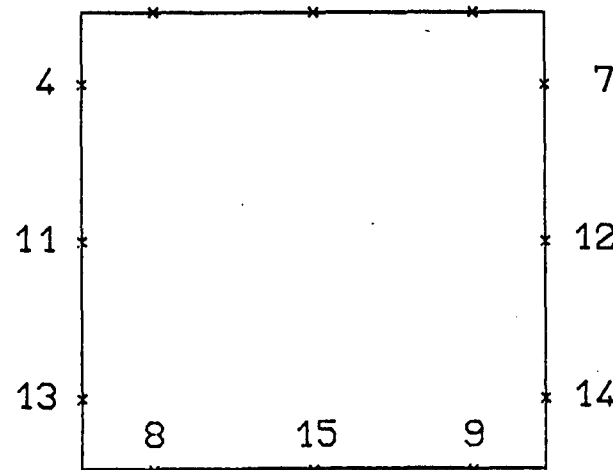
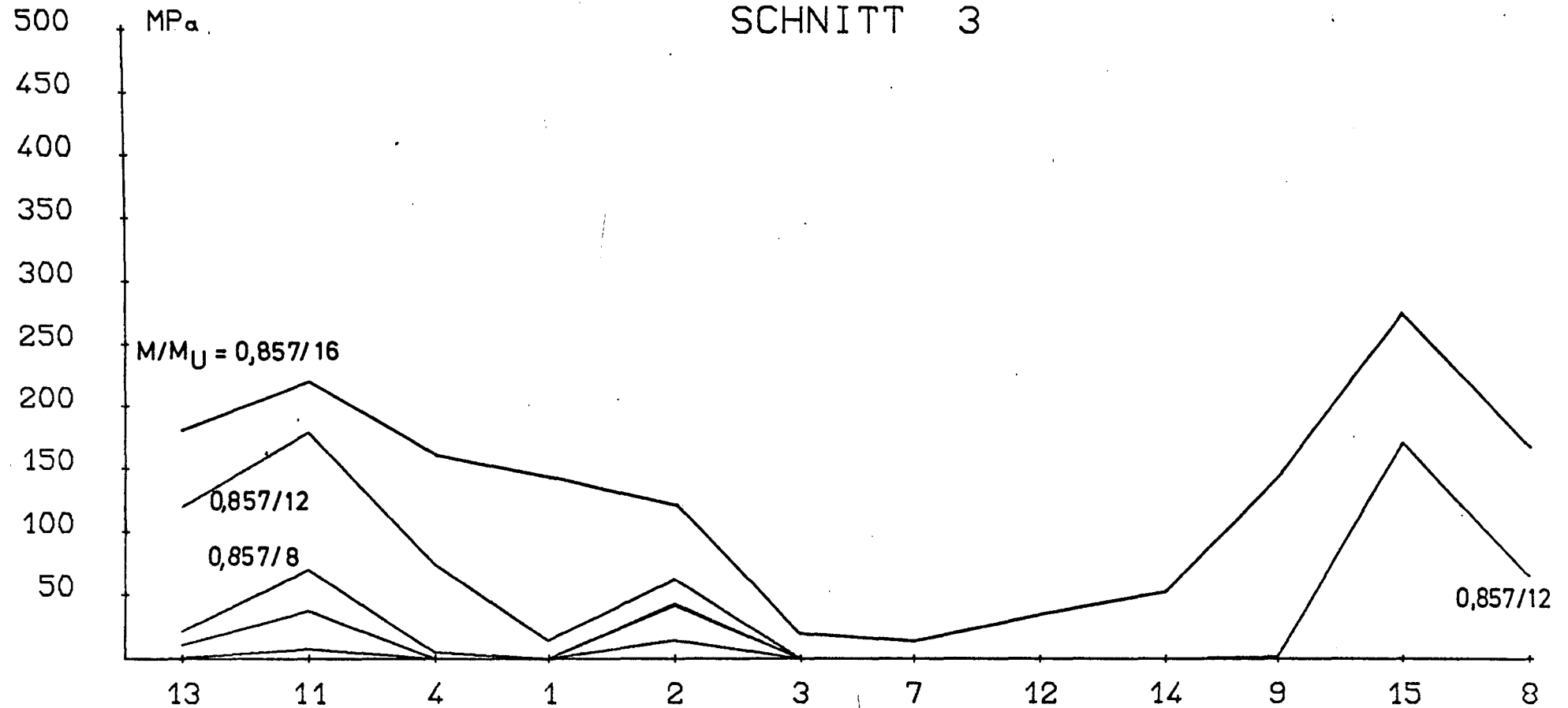
E

Bügelspannungen

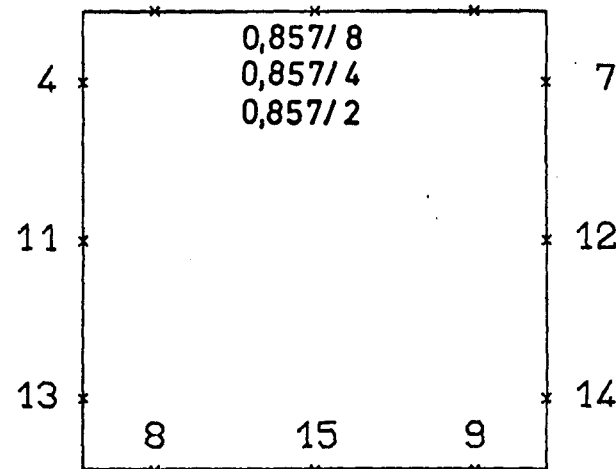
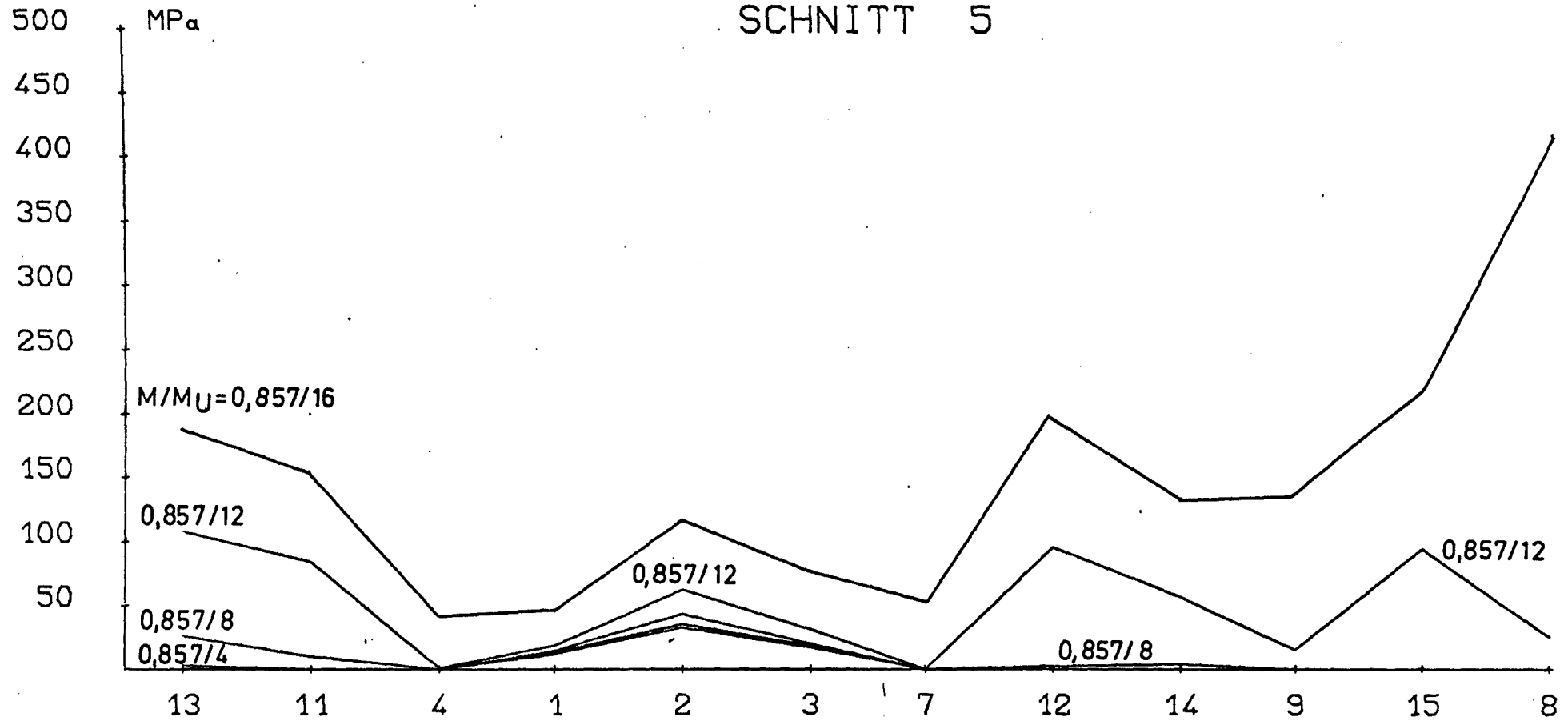
SCHNITT 1



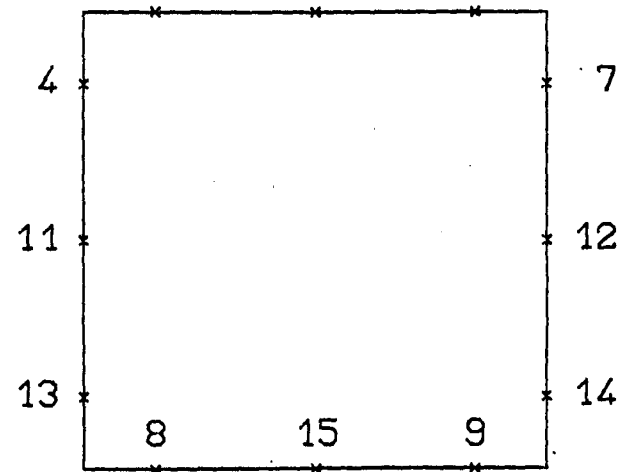
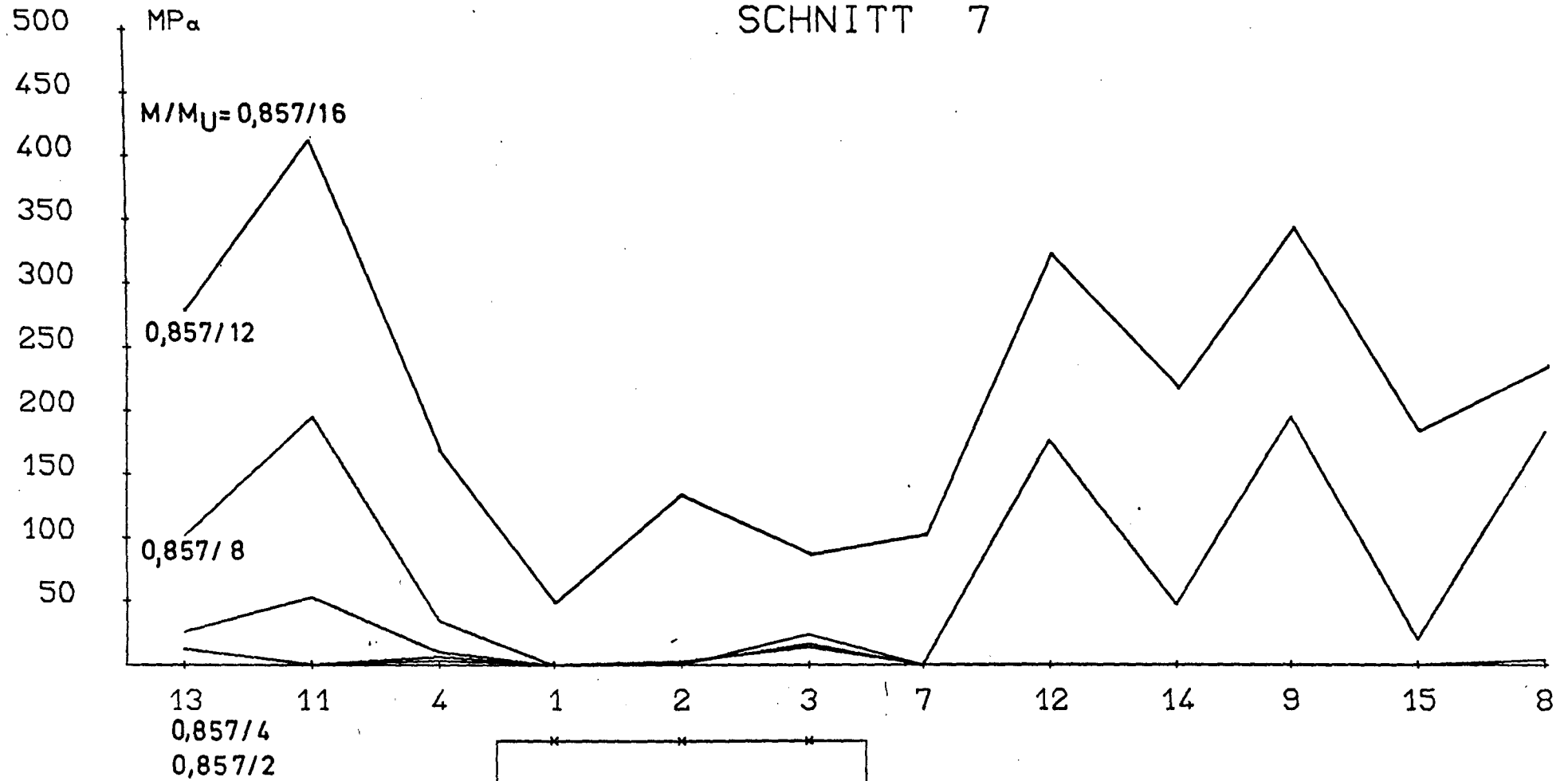
SCHNITT 3



SCHNITT 5

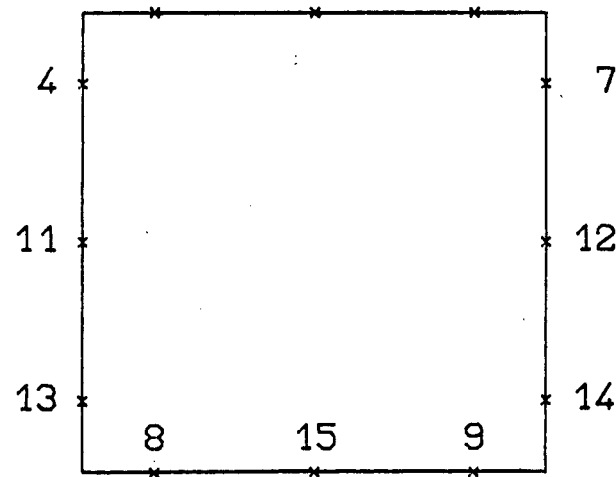
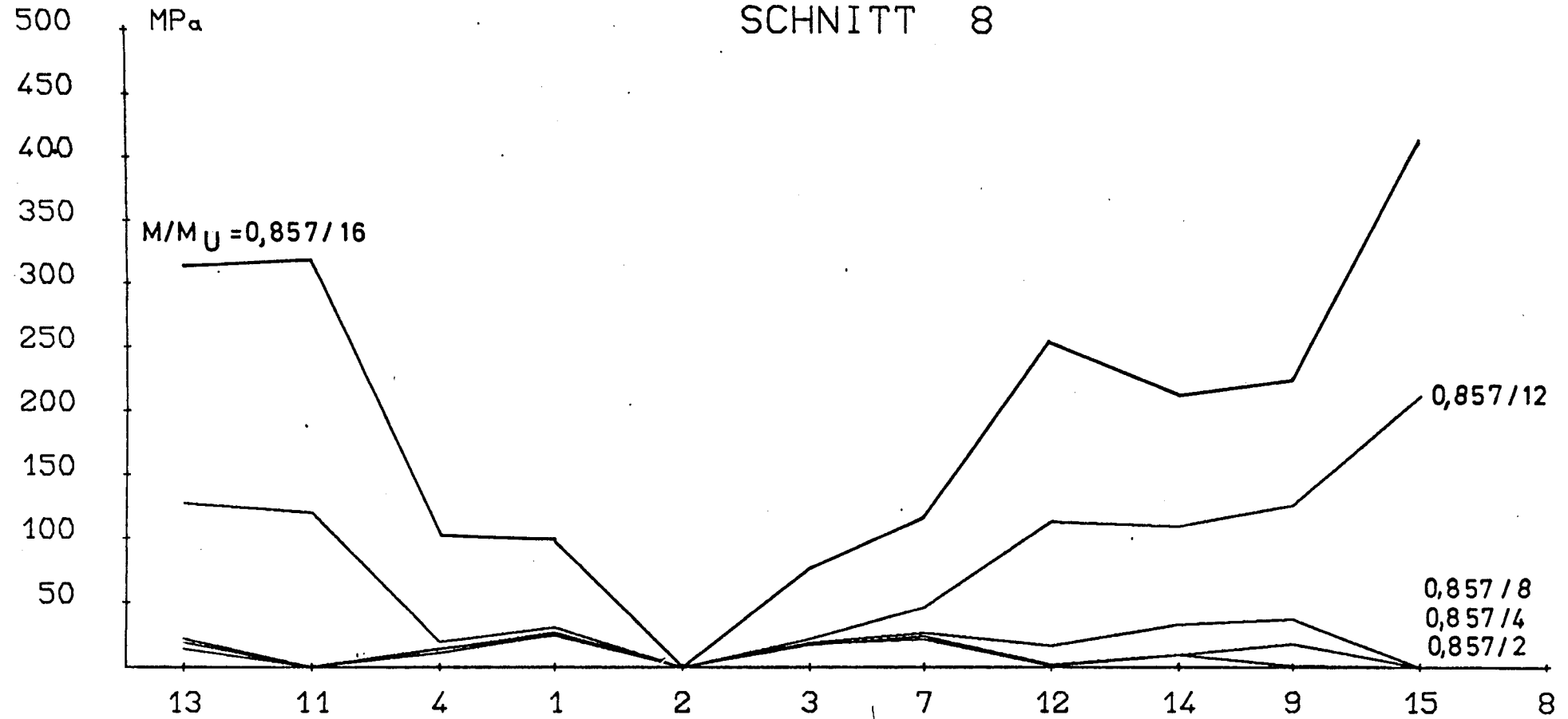


SCHNITT 7

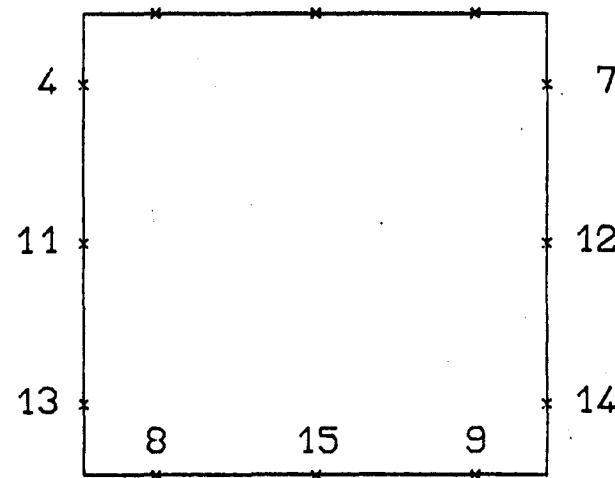
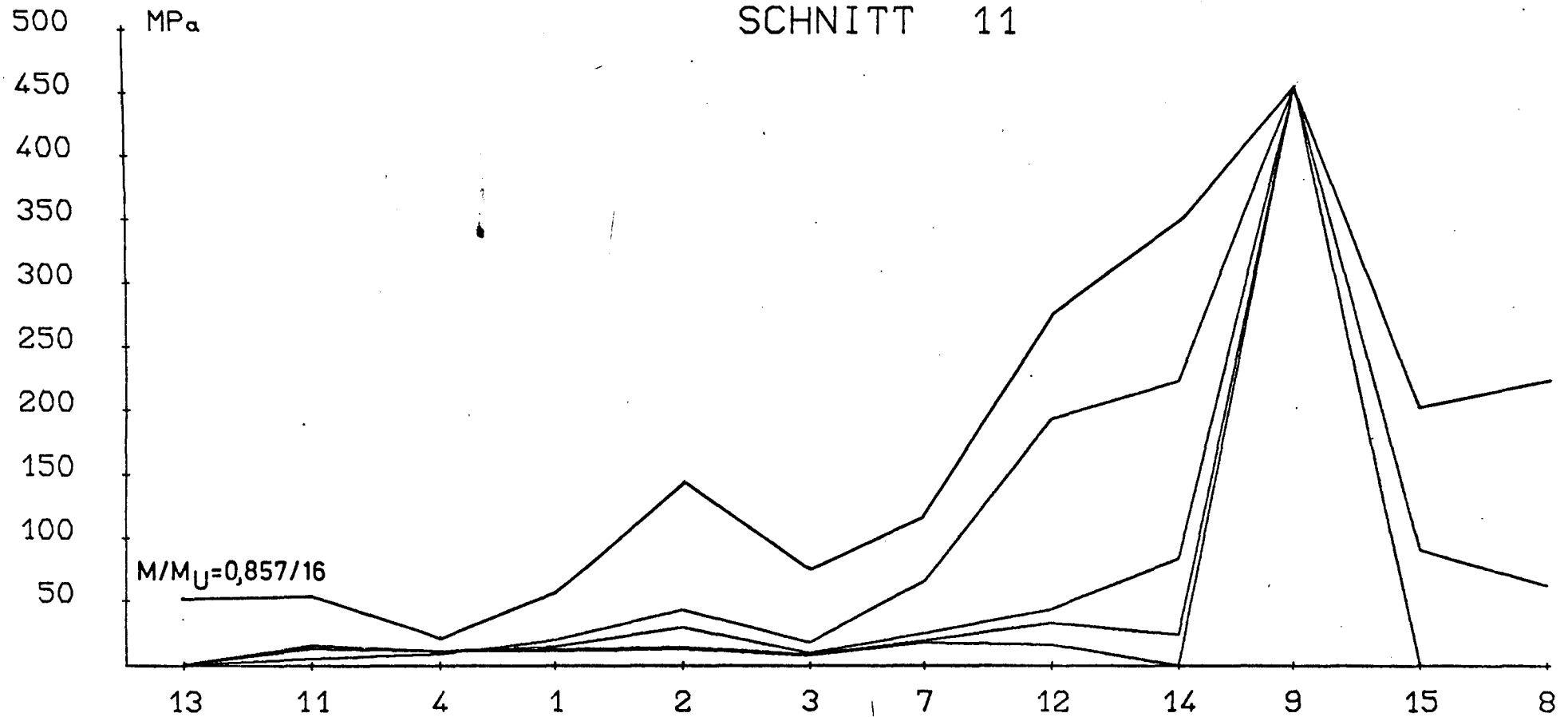


BUEGELSPANNUNGEN DES BALKENS SETMQ 1

SCHNITT 8

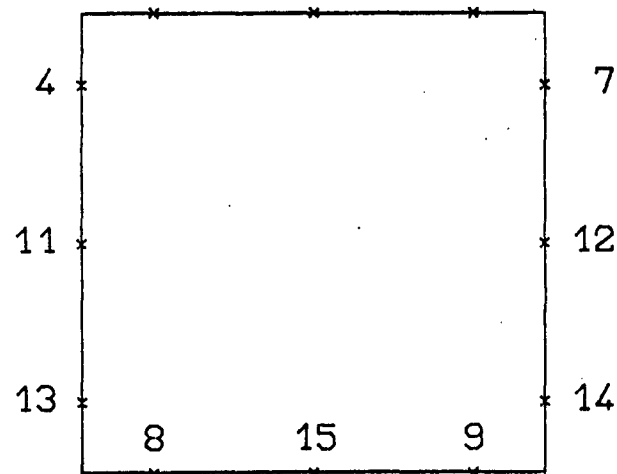
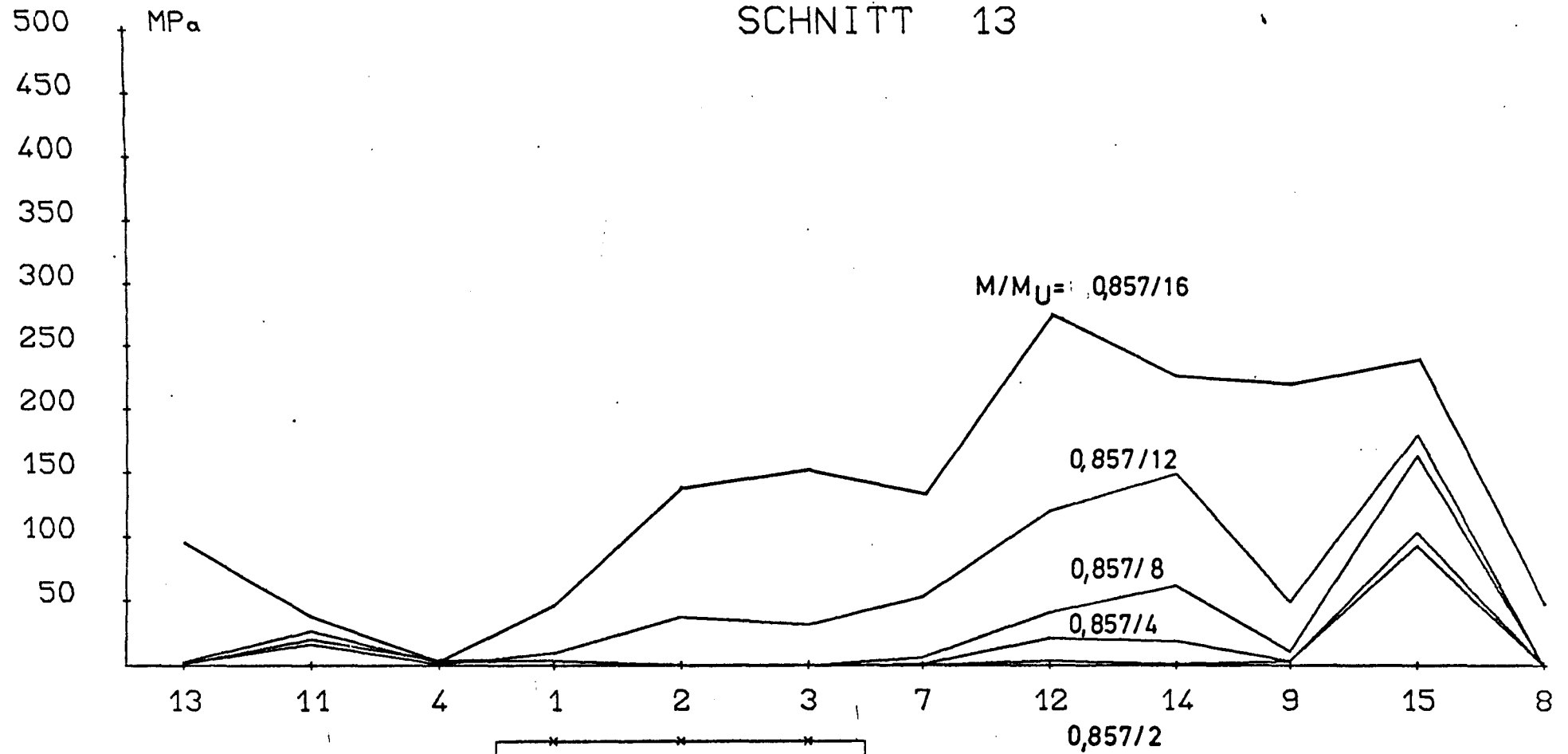


SCHNITT 11

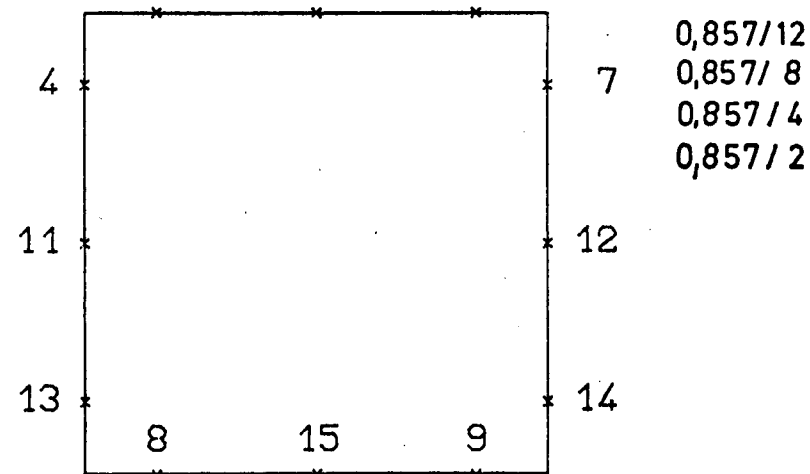
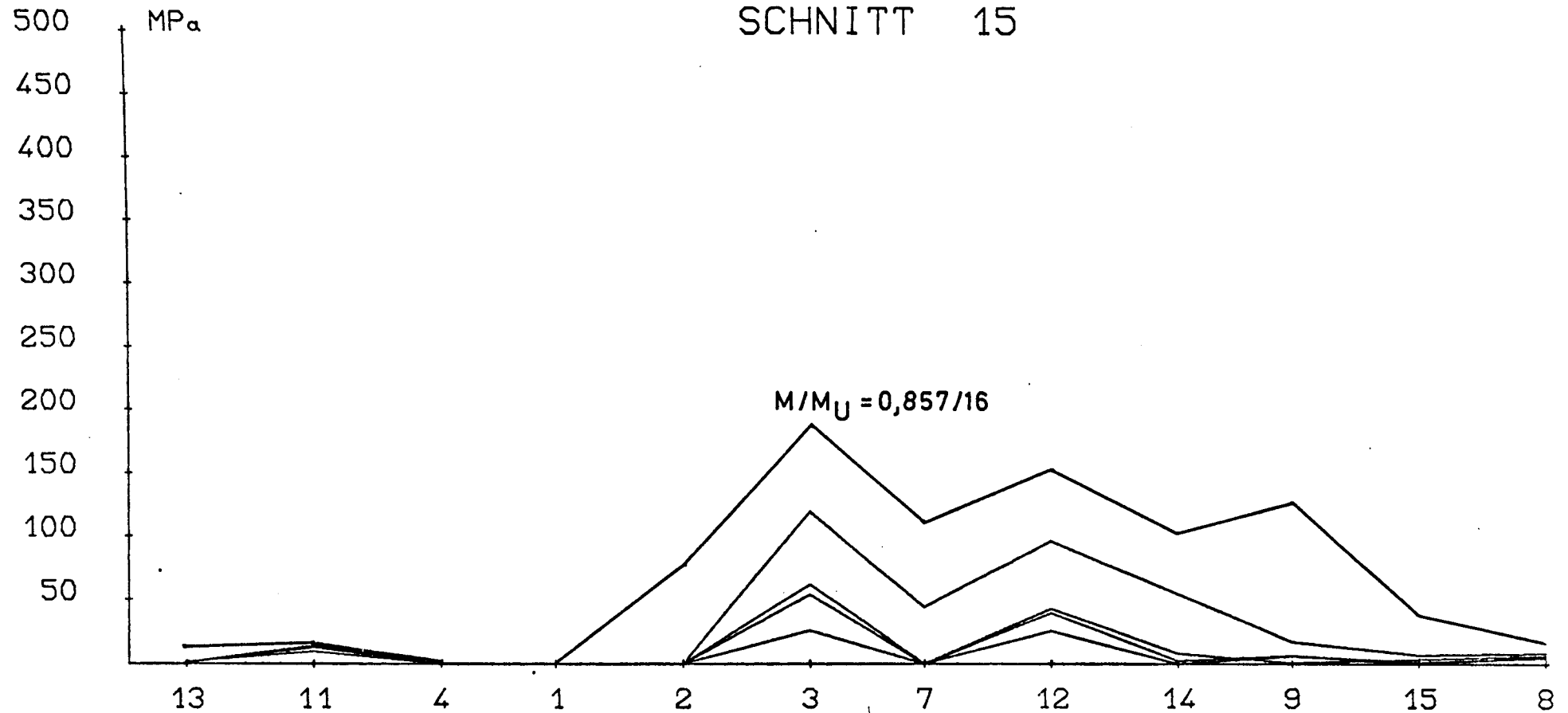


0,857/12
0,857/8
0,857/4
0,857/2

SCHNITT 13



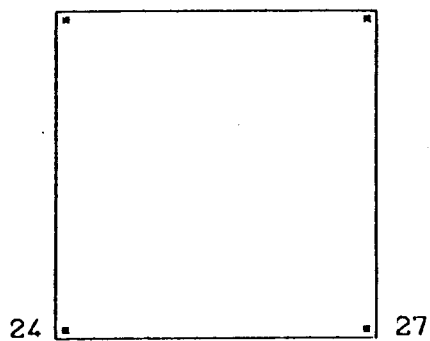
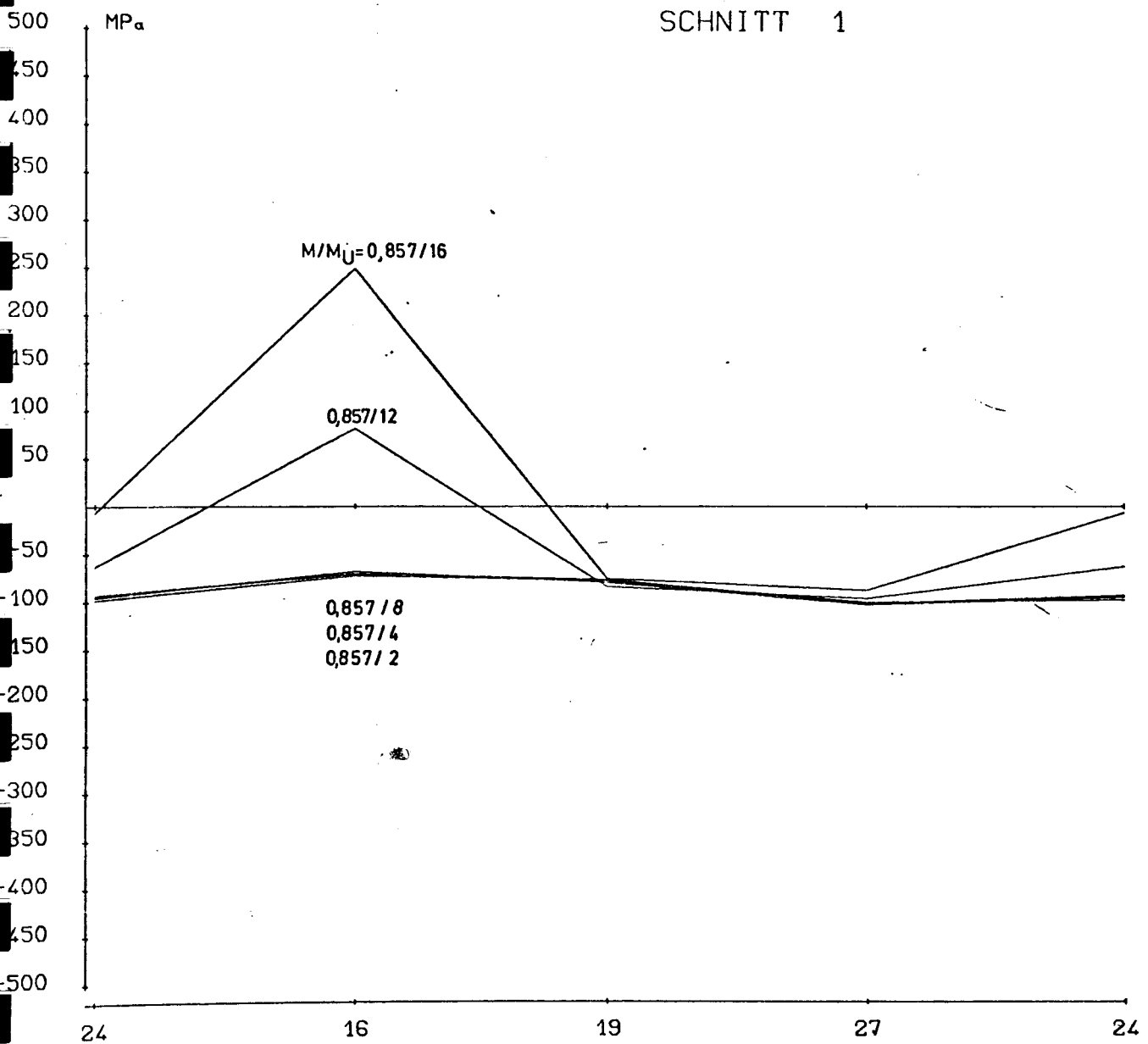
SCHNITT 15



F Längsstabspannungen in Abhängigkeit ihrer Lage im Querschnitt

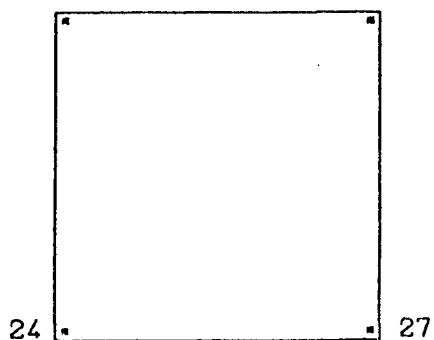
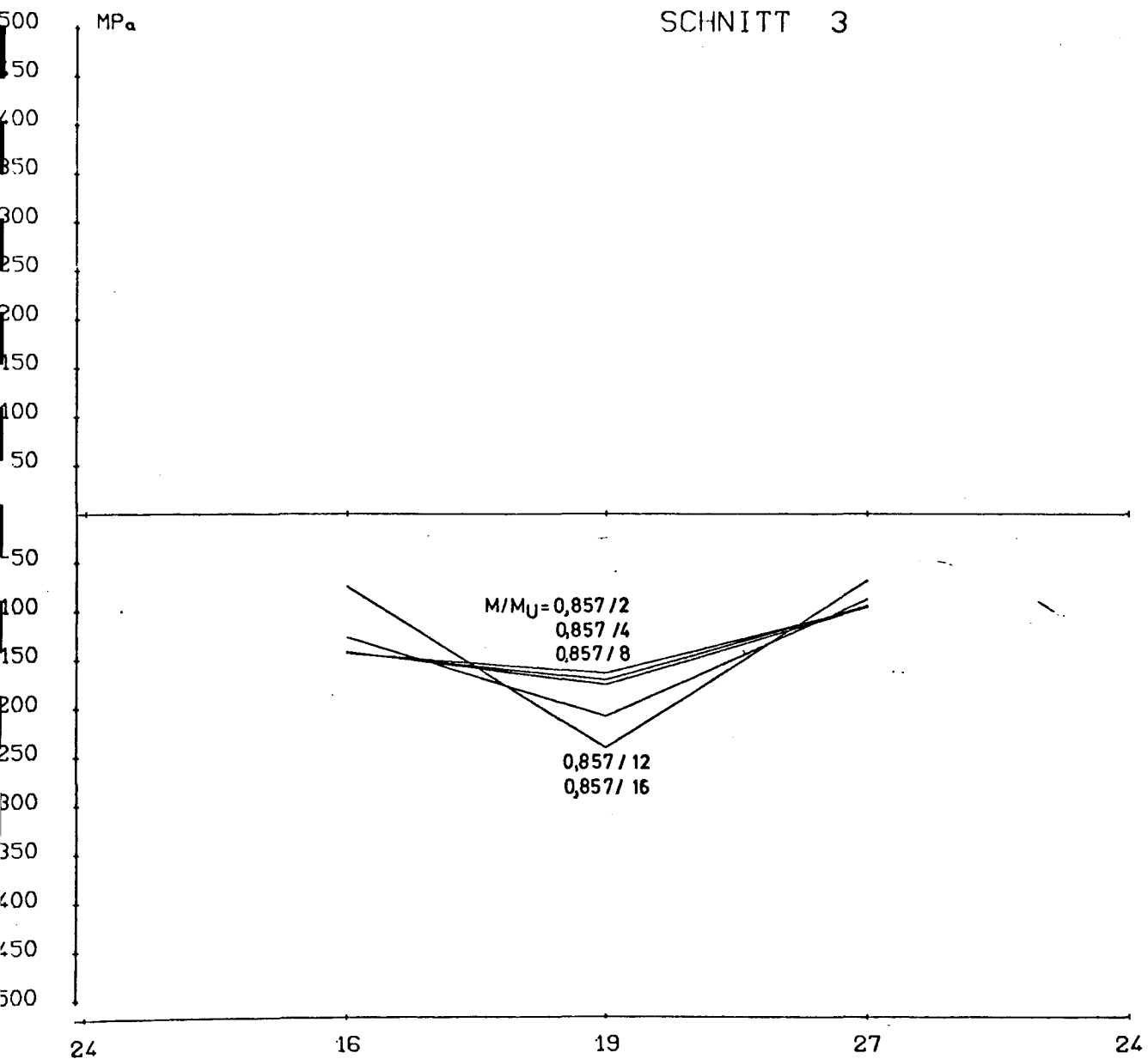
LAENGSTABSPANNUNGEN DES BALKENS SETMQ 1

SCHNITT 1



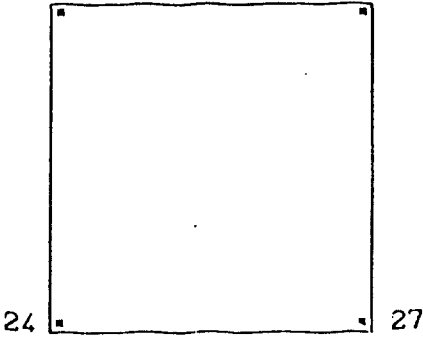
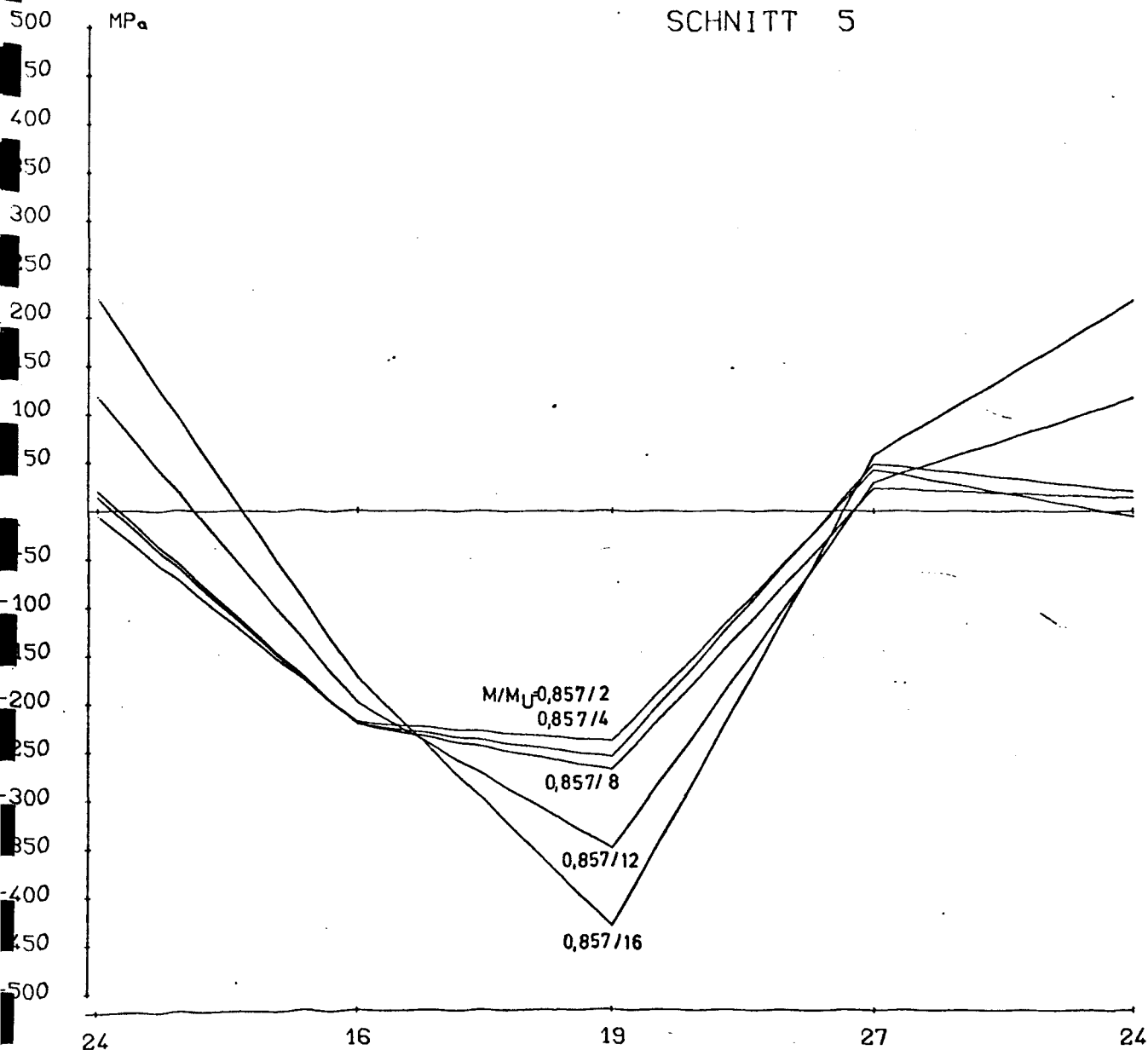
LAENGSTABSPANNUNGEN DES BALKENS SETMQ 1

SCHNITT 3



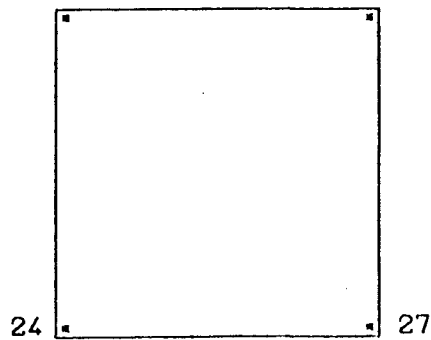
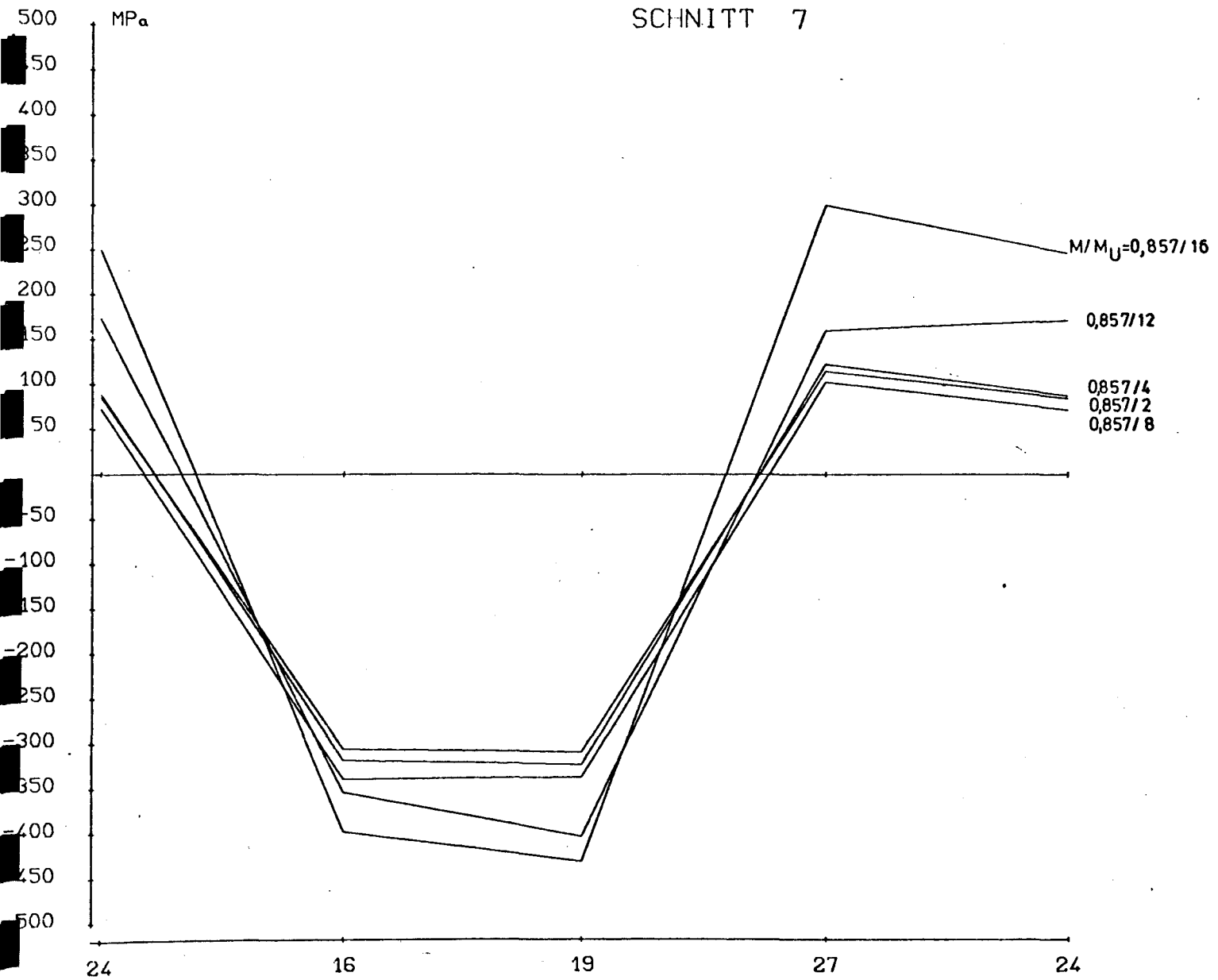
LAENGSSSTABSPANNUNGEN DES BALKENS SETMQ 1

SCHNITT 5



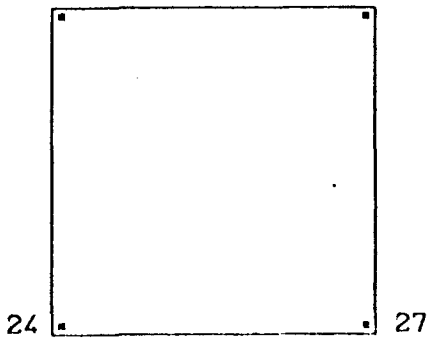
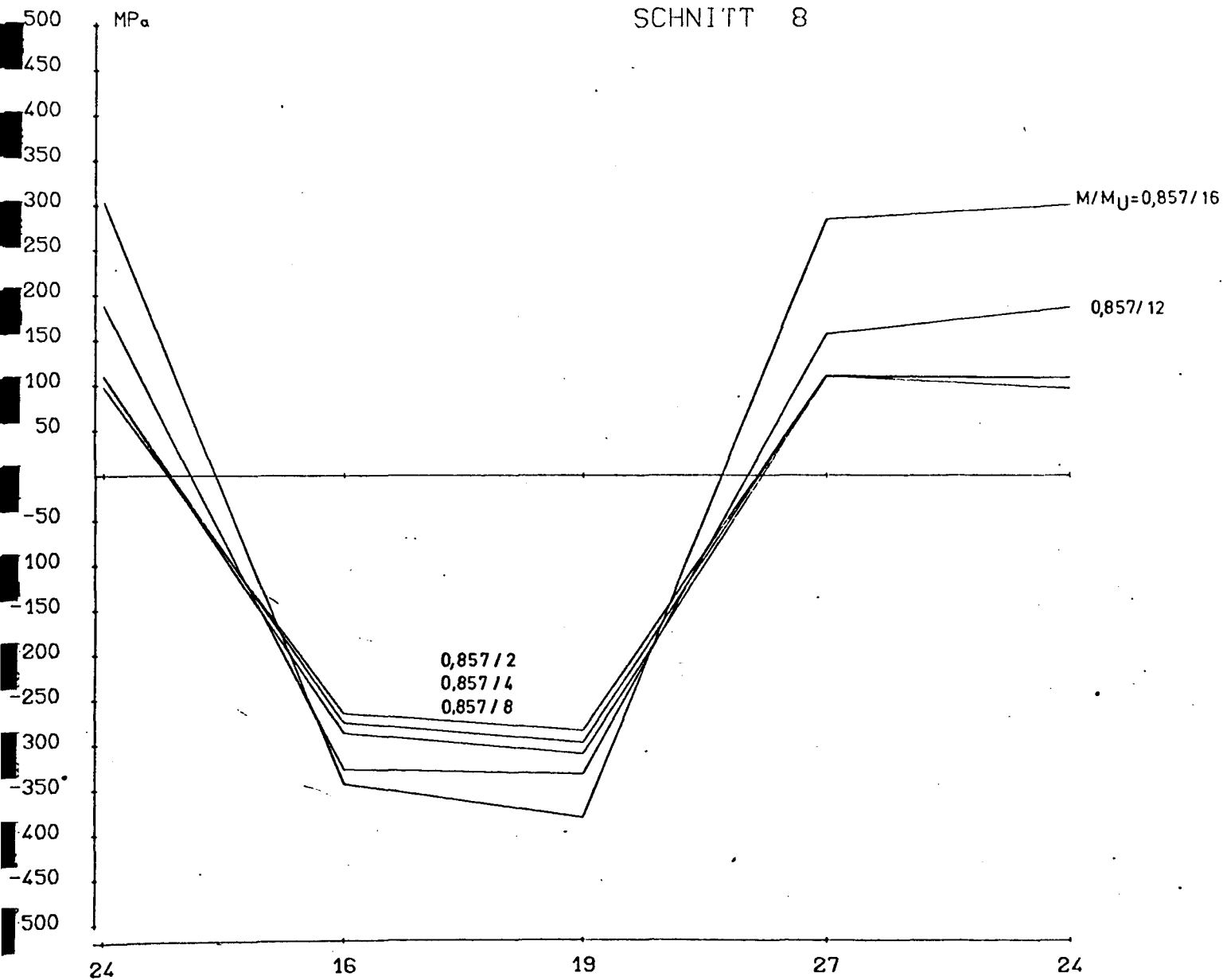
LAENGSSSTABSPANNUNGEN DES BALKENS SETMQ 1

SCHNITT 7



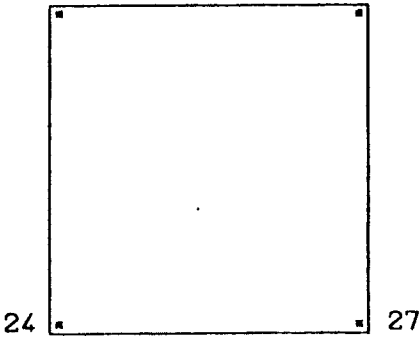
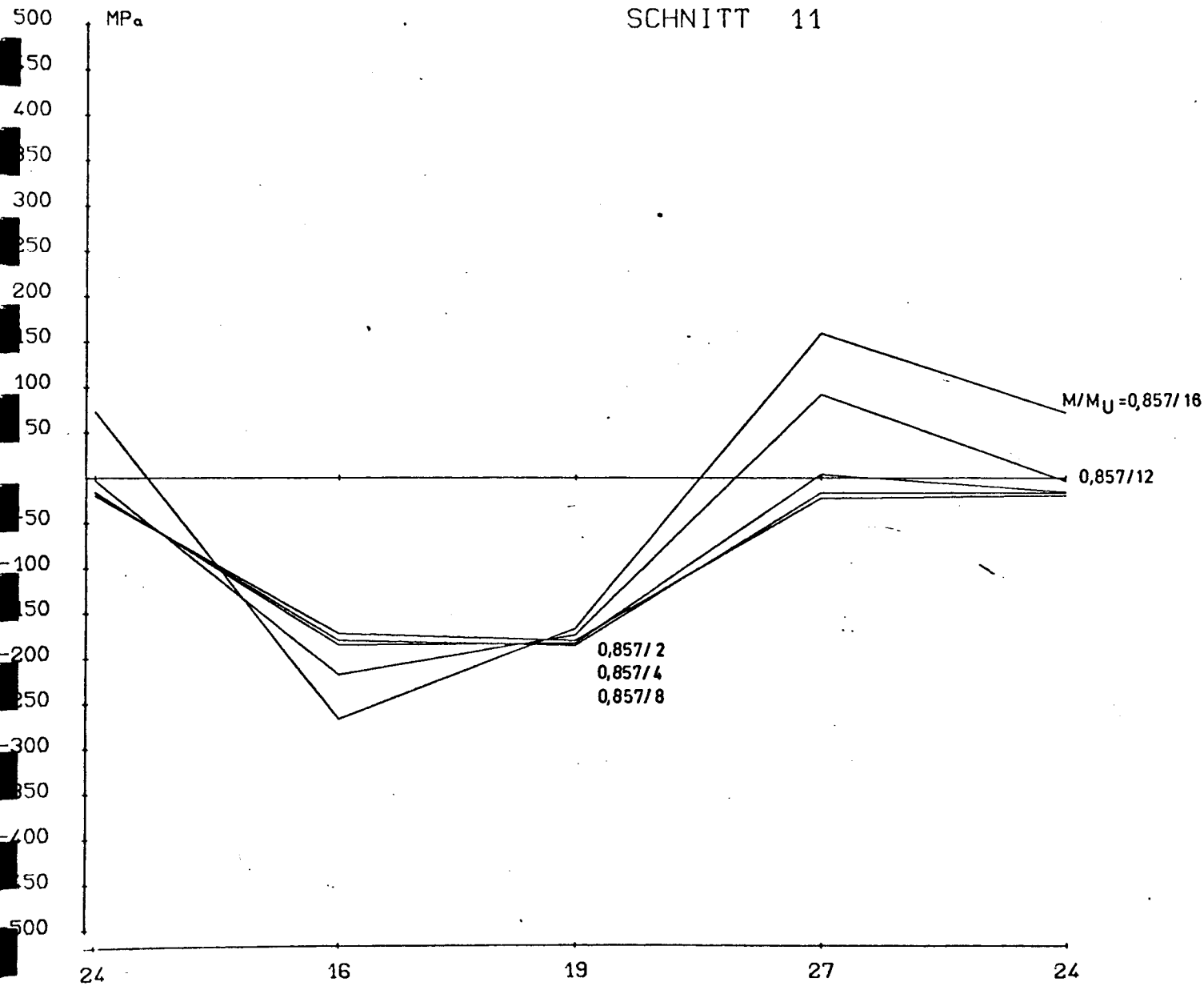
LAENGSTABSPANNUNGEN DES BALKENS SETMQ 1

SCHNITT 8



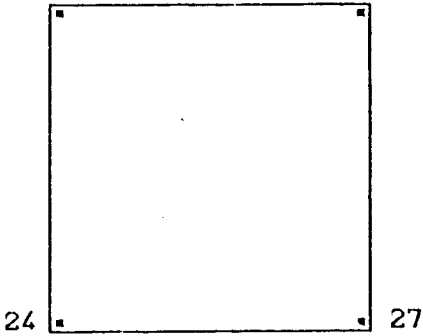
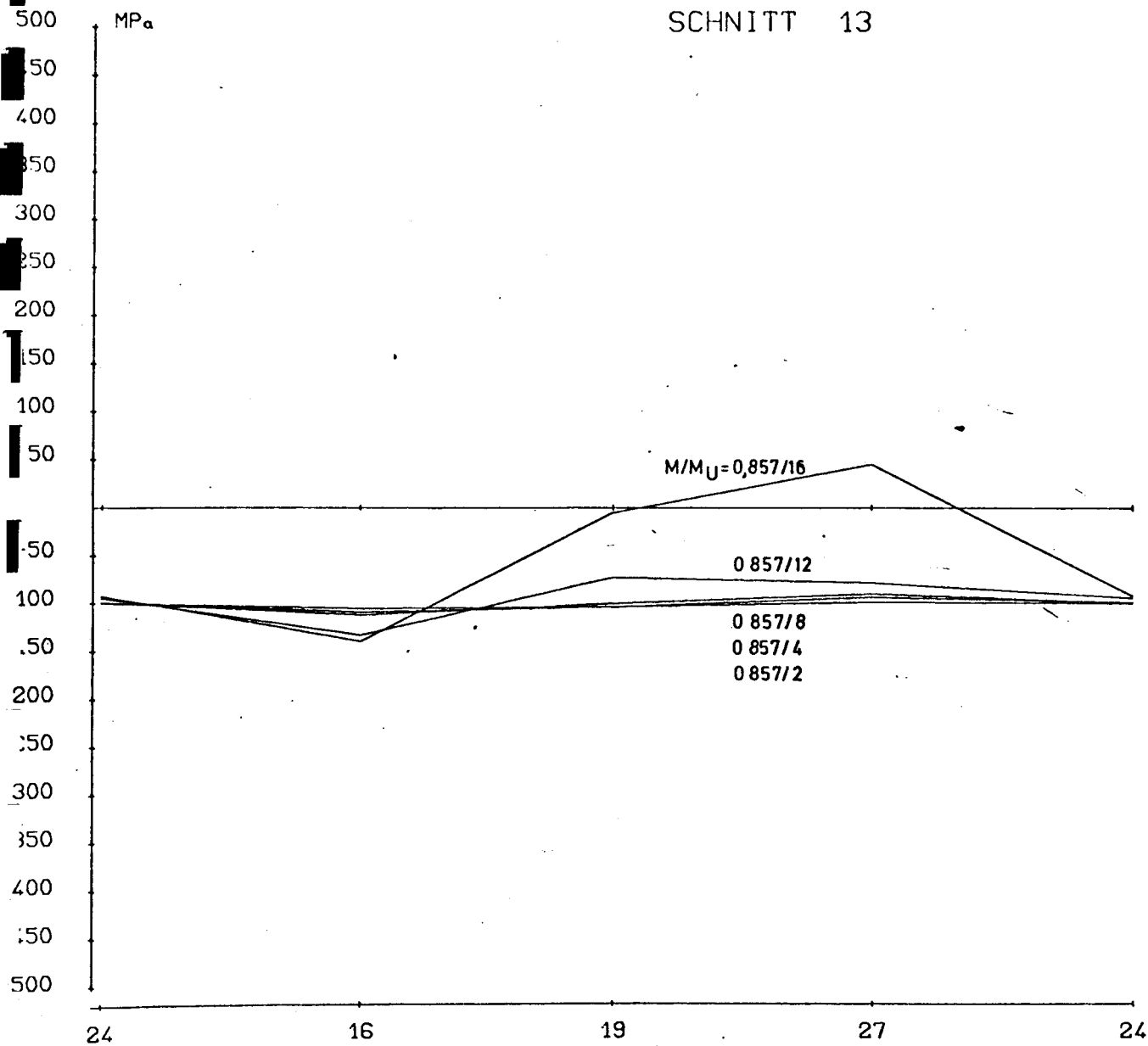
LAENGSTABSPANNUNGEN DES BALKENS SETMQ 1

SCHNITT 11



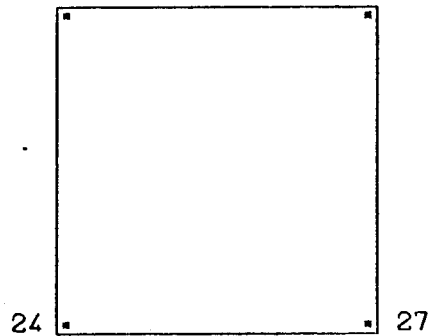
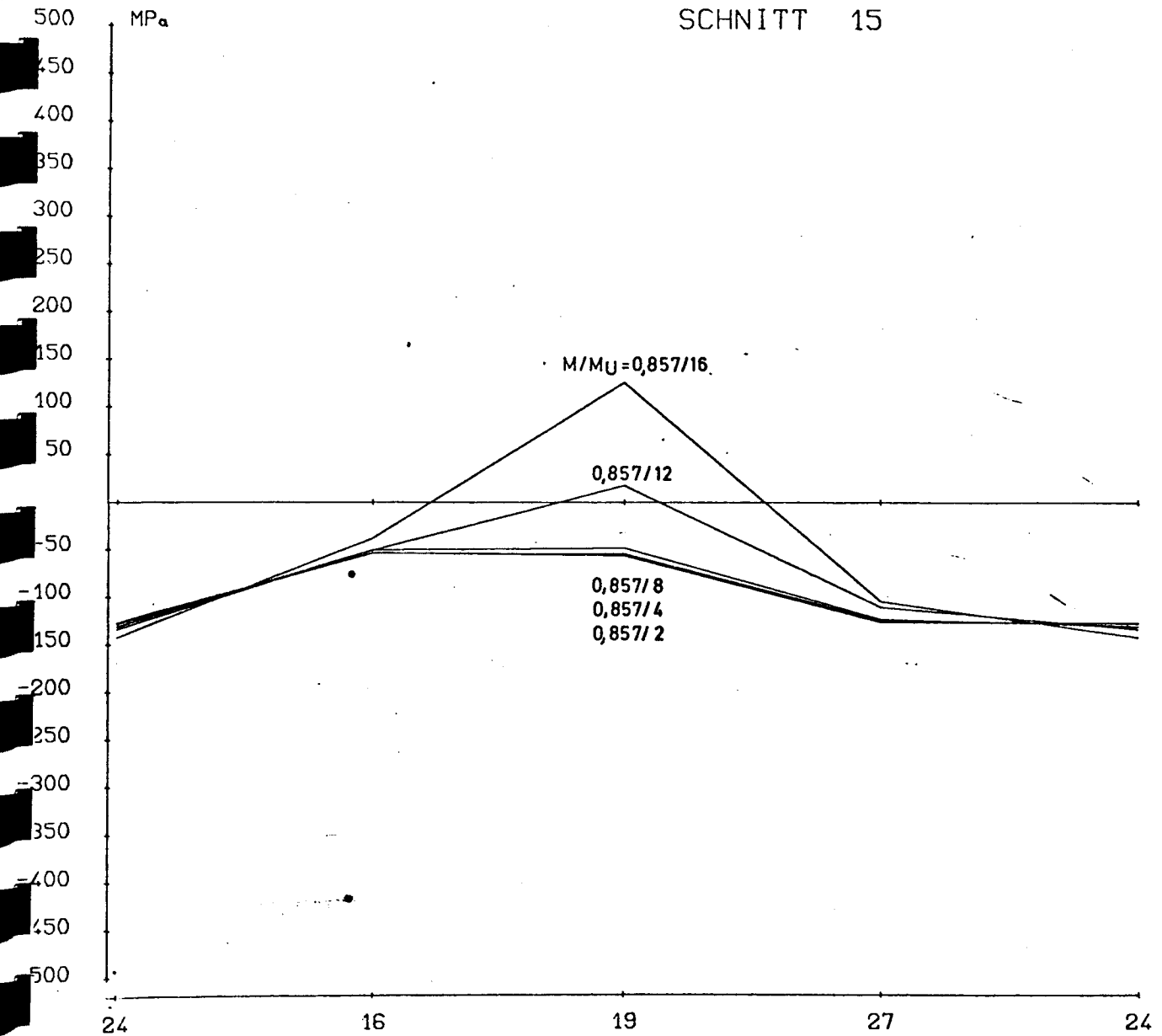
LAENGSSSTABSPANNUNGEN DES BALKENS SETMQ 1

SCHNITT 13



LAENGSSSTABSPANNUNGEN DES BALKENS SETMQ 1

SCHNITT 15



G

Betonranddehnungen (Tabellenform)

VERSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

ERMITTELTE BETONQUERDEHNUNGEN IN PROMILLE

BELASTUNGSGRAD M/MU

| SCHNITT MESSTELLE | | 0.229 | 0.343 | 0.571 | 0.629 | 0.743 | 0.857 | 0.857 | 0.857 | 0.857 | 0.400 | 0.400 | 0.000 | 0.257 |
|-------------------|----|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | | | | | | | ----- | ----- | ----- | ----- | ----- | ----- | ----- |
| | | | | | | | | 1 | 3 | 6 | 1 | 3 | 3 | 7 |
| 1 | 11 | -0.155 | 0.035 | 0.105 | 0.095 | 0.080 | 0.125 | 0.035 | -0.005 | 0.050 | 0.075 | -0.005 | 0.075 | -0.010 |
| 1 | 29 | 0.280 | 0.115 | 0.365 | 0.060 | 0.075 | 0.335 | -0.005 | 0.210 | 0.100 | 0.065 | 0.045 | 0.245 | 0.255 |
| 1 | 41 | 0.030 | 0.025 | 0.035 | -0.070 | 0.040 | 0.110 | 0.070 | 0.270 | 0.665 | 0.515 | 0.600 | 0.285 | 0.520 |
| 3 | 14 | 0.020 | 0.015 | 0.110 | 0.085 | 0.060 | 0.115 | 0.150 | 0.095 | 0.105 | 0.070 | 0.035 | 0.130 | 0.130 |
| 3 | 32 | -0.045 | 0.020 | 0.020 | -0.030 | -0.015 | 0.060 | 0.075 | -0.005 | -0.085 | 0.000 | -0.015 | 0.085 | 0.070 |
| 3 | 44 | -0.010 | 0.040 | 0.010 | -0.120 | 0.015 | 0.075 | 0.095 | 0.150 | 0.375 | 0.210 | 0.295 | 0.230 | 0.360 |
| 5 | 35 | -0.095 | -0.140 | 0.040 | -0.020 | -0.030 | 0.085 | 0.040 | -0.080 | 0.015 | -0.035 | 0.060 | -0.060 | 0.080 |
| 7 | 17 | 0.010 | 0.050 | 0.100 | 0.060 | 0.065 | 0.165 | 0.190 | 0.170 | 0.090 | 0.080 | 0.060 | 0.125 | 0.160 |
| 7 | 38 | -0.020 | 0.010 | 0.040 | -0.040 | -0.040 | 0.000 | 0.040 | -0.010 | -0.025 | 0.020 | -0.005 | 0.055 | 0.030 |
| 8 | 2 | -0.050 | -0.105 | -0.100 | 0.055 | -0.155 | 0.035 | -0.020 | 0.080 | -0.085 | -0.085 | -0.150 | 0.040 | 0.170 |
| 8 | 20 | -0.050 | 0.000 | 0.005 | -0.085 | -0.135 | -0.050 | -0.055 | -0.095 | -0.155 | -0.110 | -0.160 | -0.035 | -0.115 |
| 11 | 5 | -0.050 | 0.005 | -0.055 | 0.035 | 0.010 | 0.155 | -0.030 | 0.130 | 0.070 | 0.065 | 0.095 | 0.075 | 0.200 |
| 11 | 26 | -0.005 | 0.060 | 0.085 | 0.020 | 0.020 | 0.075 | 0.100 | 0.040 | 0.015 | -0.005 | -0.040 | 0.060 | 0.035 |
| 13 | 8 | -0.025 | 0.015 | 0.020 | -0.095 | -0.005 | 0.005 | -0.100 | 0.075 | 0.000 | -0.045 | -0.090 | 0.050 | 0.070 |
| 13 | 23 | 0.010 | 0.040 | 0.095 | 0.060 | 0.055 | 0.115 | 0.120 | 0.095 | 0.060 | 0.090 | 0.015 | 0.070 | 0.085 |

VERSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

ERMITTELTE BETONQUERDEHNUNGEN IN PROMILLE

BELASTUNGSGRAD M/MU

| SCHNITT MESSTELLE | | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
|-------------------|----|--------|--------|--------|--------|--------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | ----- | ----- | ----- | ----- | ----- | | | | | | | | |
| | | 9 | 11 | 13 | 15 | 16 | | | | | | | | |
| 1 | 11 | 0.000 | -0.110 | -0.080 | -0.265 | -0.215 | | | | | | | | |
| 1 | 29 | 0.355 | 0.310 | 0.155 | 0.140 | -0.050 | | | | | | | | |
| 1 | 41 | 0.665 | 1.060 | 1.250 | 1.295 | 1.230 | | | | | | | | |
| 3 | 14 | 0.120 | 0.140 | 0.340 | 0.455 | 0.480 | | | | | | | | |
| 3 | 32 | 0.005 | -0.010 | -0.005 | 0.105 | 0.130 | | | | | | | | |
| 3 | 44 | 0.330 | 0.725 | 1.270 | 1.540 | 1.355 | | | | | | | | |
| 5 | 35 | 0.025 | 0.260 | 0.465 | 0.825 | 0.885 | | | | | | | | |
| 7 | 17 | 0.140 | -0.930 | 0.005 | 0.035 | 0.070 | | | | | | | | |
| 7 | 38 | 0.020 | 0.910 | 2.050 | 2.570 | 2.640 | | | | | | | | |
| 8 | 2 | 0.020 | 0.095 | 0.680 | 0.965 | 1.030 | | | | | | | | |
| 8 | 20 | -0.205 | -0.250 | -0.400 | -0.400 | -0.420 | | | | | | | | |
| 11 | 5 | 0.145 | 0.045 | 0.100 | 0.165 | 0.355 | | | | | | | | |
| 11 | 26 | 0.000 | -0.010 | 0.180 | 0.490 | 0.565 | | | | | | | | |
| 13 | 8 | -0.020 | 0.015 | -0.030 | -0.040 | -0.095 | | | | | | | | |
| 13 | 23 | 0.085 | 0.135 | 0.365 | 0.480 | 0.430 | | | | | | | | |

ERMITTELTE BETONQUERDEHNUNGEN IN PROMILLE

BELASTUNGSGRAD M/MU

| SCHNITT MESSTELLE | | 0.000 | 0.229 | 0.343 | 0.571 | 0.629 | 0.743 | 0.857 | 0.857 | 0.857 | 0.857 | 0.400 | 0.400 | 0.00 |
|-------------------|----|--------|--------|--------|--------|--------|--------|--------|------------|------------|------------|------------|------------|------------|
| | | | | | | | | | ----- 1 | ----- 3 | ----- 6 | ----- 1 | ----- 3 | ----- 5 |
| 1 | 11 | 0.040 | -0.115 | 0.075 | 0.145 | 0.135 | 0.120 | 0.165 | 0.075 | 0.035 | 0.090 | 0.115 | 0.035 | 0.115 |
| 1 | 29 | -0.040 | 0.240 | 0.075 | 0.325 | 0.020 | 0.035 | 0.295 | -0.045 | 0.170 | 0.060 | 0.025 | 0.005 | 0.200 |
| 1 | 41 | 0.005 | 0.035 | 0.030 | 0.040 | -0.065 | 0.045 | 0.115 | 0.075 | 0.275 | 0.670 | 0.520 | 0.605 | 0.295 |
| 3 | 14 | -0.080 | -0.060 | -0.065 | 0.030 | 0.005 | -0.020 | 0.035 | 0.070 | 0.015 | 0.025 | -0.010 | -0.045 | 0.095 |
| 3 | 32 | 0.080 | 0.035 | 0.100 | 0.100 | 0.050 | 0.065 | 0.140 | 0.155 | 0.075 | -0.005 | 0.080 | 0.065 | 0.140 |
| 3 | 44 | 0.010 | 0.000 | 0.050 | 0.020 | -0.110 | 0.025 | 0.085 | 0.105 | 0.160 | 0.385 | 0.220 | 0.305 | 0.240 |
| 5 | 35 | 0.030 | -0.065 | -0.110 | 0.070 | 0.010 | 0.000 | 0.115 | 0.070 | -0.050 | 0.045 | -0.005 | 0.090 | -0.005 |
| 7 | 17 | -0.080 | -0.070 | -0.030 | 0.020 | -0.020 | -0.015 | 0.085 | 0.110 | 0.090 | 0.010 | 0.000 | -0.020 | 0.000 |
| 7 | 38 | 0.070 | 0.050 | 0.080 | 0.110 | 0.030 | 0.030 | 0.070 | 0.110 | 0.060 | 0.045 | 0.090 | 0.065 | 0.140 |
| 8 | 2 | -0.085 | -0.135 | -0.190 | -0.185 | -0.030 | -0.240 | -0.050 | -0.105 | -0.005 | -0.170 | -0.170 | -0.235 | -0.005 |
| 8 | 20 | -0.105 | -0.155 | -0.105 | -0.100 | -0.190 | -0.240 | -0.155 | -0.160 | -0.200 | -0.260 | -0.215 | -0.265 | -0.140 |
| 11 | 5 | -0.005 | -0.055 | 0.000 | -0.060 | 0.030 | 0.005 | 0.150 | -0.035 | 0.125 | 0.065 | 0.060 | 0.090 | 0.000 |
| 11 | 26 | -0.050 | -0.055 | 0.010 | 0.035 | -0.030 | -0.030 | 0.025 | 0.050 | -0.010 | -0.035 | -0.055 | -0.090 | 0.000 |
| 13 | 8 | 0.055 | 0.030 | 0.070 | 0.075 | -0.040 | 0.050 | 0.060 | -0.045 | 0.130 | 0.055 | 0.010 | -0.035 | 0.110 |
| 13 | 23 | -0.060 | -0.050 | -0.020 | 0.035 | 0.000 | -0.005 | 0.055 | 0.060 | 0.035 | 0.000 | 0.030 | -0.045 | 0.000 |

ERMITTELTE BETONQUERDEHNUNGEN IN PROMILLE

BELASTUNGSGRAD M/MU

| SCHNITT | MESSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
|---------|-----------|--------|--------|--------|--------|--------|--------|-------|-------|-------|-------|-------|-------|-------|
| | | 7 | 9 | 11 | 13 | 15 | 16 | | | | | | | |
| 1 | 11 | 0.030 | 0.040 | -0.070 | -0.040 | -0.225 | -0.175 | | | | | | | |
| 1 | 29 | 0.215 | 0.315 | 0.270 | 0.115 | 0.100 | -0.090 | | | | | | | |
| 1 | 41 | 0.525 | 0.670 | 1.065 | 1.255 | 1.300 | 1.235 | | | | | | | |
| 3 | 14 | 0.050 | 0.040 | 0.060 | 0.260 | 0.375 | 0.400 | | | | | | | |
| 3 | 32 | 0.150 | 0.085 | 0.070 | 0.075 | 0.185 | 0.210 | | | | | | | |
| 3 | 44 | 0.370 | 0.340 | 0.735 | 1.280 | 1.550 | 1.365 | | | | | | | |
| 5 | 35 | 0.110 | 0.055 | 0.290 | 0.495 | 0.855 | 0.915 | | | | | | | |
| 7 | 17 | 0.080 | 0.060 | -1.010 | -0.075 | -0.045 | -0.010 | | | | | | | |
| 7 | 38 | 0.100 | 0.090 | 0.980 | 2.120 | 2.640 | 2.710 | | | | | | | |
| 8 | 2 | 0.085 | -0.065 | 0.010 | 0.595 | 0.880 | 0.945 | | | | | | | |
| 8 | 20 | -0.220 | -0.310 | -0.355 | -0.505 | -0.505 | -0.525 | | | | | | | |
| 11 | 5 | 0.195 | 0.140 | 0.040 | 0.095 | 0.160 | 0.350 | | | | | | | |
| 11 | 26 | -0.015 | -0.050 | -0.060 | 0.130 | 0.440 | 0.515 | | | | | | | |
| 13 | 8 | 0.125 | 0.035 | 0.070 | 0.025 | 0.015 | -0.040 | | | | | | | |
| 13 | 23 | 0.025 | 0.025 | 0.075 | 0.305 | 0.420 | 0.370 | | | | | | | |

| | | | | | | | | | | | | | | |
|---------|-----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| SCHNITT | MESSTELLE | 0.229 | 0.343 | 0.571 | 0.629 | 0.743 | 0.857 | 0.857 | 0.857 | 0.857 | 0.400 | 0.400 | 0.000 | 0.857 |
|---------|-----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|

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ERMITTELTE BETONLAENGSDUEHNUNGEN IN PROMILLE

BELASTUNGSGRAD M/MU

| SNITT | MESSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
|-------|-----------|--------|--------|--------|--------|--------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | ----- | ----- | ----- | ----- | ----- | | | | | | | | |
| | | 9 | 11 | 13 | 15 | 16 | | | | | | | | |
| 1 | 12 | -0.155 | -0.100 | -0.195 | -0.180 | -0.215 | | | | | | | | |
| 1 | 30 | 0.260 | 0.040 | -0.145 | -0.060 | -0.115 | | | | | | | | |
| 1 | 42 | -0.130 | -0.185 | -0.085 | 0.020 | 0.040 | | | | | | | | |
| 3 | 15 | -0.540 | -0.530 | -0.420 | -0.430 | -0.475 | | | | | | | | |
| 3 | 33 | -0.150 | -0.210 | -0.240 | -0.185 | -0.230 | | | | | | | | |
| 3 | 45 | -0.005 | 0.085 | 0.180 | 0.275 | 0.275 | | | | | | | | |
| 5 | 36 | 0.005 | 0.100 | 0.035 | -0.040 | -0.080 | | | | | | | | |
| 7 | 18 | -1.350 | -1.480 | -1.660 | -1.900 | -2.015 | | | | | | | | |
| 7 | 39 | -0.015 | -0.025 | -0.300 | -0.380 | -0.495 | | | | | | | | |
| 8 | 3 | 0.100 | 0.200 | 0.775 | 1.245 | 1.410 | | | | | | | | |
| 8 | 21 | -1.130 | -1.305 | -1.375 | -1.430 | -1.490 | | | | | | | | |
| 11 | 6 | -0.145 | -0.110 | -0.130 | -0.095 | -0.165 | | | | | | | | |
| 11 | 27 | -0.665 | -0.675 | -0.655 | -0.690 | -0.785 | | | | | | | | |
| 13 | 9 | -0.110 | -0.115 | -0.155 | -0.145 | -0.245 | | | | | | | | |
| 13 | 24 | -0.300 | -0.335 | -0.230 | -0.135 | -0.180 | | | | | | | | |

ERMITTELTE BETONLAENGSDUEHNUNGEN IN PROMILLE

BELASTUNGSGRAD M/MU

| SCHNITT MESSTELLE | | 0.000 | 0.229 | 0.343 | 0.571 | 0.629 | 0.743 | 0.857 | 0.857 | 0.857 | 0.857 | 0.400 | 0.400 | 0.00 |
|-------------------|----|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|
| | | | | | | | | | 1 | 3 | 6 | 1 | 3 | |
| 1 | 12 | -0.095 | -0.225 | -0.150 | -0.140 | -0.250 | -0.280 | -0.250 | -0.200 | -0.255 | -0.285 | -0.175 | -0.215 | -0.00 |
| 1 | 30 | -0.590 | -0.595 | -0.485 | -0.395 | -0.370 | -0.490 | -0.340 | -0.260 | -0.400 | -0.465 | -0.550 | -0.515 | -0.39 |
| 1 | 42 | -0.365 | -0.375 | -0.345 | -0.340 | -0.400 | -0.415 | -0.400 | -0.335 | -0.425 | -0.510 | -0.430 | -0.500 | -0.39 |
| 3 | 15 | -0.095 | -0.220 | -0.275 | -0.250 | -0.470 | -0.555 | -0.620 | -0.565 | -0.640 | -0.655 | -0.420 | -0.445 | -0.12 |
| 3 | 33 | -0.515 | -0.535 | -0.480 | -0.485 | -0.560 | -0.560 | -0.515 | -0.540 | -0.610 | -0.650 | -0.635 | -0.660 | -0.53 |
| 3 | 45 | -0.550 | -0.510 | -0.550 | -0.545 | -0.620 | -0.635 | -0.565 | -0.565 | -0.645 | -0.585 | -0.545 | -0.515 | -0.49 |
| 5 | 36 | -0.500 | -0.535 | -0.505 | -0.445 | -0.505 | -0.570 | -0.395 | -0.440 | -0.515 | -0.480 | -0.590 | -0.635 | -0.50 |
| 7 | 18 | -0.200 | -0.440 | -0.520 | -0.585 | -0.870 | -1.060 | -1.225 | -1.325 | -1.405 | -1.575 | -1.020 | -1.080 | -0.41 |
| 7 | 39 | -0.400 | -0.450 | -0.455 | -0.375 | -0.450 | -0.450 | -0.405 | -0.370 | -0.435 | -0.440 | -0.525 | -0.540 | -0.41 |
| 8 | 3 | -0.440 | -0.495 | -0.440 | -0.490 | -0.475 | -0.505 | -0.415 | -0.395 | -0.435 | -0.300 | -0.445 | -0.505 | -0.48 |
| 8 | 21 | -0.230 | -0.410 | -0.460 | -0.410 | -0.740 | -0.975 | -1.050 | -1.150 | -1.225 | -1.370 | -0.875 | -0.920 | -0.41 |
| 11 | 6 | -0.565 | -0.600 | -0.560 | -0.565 | -0.610 | -0.655 | -0.635 | -0.560 | -0.675 | -0.680 | -0.675 | -0.685 | -0.55 |
| 11 | 27 | -0.160 | -0.330 | -0.395 | -0.455 | -0.655 | -0.740 | -0.725 | -0.725 | -0.795 | -0.865 | -0.615 | -0.615 | -0.24 |
| 13 | 9 | -0.450 | -0.445 | -0.480 | -0.435 | -0.520 | -0.495 | -0.450 | -0.430 | -0.545 | -0.515 | -0.485 | -0.525 | -0.45 |
| 13 | 24 | -0.085 | -0.205 | -0.215 | -0.220 | -0.340 | -0.385 | -0.345 | -0.375 | -0.425 | -0.410 | -0.285 | -0.320 | -0.10 |

VERSUCHSBALKEN SETMQ1 GEPRUEFT AM 19. 5. 1978

ERMITTELTE BETONLAENGSDUEHNUNGEN IN PROMILLE

BELASTUNGSGRAD M/MU

| SCHNITT | MESSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
|---------|-----------|--------|--------|--------|--------|--------|--------|-------|-------|-------|-------|-------|-------|-------|
| | | 7 | 9 | 11 | 13 | 15 | 16 | | | | | | | |
| 1 | 12 | -0.235 | -0.250 | -0.195 | -0.290 | -0.275 | -0.310 | | | | | | | |
| 1 | 30 | -0.230 | -0.330 | -0.550 | -0.735 | -0.650 | -0.705 | | | | | | | |
| 1 | 42 | -0.505 | -0.495 | -0.550 | -0.450 | -0.305 | -0.325 | | | | | | | |
| 3 | 15 | -0.020 | -0.635 | -0.625 | -0.515 | -0.525 | -0.570 | | | | | | | |
| 3 | 33 | -0.580 | -0.665 | -0.725 | -0.755 | -0.700 | -0.745 | | | | | | | |
| 3 | 45 | -0.020 | -0.555 | -0.465 | -0.370 | -0.275 | -0.275 | | | | | | | |
| 5 | 36 | -0.470 | -0.495 | -0.400 | -0.465 | -0.540 | -0.580 | | | | | | | |
| 7 | 18 | -1.465 | -1.550 | -1.680 | -1.860 | -2.100 | -2.215 | | | | | | | |
| 7 | 39 | -0.360 | -0.415 | -0.425 | -0.700 | -0.780 | -0.895 | | | | | | | |
| 8 | 3 | -0.385 | -0.340 | -0.240 | 0.335 | 0.805 | 0.970 | | | | | | | |
| 8 | 21 | -1.275 | -1.360 | -1.535 | -1.605 | -1.660 | -1.720 | | | | | | | |
| 11 | 6 | -0.060 | -0.710 | -0.675 | -0.695 | -0.660 | -0.730 | | | | | | | |
| 11 | 27 | -0.795 | -0.825 | -0.835 | -0.815 | -0.850 | -0.945 | | | | | | | |
| 13 | 9 | -0.540 | -0.560 | -0.565 | -0.605 | -0.595 | -0.695 | | | | | | | |
| 13 | 24 | -0.395 | -0.385 | -0.420 | -0.315 | -0.220 | -0.265 | | | | | | | |

ERMITTELTE BETONTRAJEKTORIENDEHNUNG IN PROMILLE

BELASTUNGSGRAD M/MU

| SCHNITT MESSTELLE | | 0.229 | 0.343 | 0.571 | 0.629 | 0.743 | 0.857 | 0.857 | 0.857 | 0.857 | 0.400 | 0.400 | 0.000 | 0.857 |
|-------------------|----|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | | | | | | | ----- | ----- | ----- | ----- | ----- | ----- | ----- |
| | | | | | | | | 1 | 3 | 6 | 1 | 3 | 3 | 7 |
| 1 | 10 | -0.090 | -0.010 | 0.015 | -0.085 | -0.100 | -0.050 | -0.010 | -0.105 | -0.180 | -0.290 | -0.335 | -0.035 | -0.105 |
| 1 | 28 | 0.030 | 0.075 | 0.230 | 0.300 | 0.205 | 0.345 | 0.350 | 0.280 | 0.185 | 0.075 | 0.005 | 0.085 | 0.440 |
| 1 | 47 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.175 |
| 1 | 40 | -0.010 | -0.005 | 0.055 | -0.050 | -0.130 | -0.105 | -0.170 | -0.245 | -0.440 | -0.350 | -0.485 | -0.085 | -0.380 |
| 2 | 48 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.140 |
| 3 | 13 | -0.080 | -0.055 | -0.055 | -0.140 | -0.195 | -0.160 | -0.120 | -0.245 | -0.365 | -0.265 | -0.325 | 0.000 | -0.230 |
| 3 | 31 | 0.005 | 0.080 | 0.125 | 0.080 | 0.120 | 0.235 | 0.210 | 0.140 | 0.030 | -0.055 | -0.130 | 0.015 | 0.195 |
| 3 | 49 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.180 |
| 3 | 43 | -0.040 | -0.055 | -0.055 | -0.125 | -0.150 | -0.150 | -0.125 | -0.195 | -0.395 | -0.315 | -0.430 | -0.085 | -0.280 |
| 4 | 50 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.235 |
| 5 | 34 | -0.015 | 0.010 | 0.140 | 0.070 | 0.070 | 0.230 | 0.170 | 0.005 | -0.170 | -0.260 | -0.215 | -0.035 | 0.110 |
| 5 | 51 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.260 |
| 5 | 46 | -0.100 | -0.130 | -0.140 | -0.135 | -0.105 | 0.015 | -0.115 | -0.155 | -0.240 | -0.285 | -0.320 | -0.160 | -0.130 |
| 7 | 16 | -0.095 | -0.125 | -0.115 | -0.280 | -0.405 | -0.445 | -0.465 | -0.590 | -0.760 | -0.510 | -0.610 | -0.115 | -0.595 |
| 7 | 37 | -0.010 | -0.020 | 0.050 | -0.010 | -0.040 | 0.050 | 0.025 | -0.095 | -0.105 | -0.150 | -0.185 | -0.030 | -0.030 |
| 7 | 53 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.140 |
| 7 | 60 | -0.005 | 0.005 | 0.065 | -0.010 | -0.055 | 0.050 | 0.080 | -0.060 | -0.160 | -0.200 | -0.245 | -0.080 | 0.000 |
| 8 | 54 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.200 |
| 8 | 59 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.140 |
| 8 | 1 | 0.010 | -0.060 | 0.030 | -0.040 | -0.080 | 0.040 | -0.025 | 0.005 | -0.190 | -0.230 | -0.300 | -0.080 | 0.010 |
| 8 | 19 | -0.130 | -0.170 | -0.150 | -0.365 | -0.485 | -0.520 | -0.515 | -0.670 | -0.905 | -0.635 | -0.680 | -0.230 | -0.700 |
| 8 | 61 | -0.005 | 0.005 | 0.075 | -0.030 | -0.010 | 0.065 | 0.095 | -0.035 | -0.115 | -0.155 | -0.200 | -0.035 | 0.035 |
| 10 | 56 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.030 |
| 11 | 57 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.020 |
| 11 | 4 | 0.000 | 0.010 | 0.070 | 0.075 | 0.110 | 0.135 | 0.225 | 0.110 | 0.065 | -0.055 | -0.055 | 0.045 | 0.185 |
| 11 | 25 | -0.105 | -0.140 | -0.120 | -0.255 | -0.315 | -0.280 | -0.275 | -0.370 | -0.515 | -0.390 | -0.465 | -0.065 | -0.405 |
| 11 | 62 | 0.030 | -0.040 | 0.035 | -0.075 | -0.140 | -0.120 | -0.140 | -0.250 | -0.295 | -0.195 | -0.245 | -0.070 | -0.185 |
| 12 | 58 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.180 |
| 13 | 55 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.130 |
| 13 | 7 | 0.020 | 0.070 | 0.080 | 0.065 | 0.110 | 0.185 | 0.250 | 0.145 | 0.045 | -0.055 | -0.145 | 0.030 | 0.175 |
| 13 | 22 | 0.000 | -0.005 | -0.015 | -0.090 | -0.075 | -0.065 | -0.045 | -0.155 | -0.270 | -0.120 | -0.235 | 0.040 | -0.155 |
| 13 | 63 | -0.070 | -0.055 | -0.020 | -0.140 | -0.185 | -0.170 | -0.135 | -0.285 | -0.425 | -0.335 | -0.375 | -0.110 | -0.315 |
| 13 | 52 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

 ERMITTELTE BETONTRAJEKTORIENDEHNUNG IN PROMILLE

BELASTUNGSGRAD M/MU

| SCHNITT | MESSTELLE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0. |
|---------|-----------|--------|--------|--------|--------|--------|--------|-------|-------|-------|-------|-------|-------|----|
| | | ----- | ----- | ----- | ----- | ----- | ----- | | | | | | | |
| | | 7 | 9 | 11 | 13 | 15 | 16 | | | | | | | |
| 1 | 10 | -0.075 | -0.185 | -0.270 | -0.440 | -0.590 | -0.690 | | | | | | | |
| 1 | 28 | 0.310 | 0.175 | -0.070 | -0.375 | -0.480 | -0.625 | | | | | | | |
| 1 | 47 | -0.175 | -0.255 | -0.460 | -0.430 | -0.595 | -0.710 | | | | | | | |
| 1 | 40 | -0.645 | -0.760 | -0.850 | -1.110 | -1.330 | -1.490 | | | | | | | |
| 2 | 48 | -0.140 | -0.225 | -0.370 | -0.520 | -0.655 | -0.815 | | | | | | | |
| 3 | 13 | -0.295 | -0.365 | -0.480 | -0.630 | -0.740 | -0.810 | | | | | | | |
| 3 | 31 | -0.015 | -0.125 | -0.315 | -0.530 | -0.600 | -0.665 | | | | | | | |
| 3 | 49 | -0.180 | -0.370 | -0.595 | -0.845 | -0.960 | -1.125 | | | | | | | |
| 3 | 43 | -0.560 | -0.705 | -0.870 | -0.995 | -1.055 | -1.175 | | | | | | | |
| 4 | 50 | -0.235 | -0.360 | -0.580 | -0.975 | -1.245 | -1.345 | | | | | | | |
| 5 | 34 | -0.140 | -0.315 | -0.565 | -1.015 | -1.270 | -1.500 | | | | | | | |
| 5 | 51 | -0.285 | -0.365 | -0.560 | -0.895 | -1.070 | -1.275 | | | | | | | |
| 5 | 46 | -0.295 | -0.435 | -0.575 | -0.730 | -0.870 | -1.030 | | | | | | | |
| 7 | 16 | -0.765 | -0.930 | -1.230 | -1.770 | -2.105 | -2.320 | | | | | | | |
| 7 | 37 | -0.220 | -0.245 | -0.485 | -0.720 | -0.880 | -1.005 | | | | | | | |
| 7 | 53 | -0.140 | 0.000 | -0.550 | -0.935 | -1.200 | -1.530 | | | | | | | |
| 7 | 60 | -3.590 | -3.720 | -3.835 | -4.140 | -4.270 | -4.390 | | | | | | | |
| 8 | 54 | 0.200 | 0.090 | -0.060 | -0.290 | -0.385 | -0.465 | | | | | | | |
| 8 | 59 | -0.140 | -0.310 | -0.505 | -0.740 | -0.940 | -0.980 | | | | | | | |
| 8 | 1 | -0.140 | -0.335 | -0.455 | -0.955 | -1.200 | -1.155 | | | | | | | |
| 8 | 19 | -0.855 | -0.980 | -1.290 | -1.835 | -2.250 | -2.445 | | | | | | | |
| 8 | 61 | -0.230 | -0.350 | -0.455 | -0.715 | -0.885 | -1.040 | | | | | | | |
| 10 | 56 | 0.030 | -0.015 | -0.070 | -0.360 | -0.460 | -0.615 | | | | | | | |
| 11 | 57 | -0.020 | -0.225 | -0.395 | -0.510 | -0.520 | -0.585 | | | | | | | |
| 11 | 4 | -0.025 | -0.140 | -0.325 | -0.550 | -0.670 | -0.660 | | | | | | | |
| 11 | 25 | -0.555 | -0.660 | -0.800 | -1.040 | -1.285 | -1.430 | | | | | | | |
| 11 | 62 | -0.510 | -0.605 | -0.850 | -1.230 | -1.370 | -1.495 | | | | | | | |
| 12 | 58 | -0.180 | -0.250 | -0.495 | -0.640 | -0.640 | -0.780 | | | | | | | |
| 13 | 55 | -0.135 | -0.245 | -0.445 | -0.745 | -0.845 | -0.930 | | | | | | | |
| 13 | 7 | 0.015 | -0.130 | -0.235 | -0.440 | -0.495 | -0.665 | | | | | | | |
| 13 | 22 | -0.325 | -0.395 | -0.490 | -0.590 | -0.670 | -0.730 | | | | | | | |
| 13 | 63 | -0.465 | -0.570 | -0.725 | -1.035 | -1.145 | -1.240 | | | | | | | |
| 14 | 52 | -0.045 | 0.640 | -0.185 | -0.370 | -0.415 | -0.550 | | | | | | | |

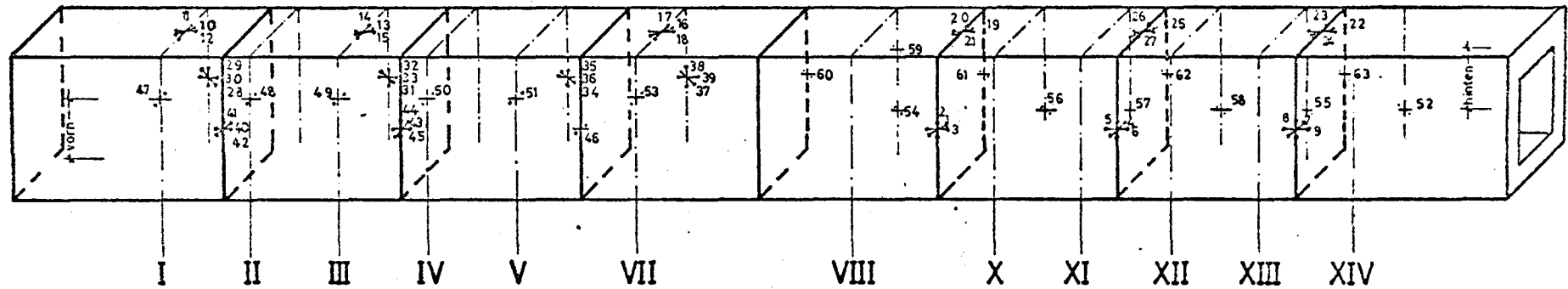
<http://www.digibib.tu-bs.de/?docid=00055325>

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Betonranddehnungen (graphische Form)

Betondehnung in Querrrichtung des Versuchsbalkens SETMQ 1

ohne Berücksichtigung der Vorspannung



MESZSTELLENUMMER 11

29

41

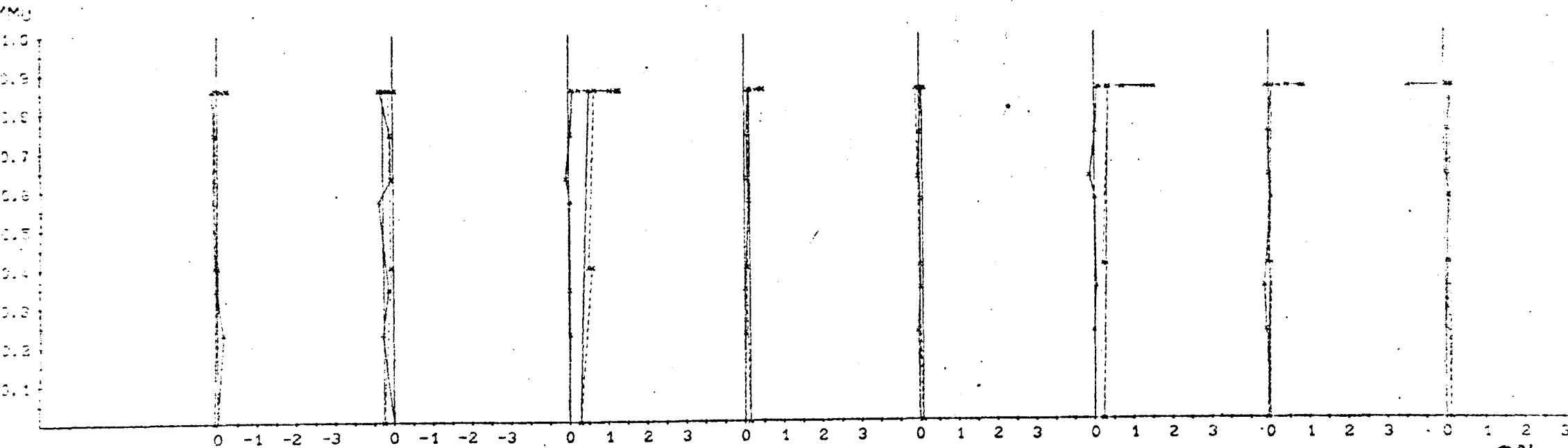
14

32

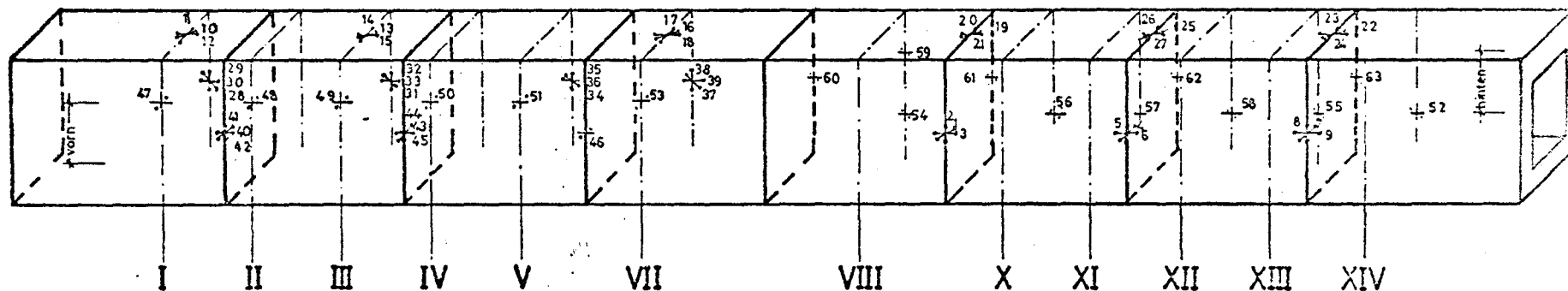
44

35

17



Betondehnung in Querrichtung des Versuchsbalkens SETMQ 1 ohne Berücksichtigung der Vorspannung



MESSTSTELLENNUMMER 38

2

20

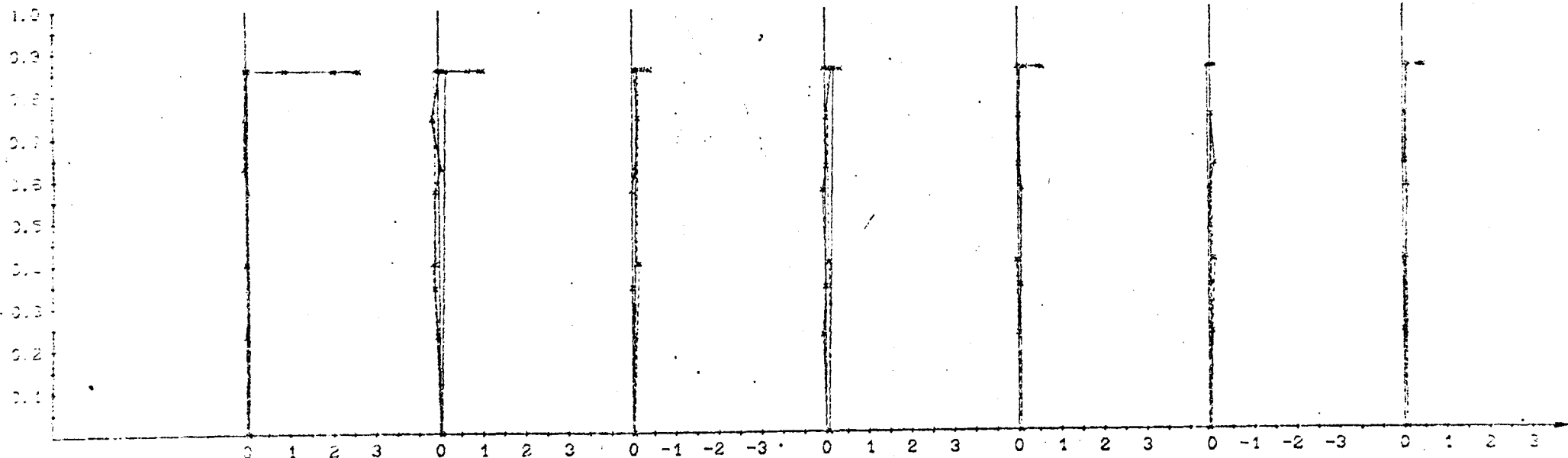
5

26

8

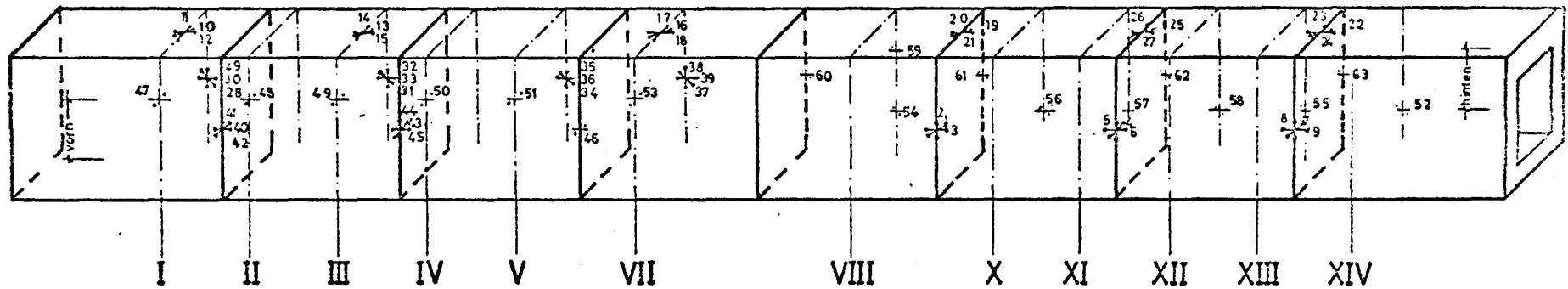
23

$\mu\text{m/m}$



ϵ ‰

Betondehnung in Längsrichtung des Versuchsbalkens SETMQ 1 ohne Berücksichtigung der Vorspannung



Messstellennummer 39

3

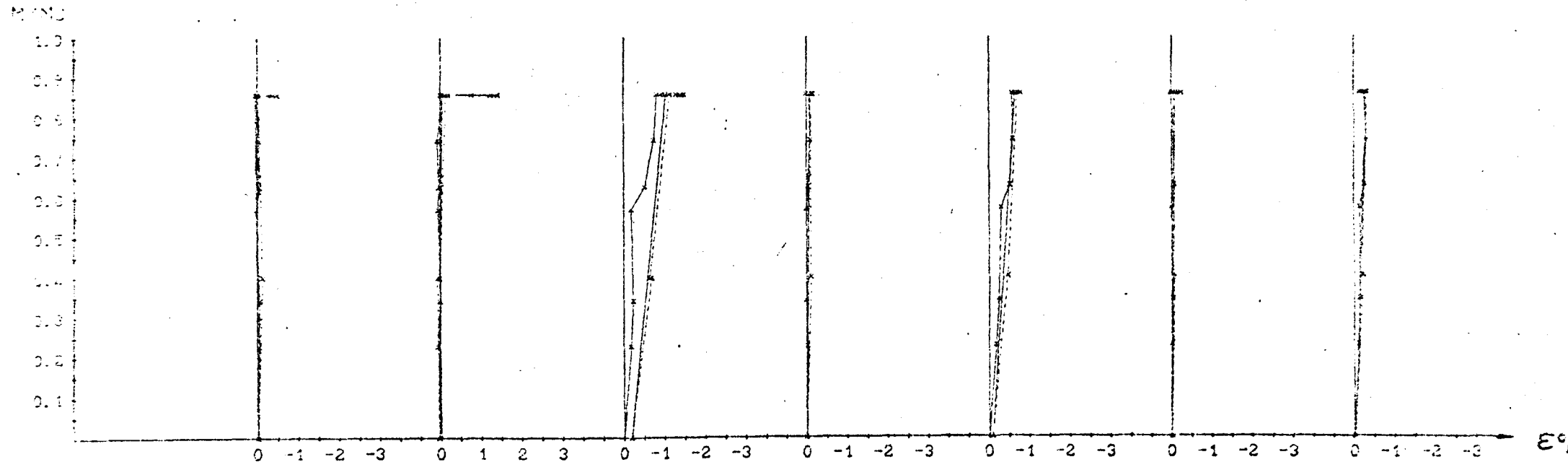
21

6

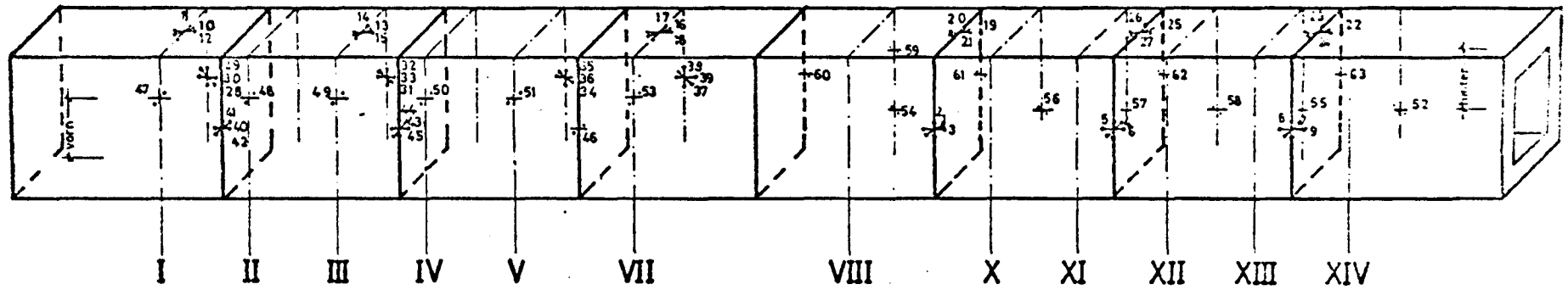
27

9

24



Betondehnung in Längsrichtung des Versuchsbalkens SETMQ 1 ohne Berücksichtigung der Vorspannung



MESSSTELLENNUMMER 12

30

42

15

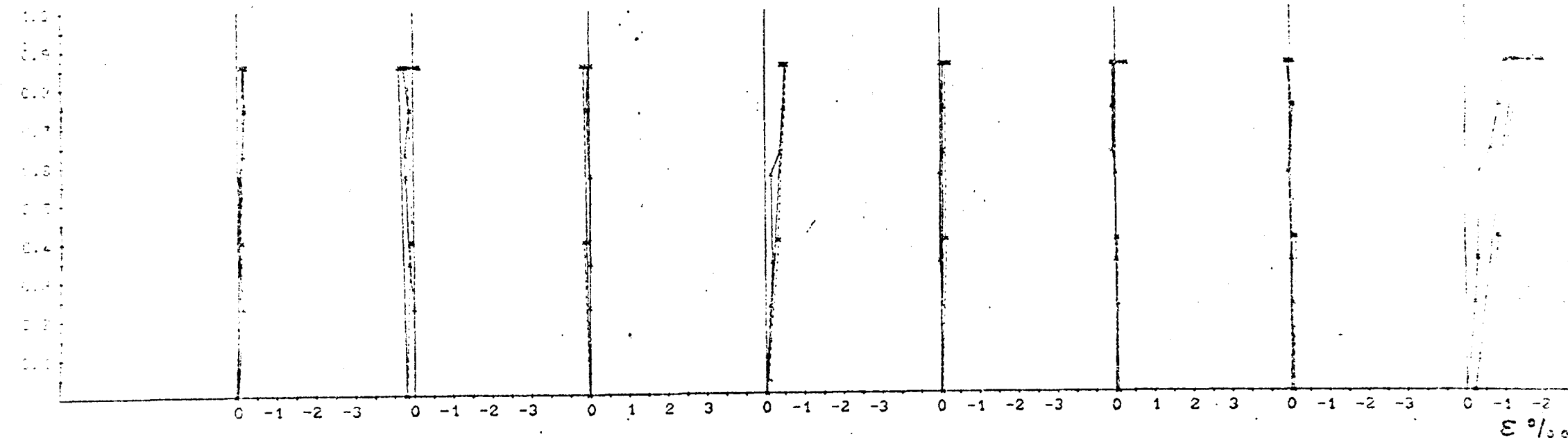
33

45

36

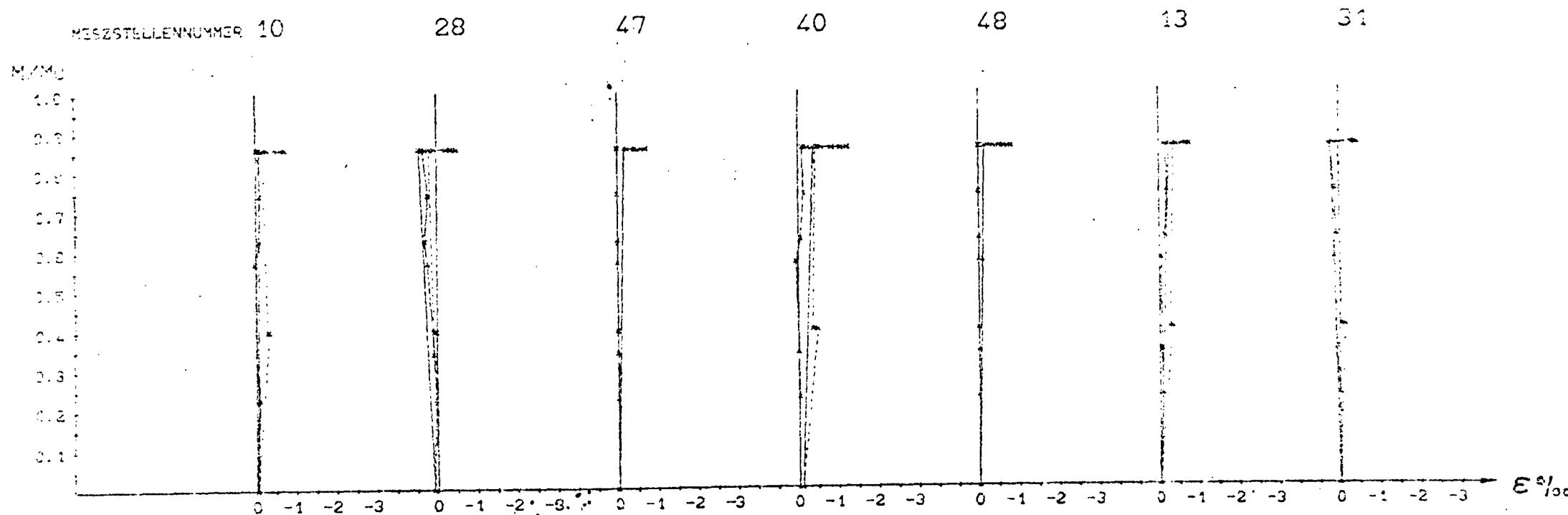
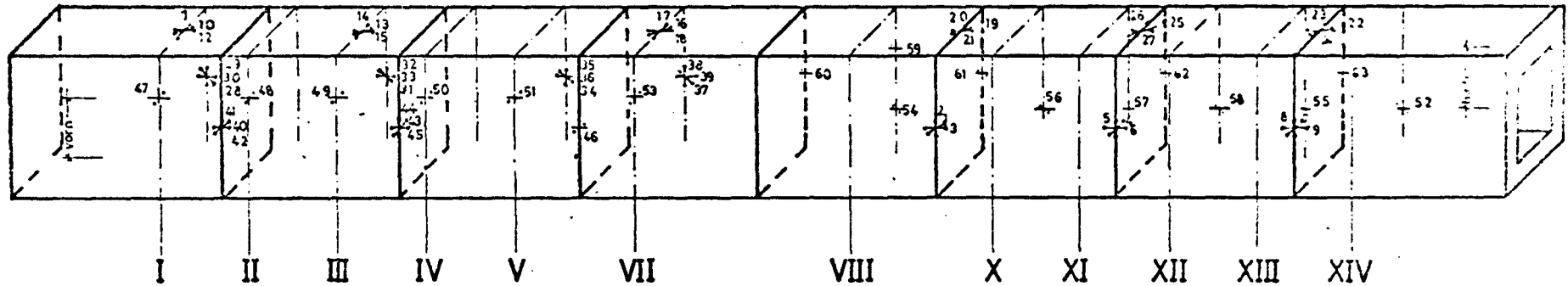
16

MCMJ

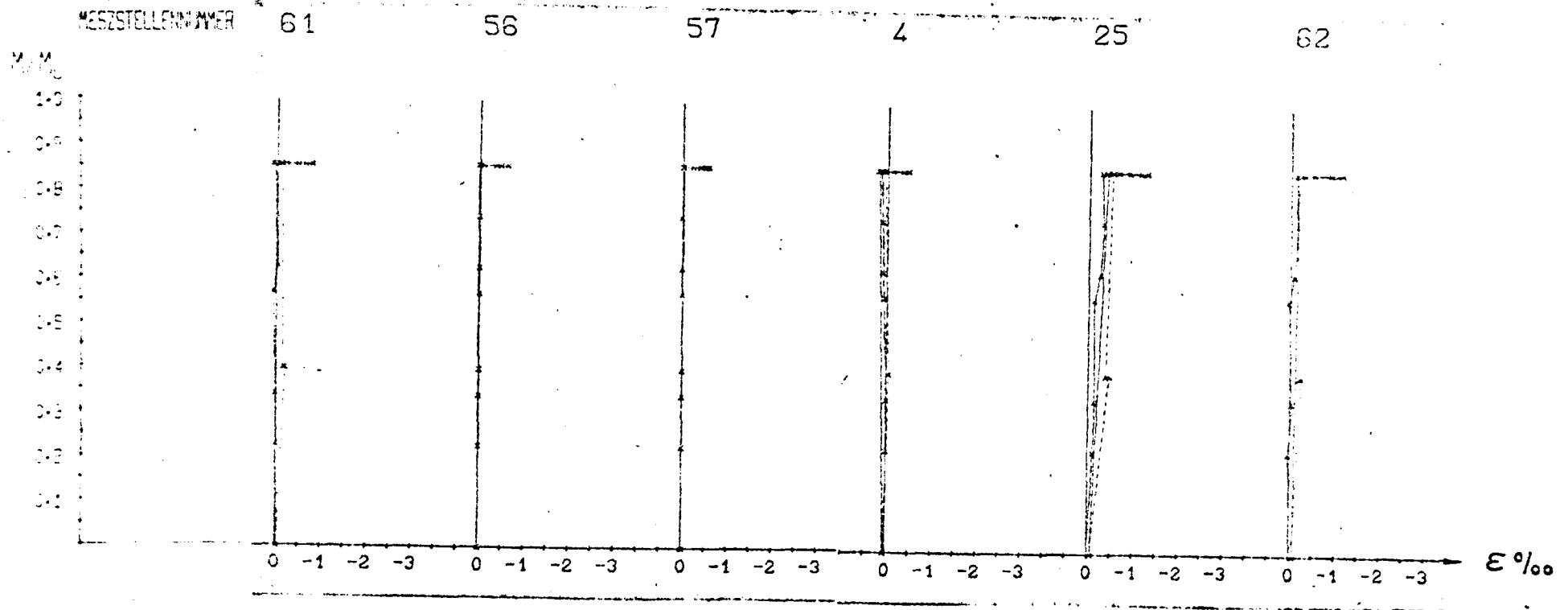
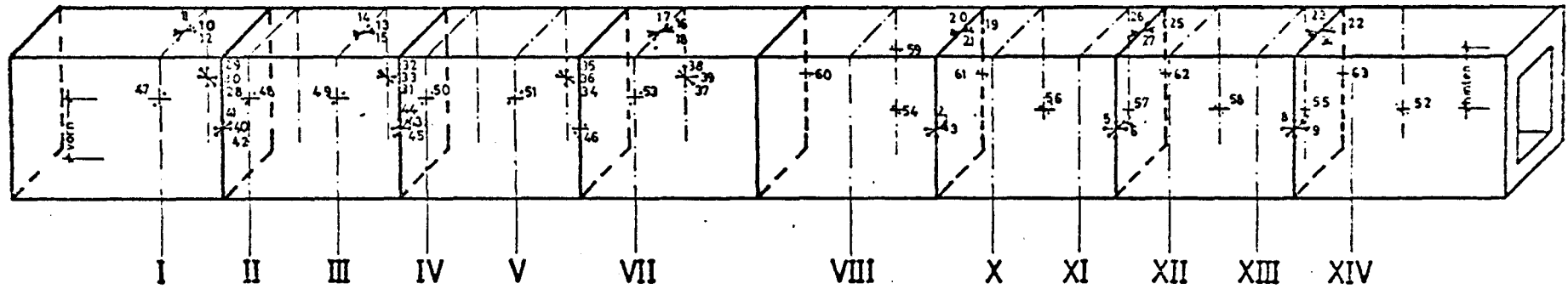


Betondehnung in Trajektorienrichtung des Versuchsbalkens SETMQ 1

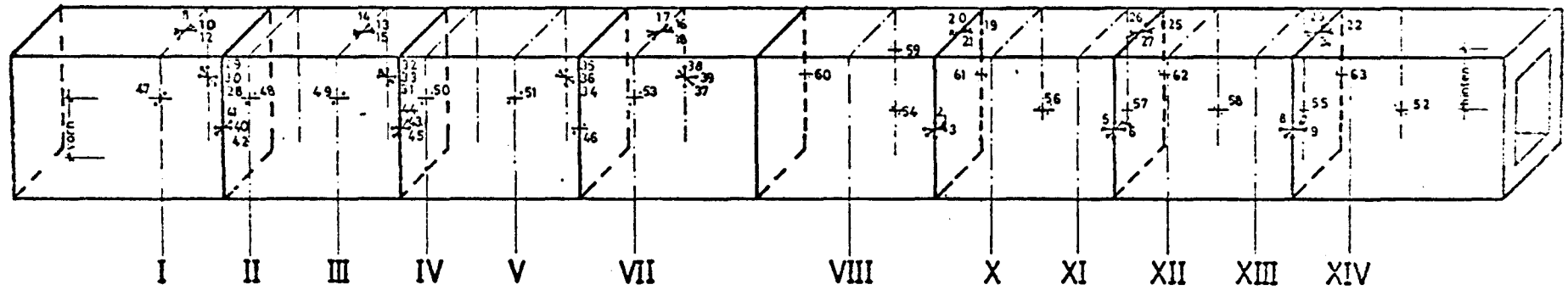
ohne Berücksichtigung der Vorspannung



Betondehnung in Trajektorienrichtung des Versuchsbalkens SETMQ 1 ohne Berücksichtigung der Vorspannung



Betondehnung in Trajektorienrichtung des Versuchsbalkens SETM Q 1 ohne Berücksichtigung der Vorspannung



KERZSTÄBENNUMMER 37

53

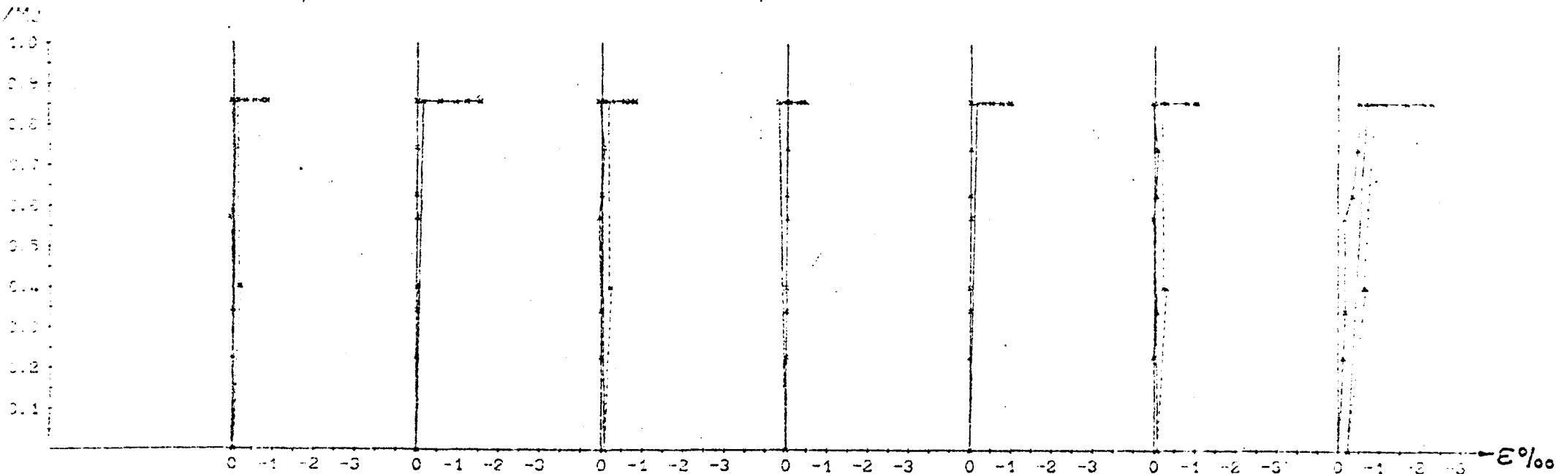
60

54

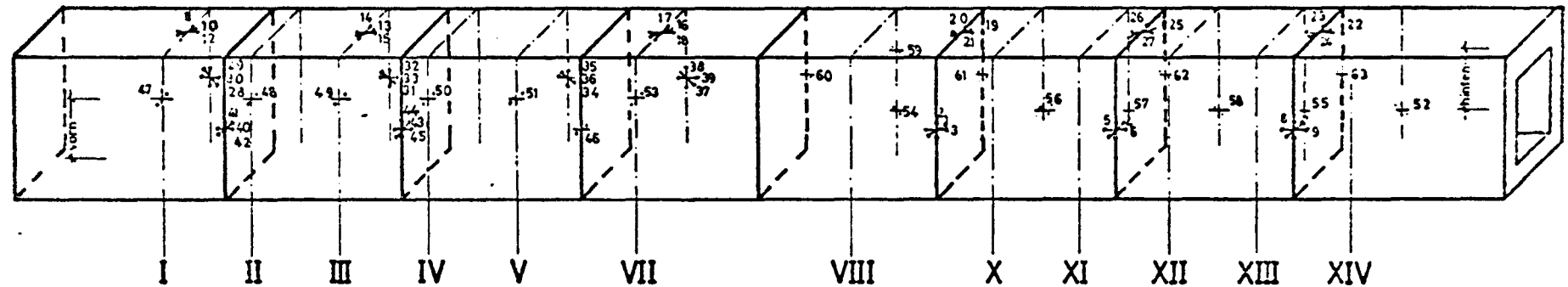
59

1

19



Betondehnung in Trajektorienrichtung des Versuchsbalkens SETMQ 1 ohne Berücksichtigung der Vorspannung



Messstellennummer 49

43

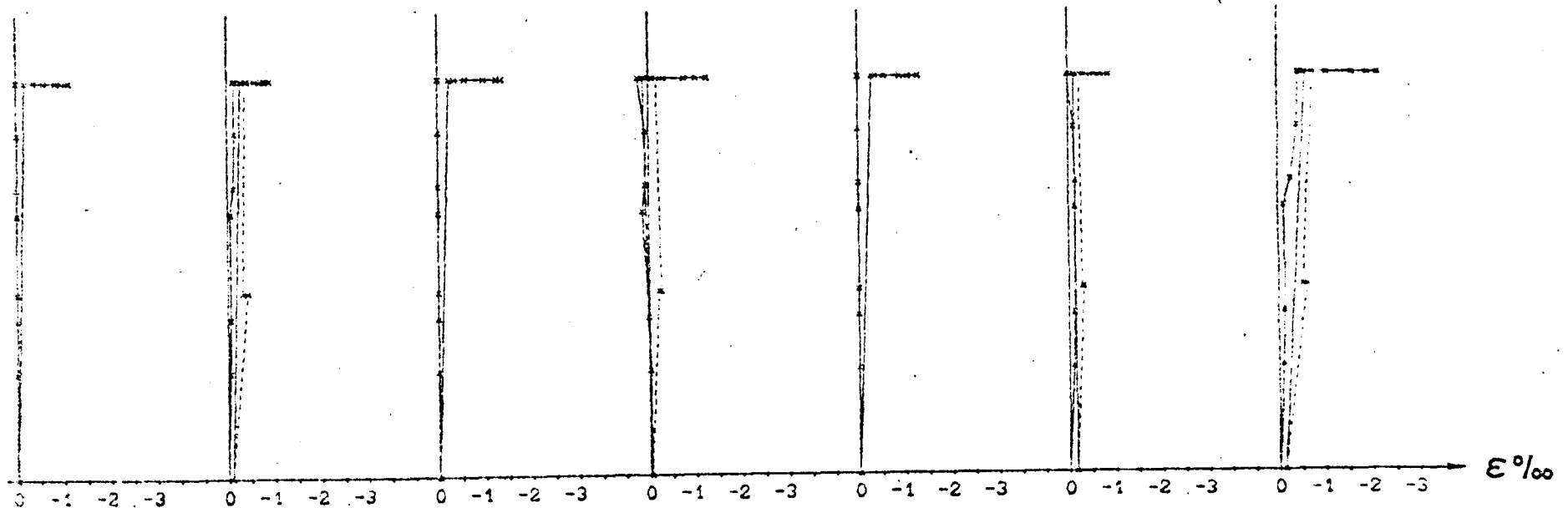
50

34

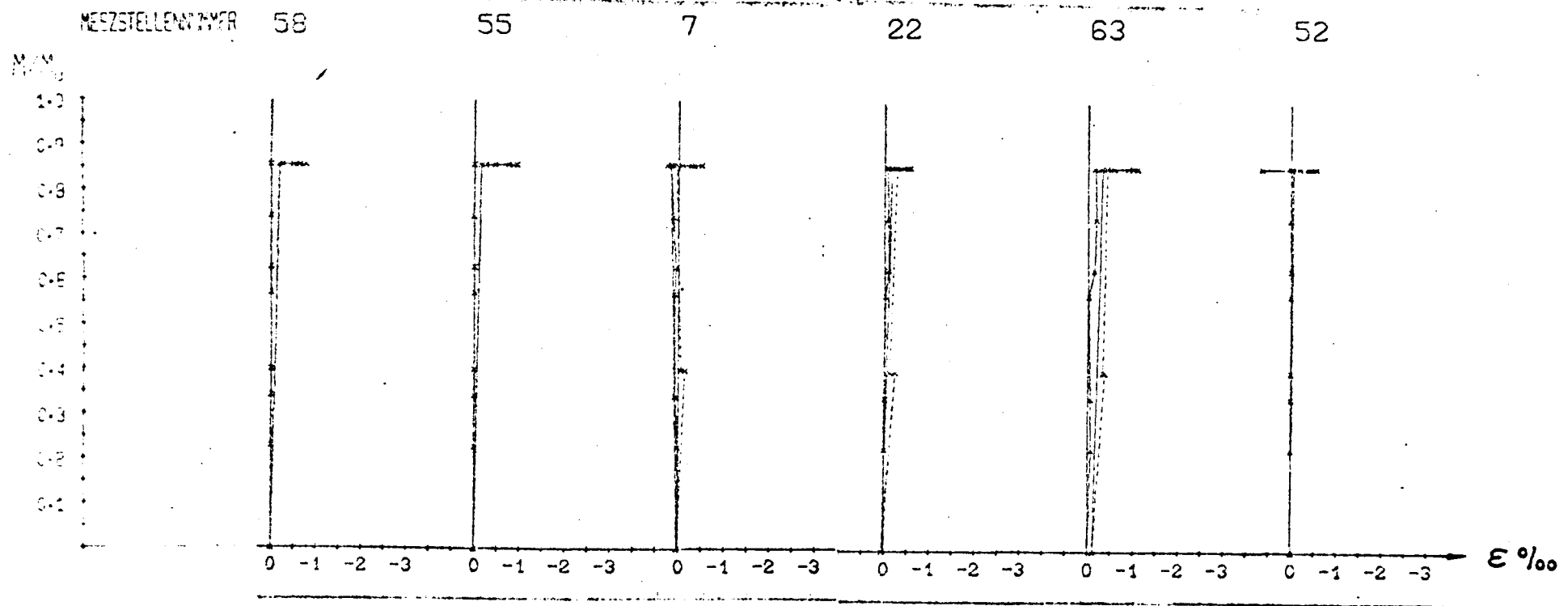
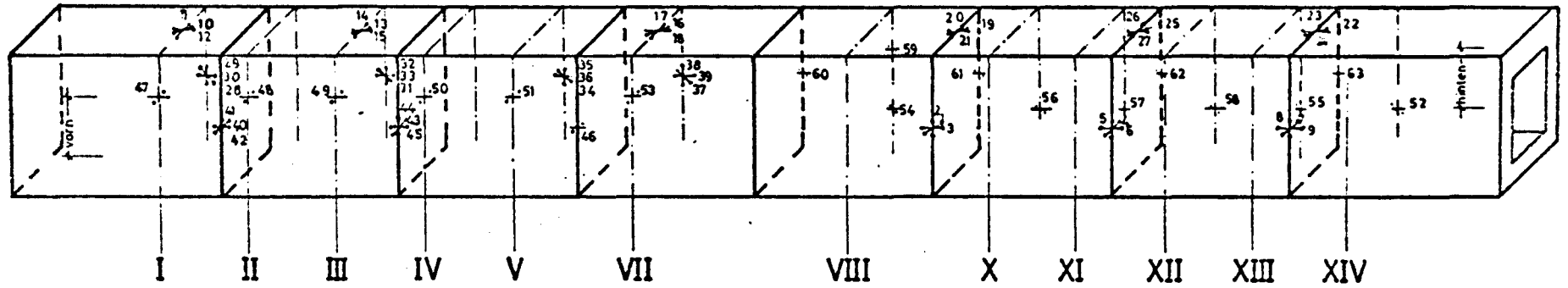
51

46

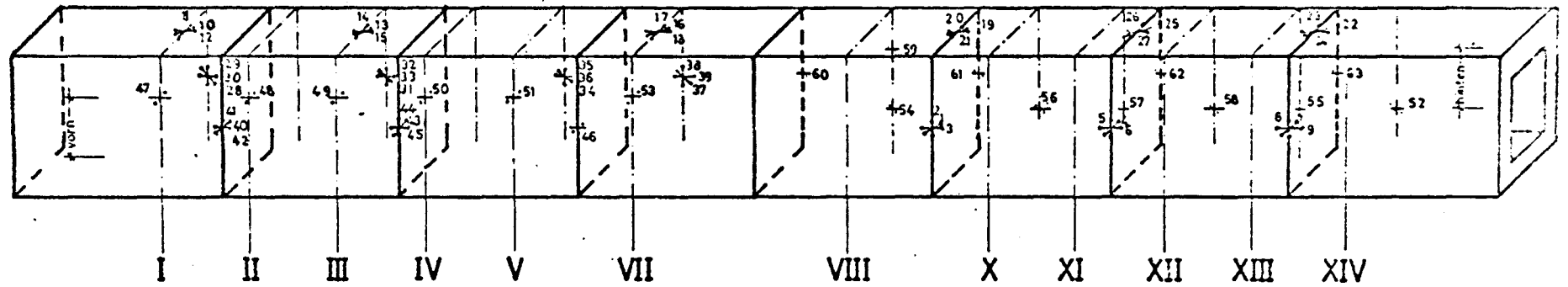
16



Betondehnung in Trajektorienrichtung des Versuchsbalkens SETMQ 1 ohne Berücksichtigung der Vorspannung



Betondehnung in Querrichtung des Versuchsbalkens SETMQ 1 unter Berücksichtigung der Vorspannung



MESSTEILNUMMER 11

29

41

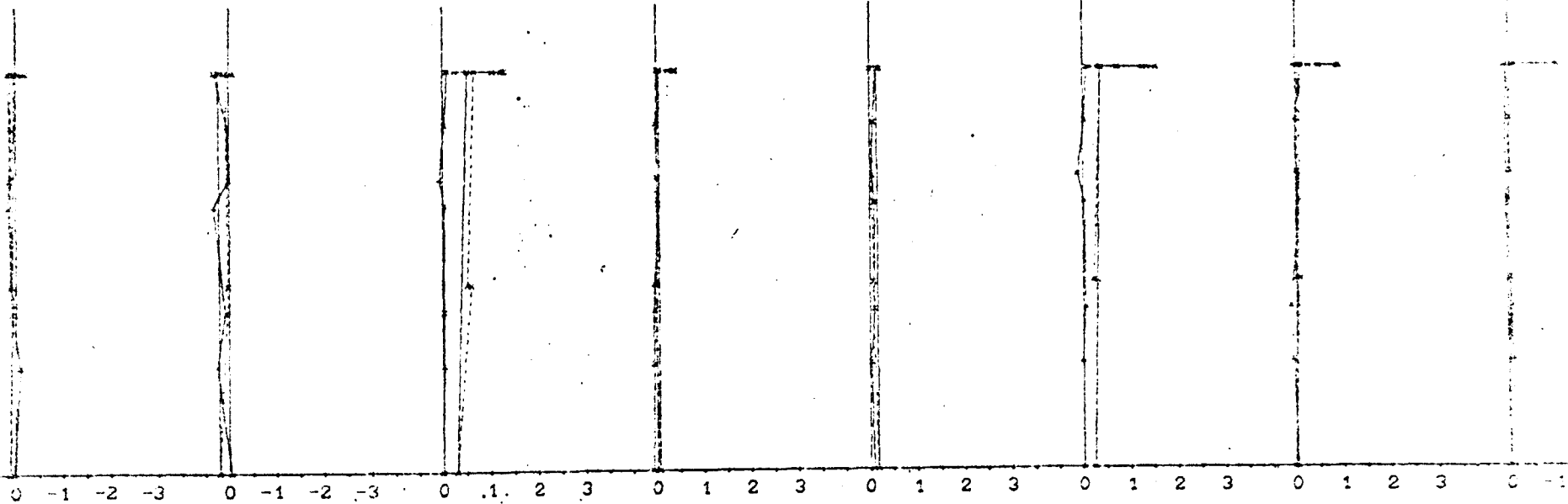
14

32

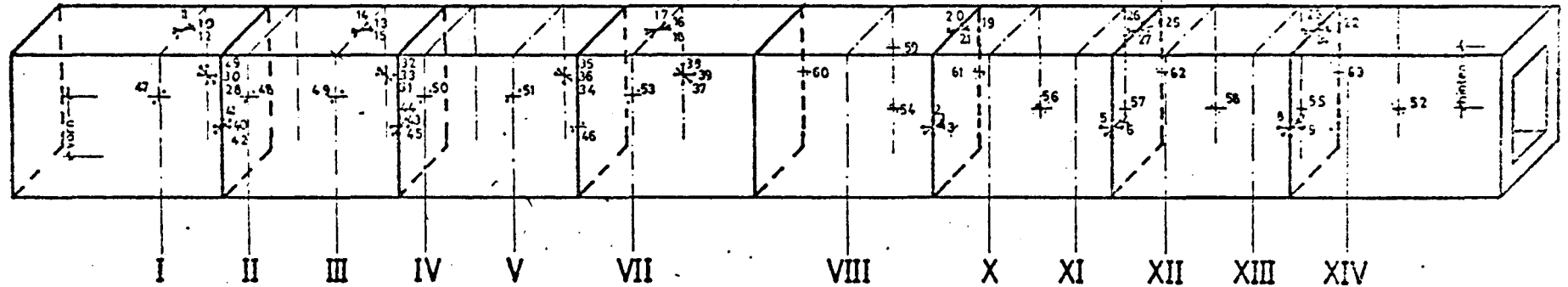
44

35

17



Betondehnung in Querrichtung des Versuchsbalkens SETMQ 1 unter Berücksichtigung der Vorspannung



MESSTELLENNUMMER 33

2

20

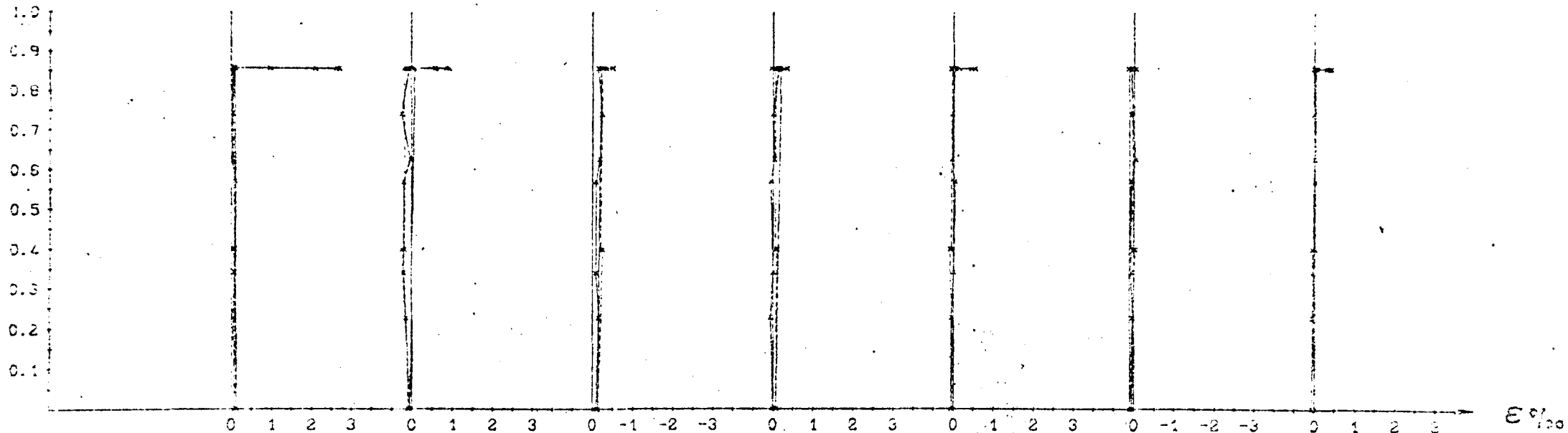
5

26

8

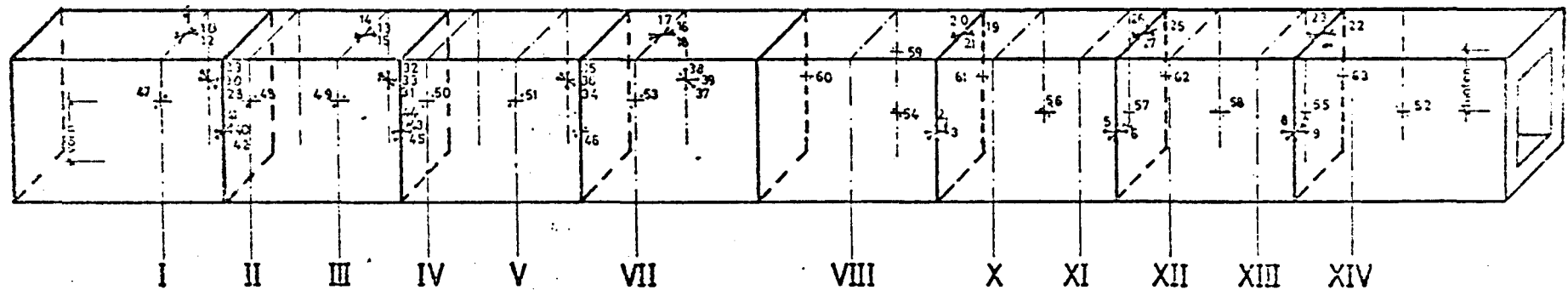
23

MM

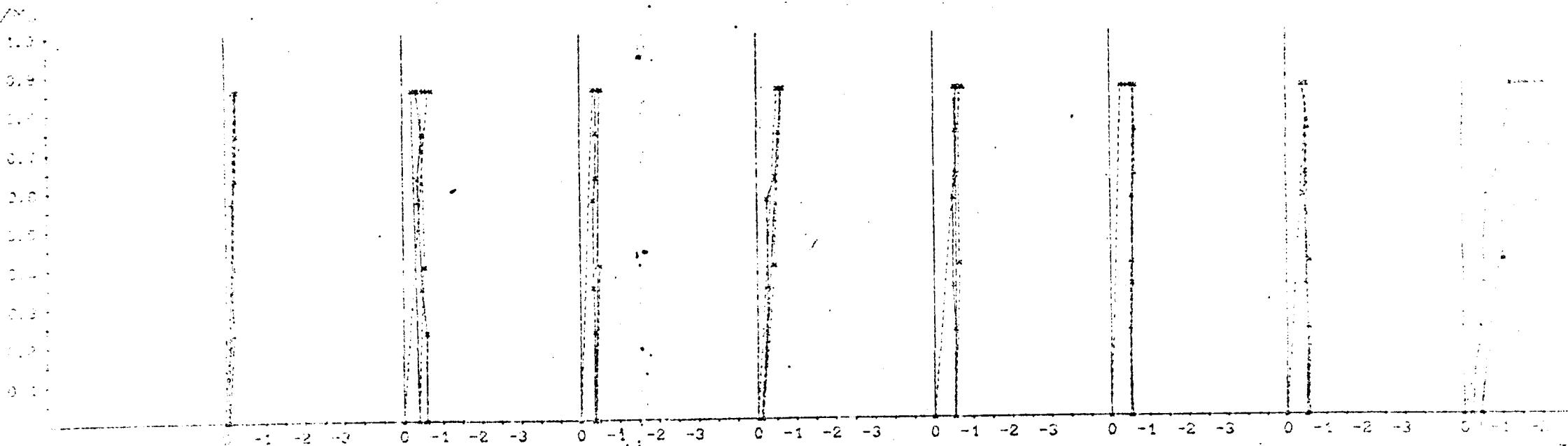


Betondehnung in Längsrichtung des Versuchsbalkens SETMQ 1

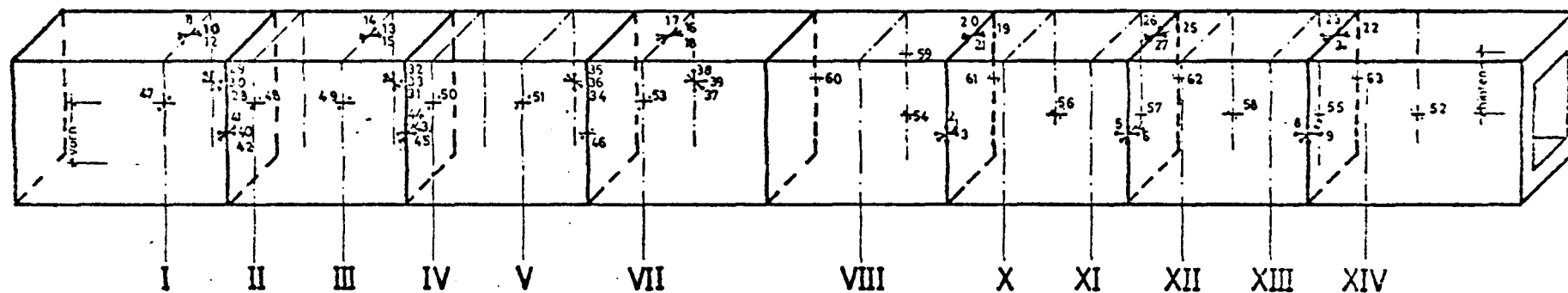
unter Berücksichtigung der Vorspannung



MESSSTELLENNUMMER 12 30 42 15 33 45 36 13



Betondehnung in Längsrichtung des Versuchsbalkens SETMQ 1 unter Berücksichtigung der Vorspannung



MESZSTELLENNUMMER 39

3

21

6

27

9

24

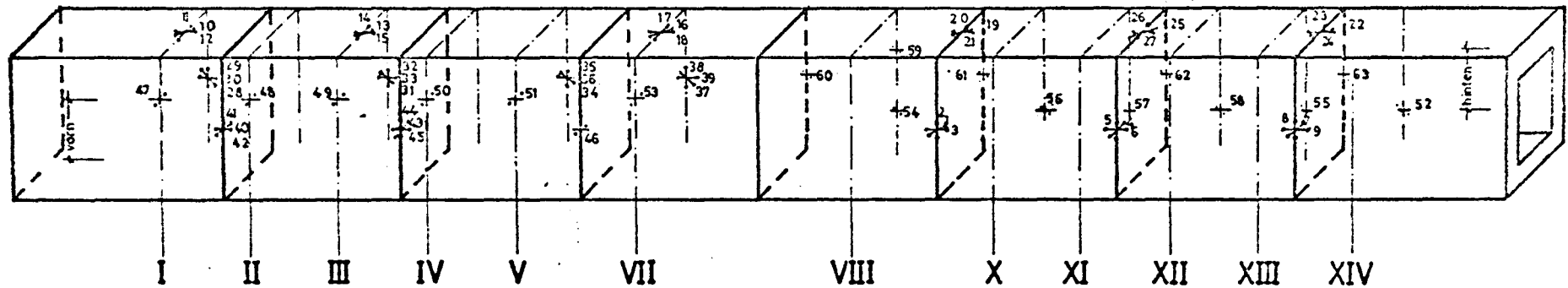
M/M₀

1.0
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0.0

0 -1 -2 -3 0 1 2 3 0 -1 -2 -3 0 -1 -2 -3 0 -1 -2 -3 0 -1 -2 -3

ϵ %

Betondehnung in Trajektorienrichtung des Versuchsbalkens SETMQ 1 unter Berücksichtigung der Vorspannung



MESSSTELLENNUMMER 61

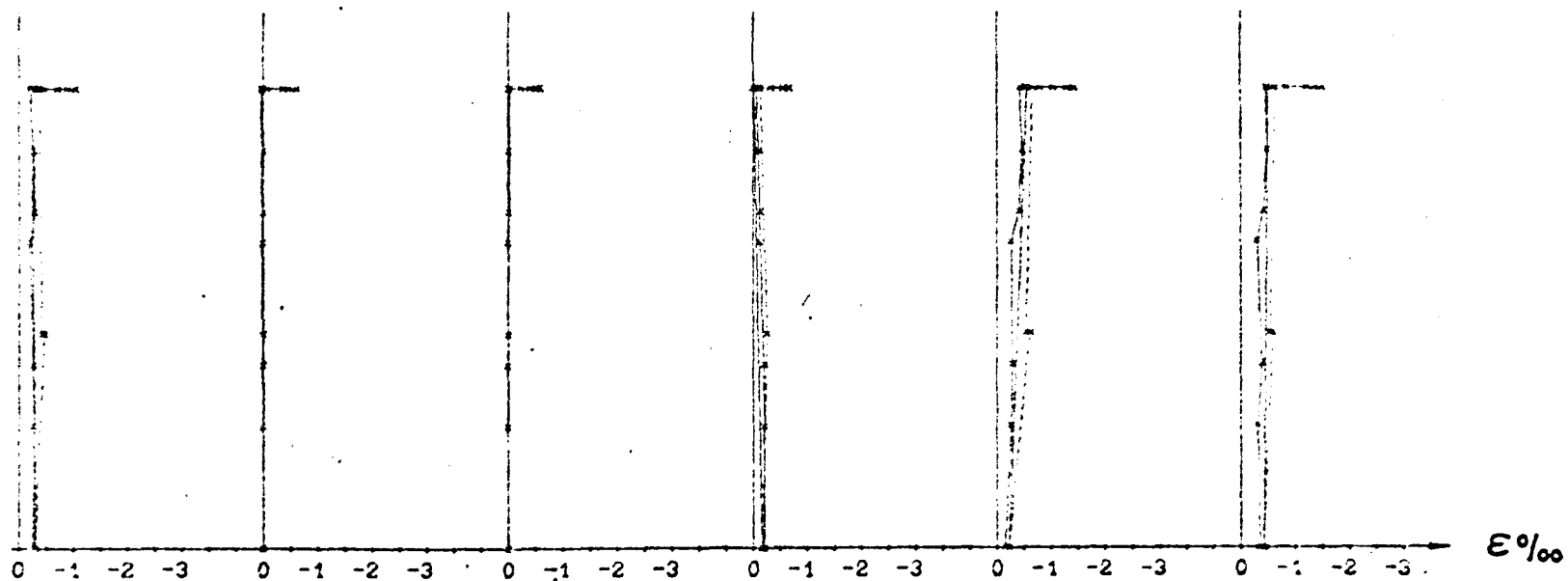
56

57

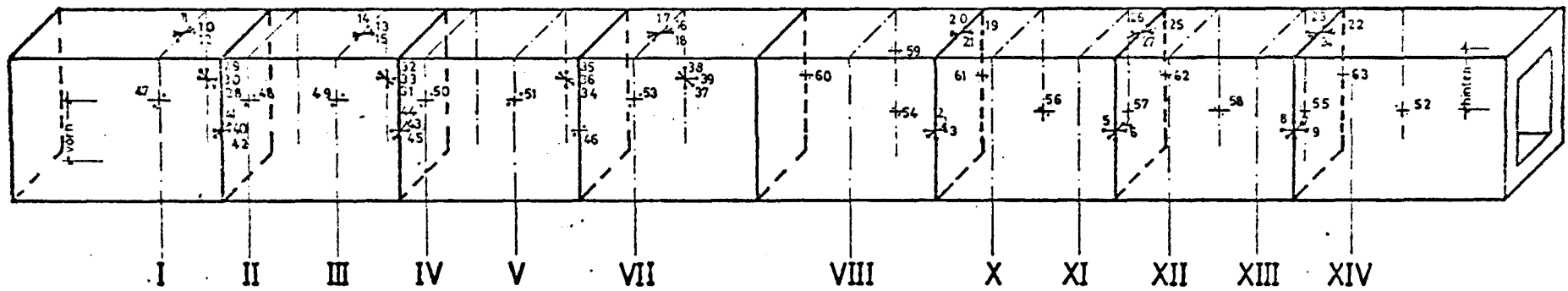
4

25

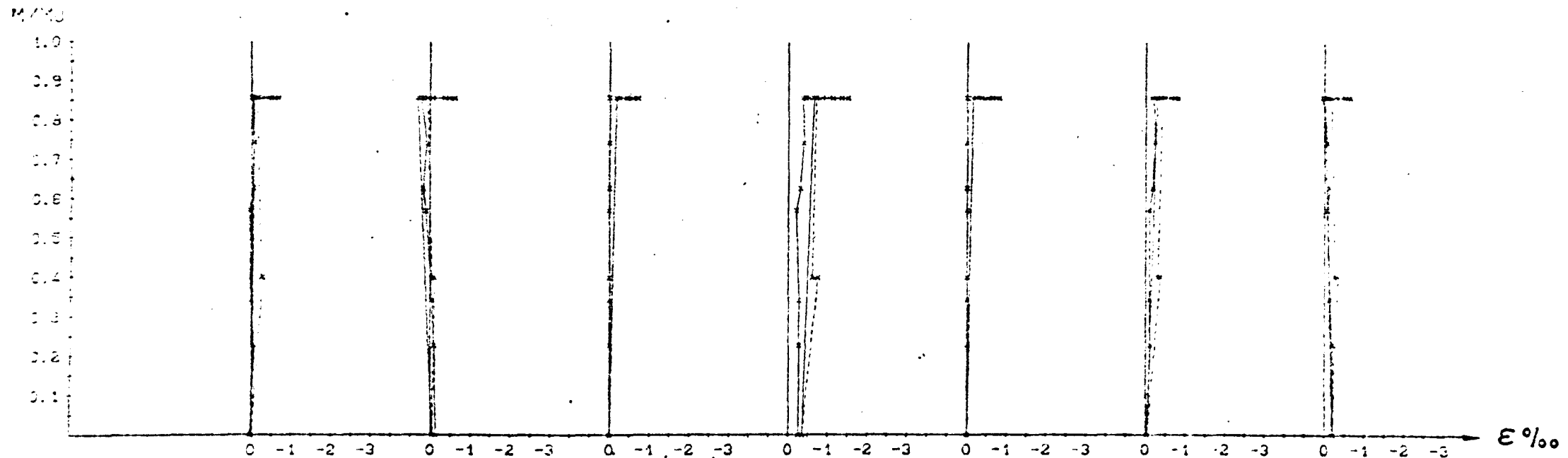
62



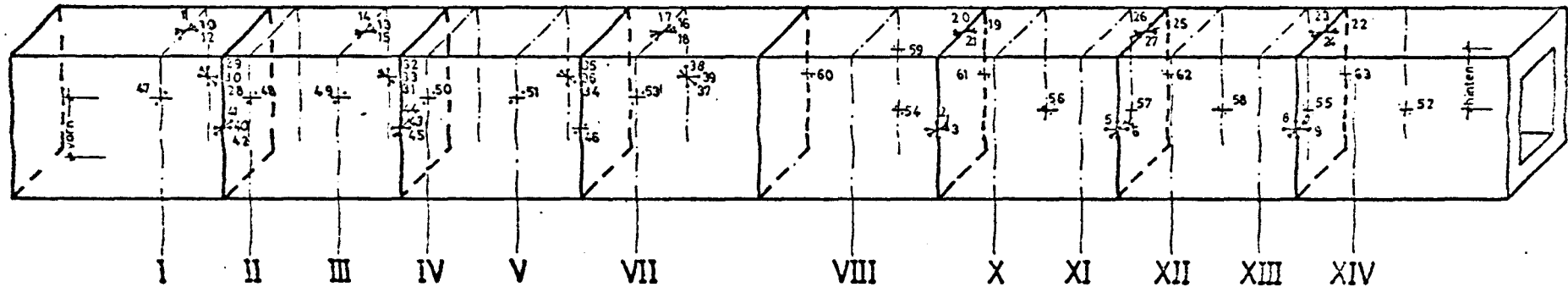
Betondehnung in Trajektorienrichtung des Versuchsbalkens SETM Q 1 unter Berücksichtigung der Vorspannung



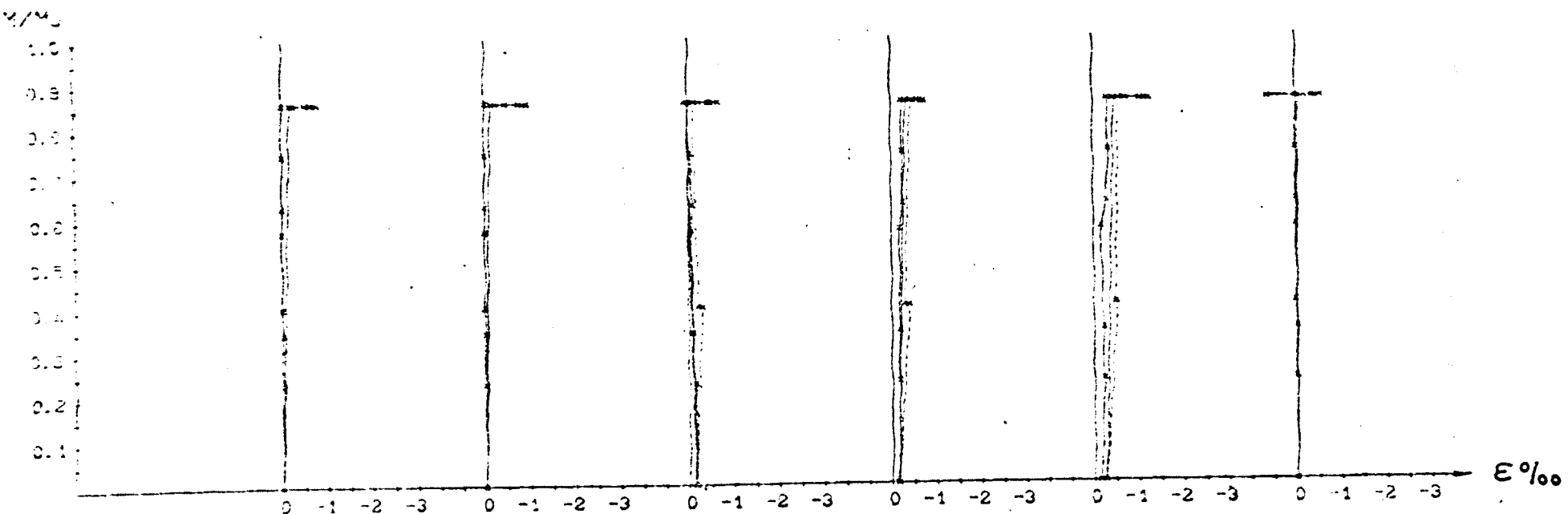
MESSSTELLENNUMMER 10 28 47 40 48 13 31



Betondehnung in Trajektorienrichtung des Versuchsbalkens SETMQ 1 unter Berücksichtigung der Vorspannung

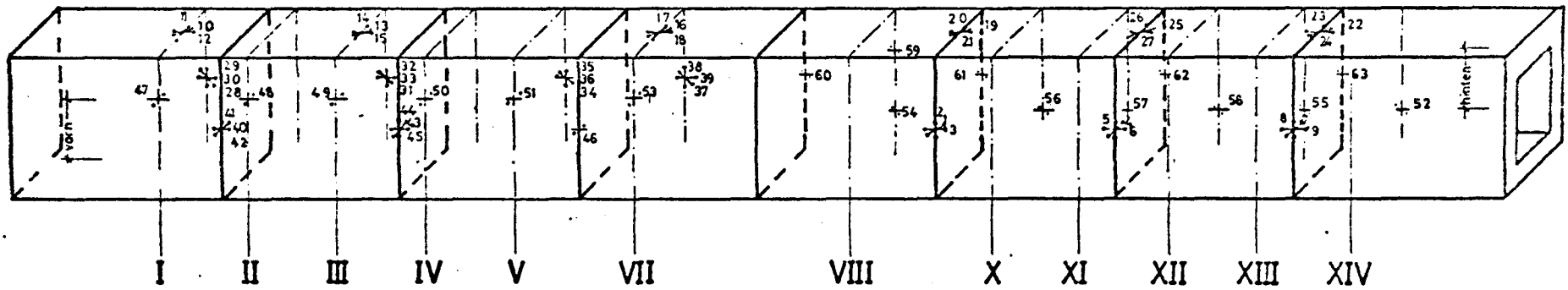


MESSTELLENNUMMER 58 55 7 22 63 52



Betondehnung in Trajektorienrichtung des Versuchsbalkens SETMQ 1

unter Berücksichtigung der Vorspannung



MEßFELDNUMMERN 37

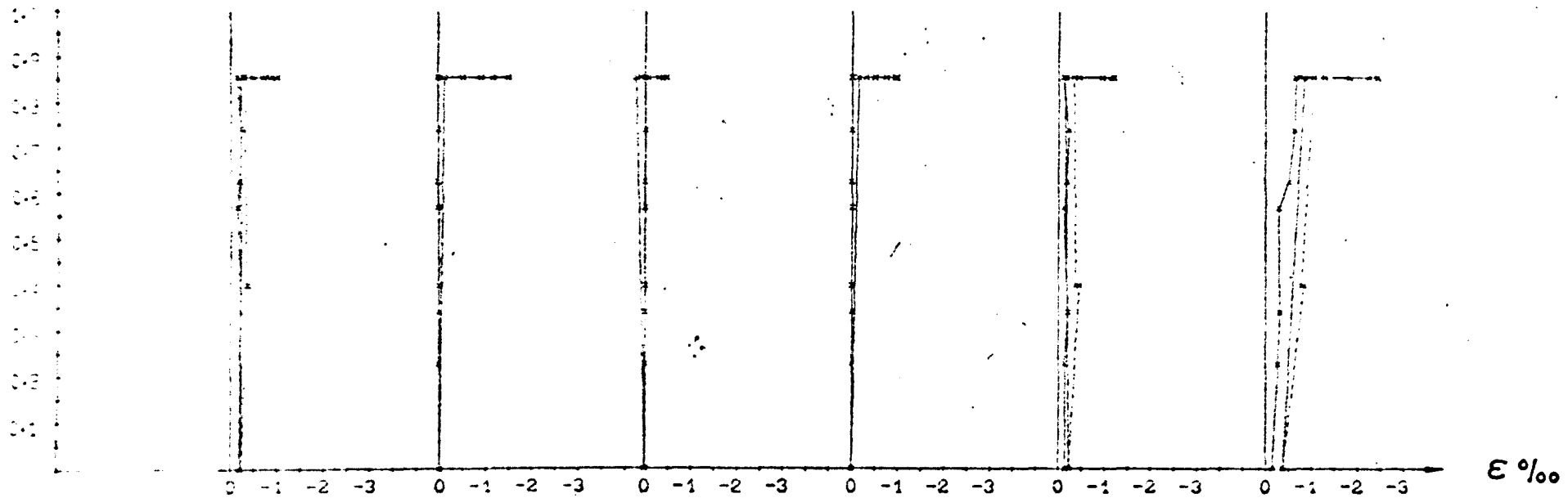
53

54

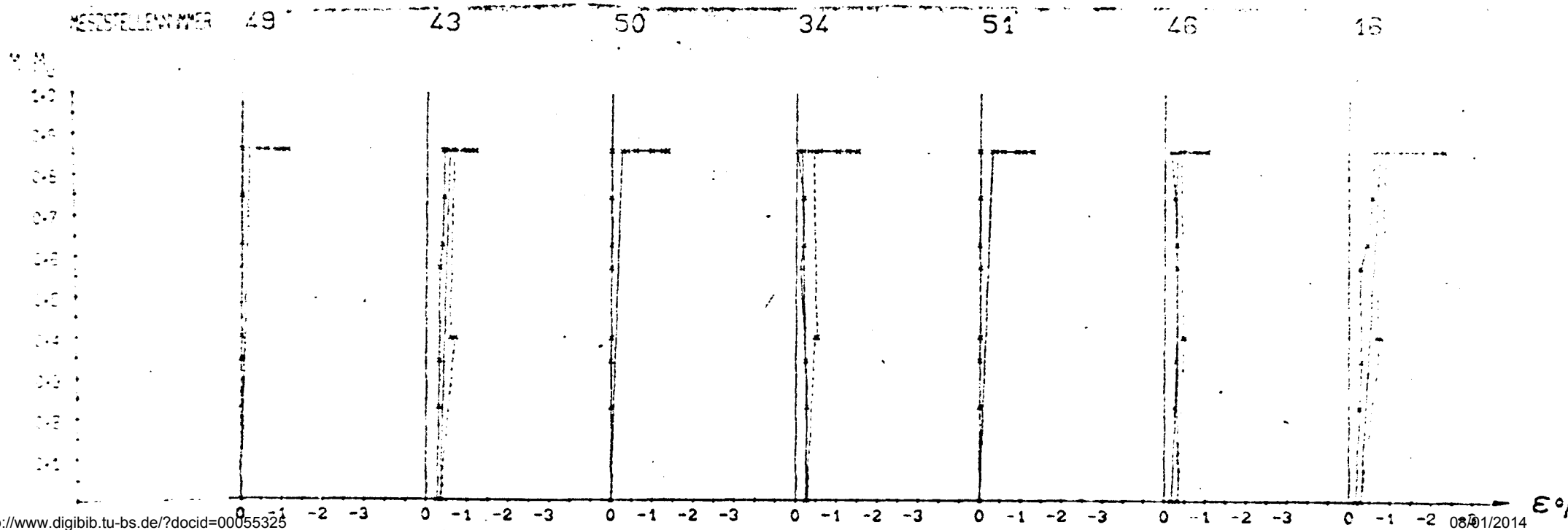
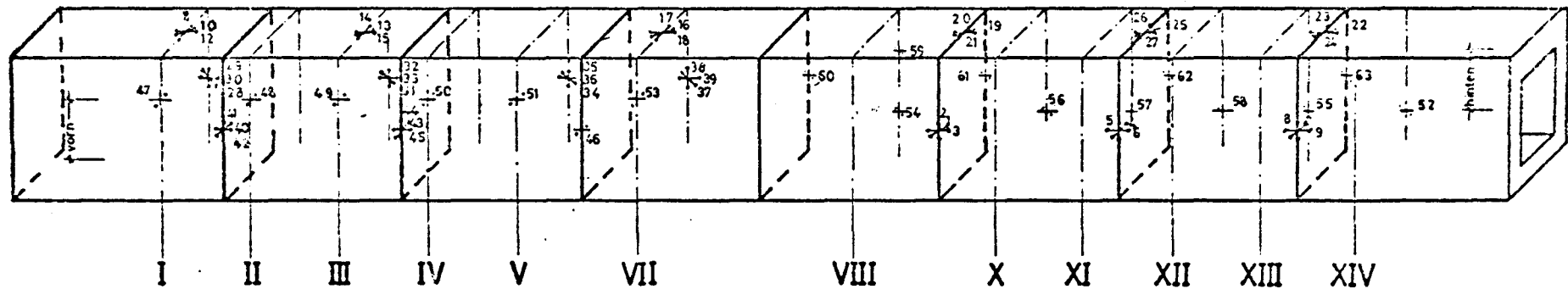
59

1

19



Betondehnung in Trajektorienrichtung des Versuchsbalkens SETMQ 1 unter Berücksichtigung der Vorspannung



Betonhauptdehnungen

HAUPTDEHNUNGEN DES BETONS

1. ZEILE = EPSILON MAX IN PROMILLE

2. ZEILE = EPSILON MIN IN PROMILLE

3. ZEILE = WINKEL ZWISCHEN EPSILON MIN UND DER LAENGSSACHSE

BELASTUNGSGRAD M/MU

| SCHNITT | LAGE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
|---------|--------|---------|---------|--------|--------|--------|--------|-------|-------|-------|-------|-------|-------|-------|
| | | 7 | 9 | 11 | 13 | 15 | 16 | | | | | | | |
| 1 | HINTEN | 0.380 | 0.363 | 0.276 | 0.120 | 0.152 | -0.015 | | | | | | | |
| | | -0.395 | -0.378 | -0.556 | -0.740 | -0.702 | -0.780 | | | | | | | |
| | | -27.489 | -14.753 | -4.844 | 4.348 | 14.332 | 18.248 | | | | | | | |
| 3 | HINTEN | 0.201 | 0.120 | 0.070 | 0.116 | 0.302 | 0.354 | | | | | | | |
| | | -0.631 | -0.700 | -0.725 | -0.796 | -0.817 | -0.889 | | | | | | | |
| | | -14.360 | -11.875 | -0.901 | 12.300 | 18.870 | 19.888 | | | | | | | |
| 5 | HINTEN | 0.113 | 0.071 | 0.561 | 1.151 | 1.746 | 1.995 | | | | | | | |
| | | -0.473 | -0.511 | -0.671 | -1.121 | -1.431 | -1.660 | | | | | | | |
| | | -3.927 | 9.529 | 27.961 | 32.507 | 31.980 | 32.927 | | | | | | | |
| 7 | HINTEN | 0.117 | 0.103 | 1.314 | 2.718 | 3.420 | 3.536 | | | | | | | |
| | | -0.377 | -0.428 | -0.759 | -1.298 | -1.560 | -1.721 | | | | | | | |
| | | 10.685 | 9.047 | 23.673 | 22.702 | 23.314 | 23.348 | | | | | | | |
| 1 | HINTEN | 0.033 | 0.061 | 0.019 | 0.137 | 0.091 | 0.210 | | | | | | | |
| | | -0.238 | -0.271 | -0.284 | -0.467 | -0.591 | -0.695 | | | | | | | |
| | | -5.863 | 14.443 | 32.778 | 32.778 | 42.897 | 40.711 | | | | | | | |
| 3 | HINTEN | 0.050 | 0.047 | 0.113 | 0.507 | 0.728 | 0.787 | | | | | | | |
| | | -0.020 | -0.642 | -0.678 | -0.762 | -0.878 | -0.957 | | | | | | | |
| | | 0.055 | 5.655 | 14.985 | 26.181 | 27.957 | 28.109 | | | | | | | |
| 7 | HINTEN | 0.083 | 0.081 | -0.991 | 0.233 | 0.384 | 0.523 | | | | | | | |
| | | -1.468 | -1.571 | -1.699 | -2.168 | -2.529 | -2.748 | | | | | | | |
| | | 2.081 | 6.471 | -9.473 | 20.980 | 22.570 | 23.801 | | | | | | | |

HAUPTDEHNUNGEN DES BETONS

1. ZEILE = EPSILON MAX IN PROMILLE

2. ZEILE = EPSILON MIN IN PROMILLE

3. ZEILE = WINKEL ZWISCHEN EPSILON MIN UND DER LAENGSSACHSE

BELASTUNGSGRAD M/MU

| SCHNITT | LAGE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
|---------|--------|---------|---------|--------|--------|--------|-------|-------|-------|-------|-------|-------|-------|
| | | 9 | 11 | 13 | 15 | 16 | | | | | | | |
| ----- | | | | | | | | | | | | | |
| 1 | HINTEN | 0.355 | 0.352 | 0.297 | 0.443 | 0.331 | | | | | | | |
| | | 0.260 | -0.002 | -0.287 | -0.363 | -0.496 | | | | | | | |
| | | 1.506 | 20.213 | 29.518 | 37.809 | 42.748 | | | | | | | |
| ----- | | | | | | | | | | | | | |
| 3 | HINTEN | 0.103 | -0.010 | 0.107 | 0.339 | 0.393 | | | | | | | |
| | | -0.248 | -0.210 | -0.352 | -0.419 | -0.493 | | | | | | | |
| | | -31.900 | -1.431 | 29.625 | 33.748 | 33.019 | | | | | | | |
| ----- | | | | | | | | | | | | | |
| 5 | HINTEN | 0.096 | 0.681 | 1.288 | 1.870 | 2.124 | | | | | | | |
| | | -0.066 | -0.321 | -0.788 | -1.085 | -1.319 | | | | | | | |
| | | 41.437 | 40.410 | 39.020 | 36.488 | 36.862 | | | | | | | |
| ----- | | | | | | | | | | | | | |
| 7 | HINTEN | 0.063 | 1.316 | 2.707 | 3.411 | 3.526 | | | | | | | |
| | | -0.058 | -0.431 | -0.957 | -1.221 | -1.381 | | | | | | | |
| | | 36.536 | 28.815 | 25.047 | 25.216 | 25.146 | | | | | | | |
| ----- | | | | | | | | | | | | | |
| 1 | OBEN | 0.080 | 0.090 | 0.200 | 0.177 | 0.290 | | | | | | | |
| | | -0.235 | -0.300 | -0.475 | -0.622 | -0.720 | | | | | | | |
| | | 30.296 | 45.734 | 40.094 | 48.051 | 45.000 | | | | | | | |
| ----- | | | | | | | | | | | | | |
| 3 | OBEN | 0.138 | 0.217 | 0.624 | 0.847 | 0.906 | | | | | | | |
| | | -0.558 | -0.607 | -0.704 | -0.822 | -0.901 | | | | | | | |
| | | 9.217 | 17.809 | 27.557 | 28.988 | 29.056 | | | | | | | |
| ----- | | | | | | | | | | | | | |
| 7 | OBEN | 0.156 | -0.894 | 0.308 | 0.461 | 0.600 | | | | | | | |
| | | -1.366 | -1.516 | -1.963 | -2.326 | -2.545 | | | | | | | |
| | | 5.876 | -13.901 | 21.430 | 23.009 | 24.240 | | | | | | | |
| ----- | | | | | | | | | | | | | |

HAUPTDEHNUNGEN DES BETONS

1. ZEILE = EPSILON MAX IN PROMILLE

2. ZEILE = EPSILON MIN IN PROMILLE

3. ZEILE = WINKEL ZWISCHEN EPSILON MIN UND DER LAENGSSACHSE

BELASTUNGSGRAD M/MU

| SCHNITT | LAGE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
|---------|------|---------|--------|--------|--------|--------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | --- | --- | --- | --- | --- | | | | | | | | |
| | | 9 | 11 | 13 | 15 | 16 | | | | | | | | |
| 8 | OBEN | -0.179 | -0.140 | 0.043 | 0.372 | 0.483 | | | | | | | | |
| | | -1.156 | -1.415 | -1.818 | -2.202 | -2.393 | | | | | | | | |
| | | 9.403 | 17.063 | 29.201 | 33.211 | 34.081 | | | | | | | | |
| 11 | OBEN | 0.044 | 0.110 | 0.537 | 1.091 | 1.241 | | | | | | | | |
| | | -0.709 | -0.795 | -1.012 | -1.291 | -1.461 | | | | | | | | |
| | | 14.047 | 21.381 | 28.693 | 30.157 | 30.009 | | | | | | | | |
| 13 | OBEN | 0.118 | 0.222 | 0.639 | 0.912 | 0.875 | | | | | | | | |
| | | -0.333 | -0.422 | -0.504 | -0.567 | -0.625 | | | | | | | | |
| | | 15.700 | 21.556 | 29.303 | 32.714 | 32.999 | | | | | | | | |
| 1 | VORN | 1.127 | 1.635 | 2.158 | 2.494 | 2.588 | | | | | | | | |
| | | -0.592 | -0.760 | -0.993 | -1.179 | -1.318 | | | | | | | | |
| | | 31.233 | 29.333 | 32.470 | 34.845 | 36.130 | | | | | | | | |
| 3 | VORN | 0.778 | 1.455 | 2.269 | 2.710 | 2.613 | | | | | | | | |
| | | -0.453 | -0.645 | -0.819 | -0.895 | -0.983 | | | | | | | | |
| | | 37.107 | 36.128 | 34.668 | 34.727 | 36.261 | | | | | | | | |
| 8 | VORN | 0.303 | 0.598 | 2.256 | 3.260 | 3.448 | | | | | | | | |
| | | -0.183 | -0.303 | -0.801 | -1.050 | -1.008 | | | | | | | | |
| | | 49.731 | 48.346 | 45.891 | 46.863 | 47.446 | | | | | | | | |
| 11 | VORN | 0.161 | 0.081 | 0.330 | 0.547 | 0.699 | | | | | | | | |
| | | -0.161 | -0.146 | -0.360 | -0.477 | -0.509 | | | | | | | | |
| | | -12.885 | 23.395 | 35.257 | 37.642 | 32.248 | | | | | | | | |
| 13 | VORN | 0.040 | 0.020 | 0.105 | 0.156 | 0.173 | | | | | | | | |
| | | -0.170 | -0.120 | -0.290 | -0.341 | -0.513 | | | | | | | | |
| | | -32.327 | 10.519 | 35.783 | 38.892 | 38.690 | | | | | | | | |

AUPTDEHNUNGEN DES BETONS

1. ZEILE = EPSILON MAX IN PROMILLE

2. ZEILE = EPSILON MIN IN PROMILLE

3. ZEILE = WINKEL ZWISCHEN EPSILON MIN UND DER LAENGSSACHSE

BELASTUNGSGRAD M/MU

| SCHNITT | LAGE | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.857 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
|---------|--------|---------|---------|--------|--------|--------|--------|-------|-------|-------|-------|-------|-------|-------|
| | | 7 | 9 | 11 | 13 | 15 | 16 | | | | | | | |
| 8 | HINTEN | -0.209 | -0.290 | -0.262 | -0.101 | 0.220 | 0.329 | | | | | | | |
| | | -1.286 | -1.380 | -1.628 | -2.009 | -2.385 | -2.574 | | | | | | | |
| | | 5.759 | 7.720 | 15.158 | 27.406 | 31.840 | 32.843 | | | | | | | |
| 11 | HINTEN | 0.013 | 0.009 | 0.076 | 0.500 | 1.053 | 1.202 | | | | | | | |
| | | -0.823 | -0.884 | -0.971 | -1.185 | -1.463 | -1.632 | | | | | | | |
| | | 10.519 | 14.932 | 21.146 | 27.943 | 29.577 | 29.501 | | | | | | | |
| 13 | HINTEN | 0.067 | 0.117 | 0.230 | 0.657 | 0.934 | 0.897 | | | | | | | |
| | | -0.437 | -0.477 | -0.575 | -0.667 | -0.734 | -0.792 | | | | | | | |
| | | 16.845 | 23.182 | 26.031 | 31.040 | 33.716 | 33.958 | | | | | | | |
| 1 | HINTEN | 0.843 | 1.116 | 1.628 | 2.139 | 2.463 | 2.551 | | | | | | | |
| | | -0.823 | -0.941 | -1.113 | -1.334 | -1.508 | -1.641 | | | | | | | |
| | | 25.912 | 27.749 | 26.952 | 30.296 | 32.766 | 34.074 | | | | | | | |
| 3 | HINTEN | 0.534 | 0.639 | 1.305 | 2.123 | 2.560 | 2.450 | | | | | | | |
| | | -0.784 | -0.854 | -1.035 | -1.213 | -1.285 | -1.360 | | | | | | | |
| | | 20.654 | 26.584 | 29.581 | 30.181 | 30.834 | 32.255 | | | | | | | |
| 8 | HINTEN | 0.085 | -0.012 | 0.247 | 1.891 | 2.885 | 3.070 | | | | | | | |
| | | -0.385 | -0.393 | -0.477 | -0.961 | -1.200 | -1.155 | | | | | | | |
| | | -1.218 | 21.970 | 34.907 | 42.385 | 44.474 | 45.170 | | | | | | | |
| 11 | HINTEN | 0.243 | 0.164 | 0.040 | 0.167 | 0.337 | 0.526 | | | | | | | |
| | | -0.708 | -0.734 | -0.675 | -0.767 | -0.837 | -0.906 | | | | | | | |
| | | -12.946 | -9.419 | 0.601 | 16.165 | 22.845 | 20.518 | | | | | | | |
| 13 | HINTEN | 0.193 | 0.063 | 0.070 | 0.059 | 0.077 | 0.075 | | | | | | | |
| | | -0.608 | -0.588 | -0.565 | -0.639 | -0.657 | -0.810 | | | | | | | |
| | | -16.895 | -12.004 | -1.127 | 12.732 | 16.953 | 21.126 | | | | | | | |

HAUPTDEHNUNGEN DES BETONS

1. ZEILE = EPSILON MAX IN PROMILLE

2. ZEILE = EPSILON MIN IN PROMILLE

3. ZEILE = WINKEL ZWISCHEN EPSILON MIN UND DER LAENGSSACHSE

BELASTUNGSGRAD M/MU

| SCHNITT | LAGE | 0.229 | 0.343 | 0.571 | 0.629 | 0.743 | 0.857 | 0.857 | 0.857 | 0.857 | 0.400 | 0.400 | 0.000 | 0.857 |
|---------|--------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|---------|---------|
| | | | | | | | | 1 | 3 | 6 | 1 | 3 | 3 | 7 |
| 1 | HINTEN | 0.516 | 0.145 | 0.379 | 0.319 | 0.206 | 0.360 | 0.414 | 0.281 | 0.186 | 0.078 | 0.117 | 0.357 | 0.459 |
| | | -0.041 | 0.075 | 0.181 | -0.039 | -0.031 | 0.225 | -0.089 | 0.119 | 0.039 | 0.027 | 0.003 | 0.083 | 0.165 |
| | | 18.515 | 40.935 | 15.233 | -58.283 | -48.036 | -25.505 | -65.888 | -41.437 | -49.891 | -30.473 | 52.628 | 39.754 | -55.807 |
| 3 | HINTEN | 0.007 | 0.081 | 0.125 | 0.080 | 0.121 | 0.237 | 0.217 | 0.145 | 0.032 | 0.000 | 0.002 | 0.086 | 0.206 |
| | | -0.072 | -0.026 | -0.075 | -0.155 | -0.181 | -0.177 | -0.167 | -0.245 | -0.252 | -0.120 | -0.162 | -0.023 | -0.201 |
| | | -54.217 | -49.065 | -46.431 | -43.174 | -42.145 | -40.837 | -37.438 | -38.338 | -39.938 | -2.382 | 18.784 | 9.217 | -35.338 |
| 5 | HINTEN | -0.007 | 0.034 | 0.140 | 0.070 | 0.072 | 0.230 | 0.170 | 0.014 | 0.205 | 0.137 | 0.165 | -0.035 | 0.115 |
| | | -0.123 | -0.179 | -0.045 | -0.095 | -0.172 | -0.040 | -0.070 | -0.109 | -0.170 | -0.262 | -0.240 | -0.085 | -0.005 |
| | | -60.482 | -64.645 | -47.318 | -47.597 | -40.269 | -47.118 | -47.382 | -60.880 | 45.382 | 41.037 | 30.610 | -45.000 | -32.778 |
| 7 | HINTEN | -0.006 | 0.010 | 0.052 | -0.010 | -0.038 | 0.050 | 0.046 | 0.051 | 0.040 | 0.069 | 0.059 | 0.081 | 0.100 |
| | | -0.064 | -0.055 | 0.013 | -0.080 | -0.052 | -0.055 | 0.024 | -0.096 | -0.105 | -0.174 | -0.204 | -0.041 | -0.030 |
| | | -29.518 | -2.199 | 33.401 | -40.935 | -22.500 | -43.637 | 31.717 | 40.109 | 42.047 | 26.683 | 29.518 | 27.504 | 47.199 |
| 1 | OBEN | -0.089 | 0.035 | 0.106 | 0.107 | 0.088 | 0.129 | 0.039 | -0.002 | 0.093 | 0.295 | 0.216 | 0.147 | -0.003 |
| | | -0.196 | -0.055 | -0.046 | -0.167 | -0.193 | -0.159 | -0.109 | -0.163 | -0.233 | -0.300 | -0.341 | -0.037 | -0.147 |
| | | -51.696 | -0.000 | 5.655 | 11.875 | 9.861 | 7.018 | -9.827 | 8.095 | 21.255 | 37.457 | 39.042 | 38.736 | 12.388 |
| 3 | OBEN | 0.025 | 0.019 | 0.114 | 0.085 | 0.060 | 0.118 | 0.153 | 0.096 | 0.132 | 0.113 | 0.098 | 0.146 | 0.134 |
| | | -0.130 | -0.184 | -0.159 | -0.375 | -0.460 | -0.528 | -0.473 | -0.546 | -0.587 | -0.368 | -0.413 | -0.041 | -0.529 |
| | | 10.586 | -7.876 | 6.891 | -0.623 | -0.551 | -4.002 | -3.676 | 1.788 | 11.233 | 17.423 | 20.514 | 17.057 | 4.554 |
| 7 | OBEN | 0.012 | 0.050 | 0.102 | 0.061 | 0.065 | 0.165 | 0.190 | 0.174 | 0.099 | 0.101 | 0.101 | 0.139 | 0.161 |
| | | -0.242 | -0.320 | -0.387 | -0.671 | -0.860 | -1.025 | -1.125 | -1.209 | -1.384 | -0.841 | -0.921 | -0.229 | -1.266 |
| | | -4.545 | -1.547 | -3.235 | -1.959 | 0.465 | 0.722 | -0.109 | 3.010 | 4.557 | 8.641 | 11.526 | 11.190 | 1.707 |

HAUPTDEHNUNGEN DES BETONS

1. ZEILE = EPSILON MAX IN PROMILLE

2. ZEILE = EPSILON MIN IN PROMILLE

3. ZEILE = WINKEL ZWISCHEN EPSILON MIN UND DER LAENGSSACHSE

BELASTUNGSGRAD M/MU

| SCHNITT | LAGE | 0.000 | 0.229 | 0.343 | 0.571 | 0.629 | 0.743 | 0.857 | 0.857 | 0.857 | 0.857 | 0.400 | 0.400 | 0.000 |
|---------|--------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|--------|--------|
| | | | | | | | | | 1 | 3 | 6 | 1 | 3 | 3 |
| 8 | HINTEN | -0.104 | -0.155 | -0.100 | -0.092 | -0.185 | -0.239 | -0.149 | -0.160 | -0.188 | -0.208 | -0.134 | -0.185 | -0.101 |
| | | -0.231 | -0.410 | -0.465 | -0.418 | -0.745 | -0.976 | -1.056 | -1.150 | -1.237 | -1.422 | -0.956 | -1.000 | -0.449 |
| | | -5.655 | 0.562 | 6.733 | 8.939 | 5.655 | 2.527 | 4.601 | 0.868 | 6.190 | 11.909 | 18.296 | 18.259 | 19.587 |
| 11 | HINTEN | -0.034 | -0.041 | 0.032 | 0.042 | -0.024 | -0.021 | 0.033 | 0.060 | 0.007 | 0.017 | 0.012 | 0.019 | 0.045 |
| | | -0.176 | -0.344 | -0.417 | -0.462 | -0.661 | -0.749 | -0.733 | -0.735 | -0.812 | -0.917 | -0.682 | -0.724 | -0.275 |
| | | 19.645 | 12.222 | 12.855 | 6.880 | 5.655 | 6.350 | 6.021 | 6.362 | 8.333 | 13.694 | 18.105 | 22.500 | 19.330 |
| 13 | HINTEN | 0.026 | -0.039 | -0.004 | 0.065 | 0.022 | 0.001 | 0.074 | 0.067 | 0.069 | 0.107 | 0.099 | 0.079 | 0.056 |
| | | -0.171 | -0.216 | -0.231 | -0.250 | -0.362 | -0.391 | -0.364 | -0.382 | -0.459 | -0.517 | -0.554 | -0.444 | -0.146 |
| | | 41.347 | 14.370 | 15.265 | 17.980 | 13.949 | 7.372 | 12.114 | 7.404 | 14.738 | 24.450 | 22.948 | 29.142 | 28.547 |
| 1 | HINTEN | 0.024 | 0.060 | 0.061 | 0.049 | -0.046 | 0.126 | 0.201 | 0.237 | 0.483 | 1.062 | 0.858 | 1.027 | 0.401 |
| | | -0.584 | -0.400 | -0.376 | -0.349 | -0.419 | -0.496 | -0.486 | -0.497 | -0.633 | -0.902 | -0.768 | -0.922 | -0.506 |
| | | 12.538 | 15.561 | 15.482 | 8.763 | 13.111 | 21.199 | 20.730 | 28.047 | 25.590 | 26.536 | 27.129 | 27.727 | 20.469 |
| 3 | HINTEN | 0.010 | 0.007 | 0.060 | 0.028 | -0.108 | 0.046 | 0.134 | 0.146 | 0.220 | 0.648 | 0.411 | 0.622 | 0.307 |
| | | -0.550 | -0.517 | -0.560 | -0.553 | -0.622 | -0.656 | -0.614 | -0.606 | -0.705 | -0.848 | -0.736 | -0.832 | -0.562 |
| | | 0.512 | 6.620 | 7.466 | 6.719 | 3.908 | 9.992 | 14.825 | 13.453 | 14.738 | 24.803 | 24.090 | 27.827 | 16.160 |
| 8 | HINTEN | -0.055 | -0.067 | -0.155 | -0.076 | -0.023 | -0.182 | -0.015 | -0.089 | 0.006 | -0.107 | -0.150 | -0.210 | -0.043 |
| | | -0.470 | -0.563 | -0.475 | -0.599 | -0.482 | -0.563 | -0.450 | -0.411 | -0.446 | -0.363 | -0.465 | -0.530 | -0.482 |
| | | -15.600 | -21.682 | -19.330 | -27.167 | -7.245 | -23.030 | -16.387 | -12.885 | -9.017 | 29.710 | 14.704 | 16.098 | -3.603 |
| 11 | HINTEN | 0.005 | -0.031 | 0.011 | -0.007 | 0.066 | 0.074 | 0.184 | 0.111 | 0.162 | 0.099 | 0.062 | 0.091 | 0.079 |
| | | -0.575 | -0.624 | -0.571 | -0.618 | -0.646 | -0.724 | -0.669 | -0.706 | -0.712 | -0.714 | -0.677 | -0.686 | -0.564 |
| | | -7.498 | -11.663 | -7.973 | -17.170 | -12.922 | -17.143 | -11.555 | -24.985 | -11.815 | -11.784 | -3.298 | -2.397 | -6.964 |
| 13 | HINTEN | 0.058 | 0.039 | 0.093 | 0.094 | 0.023 | 0.100 | 0.142 | 0.142 | 0.181 | 0.077 | 0.011 | -0.034 | 0.109 |
| | | -0.453 | -0.454 | -0.503 | -0.454 | -0.583 | -0.545 | -0.532 | -0.617 | -0.596 | -0.537 | -0.486 | -0.526 | -0.459 |
| | | -7.933 | -11.347 | -10.706 | -18.813 | -16.167 | -20.393 | -29.777 | -14.850 | -10.987 | -2.597 | 2.913 | 0.012 | 20.445 |

HAUPTDEHNUNGEN DES BETONS

- 1. ZEILE = EPSILON MAX IN PROMILLE
- 2. ZEILE = EPSILON MIN IN PROMILLE
- 3. ZEILE = WINKEL ZWISCHEN EPSILON MIN UND DER LAENGSSACHSE

BELASTUNGSGRAD M/MU

| SCHNITT | LAGE | 0.000 | 0.229 | 0.343 | 0.571 | 0.629 | 0.743 | 0.857 | 0.857 | 0.857 | 0.857 | 0.400 | 0.400 | 0.000 |
|---------|--------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|
| | | | | | | | | | 1 | 3 | 6 | 1 | 3 | 3 |
| 1 | HINTEN | 0.016 | 0.247 | 0.113 | 0.349 | 0.221 | 0.173 | 0.374 | 0.235 | 0.274 | 0.165 | 0.092 | 0.036 | 0.209 |
| | | -0.646 | -0.602 | -0.523 | -0.419 | -0.571 | -0.628 | -0.419 | -0.540 | -0.504 | -0.570 | -0.617 | -0.546 | -0.399 |
| | | -16.965 | -5.258 | -14.089 | -10.278 | -30.262 | -24.525 | -18.399 | -36.951 | -21.459 | -22.225 | -17.910 | -13.283 | -4.731 |
| 3 | HINTEN | 0.080 | 0.039 | 0.106 | 0.119 | 0.075 | 0.102 | 0.203 | 0.205 | 0.128 | 0.027 | 0.080 | 0.067 | 0.165 |
| | | -0.515 | -0.539 | -0.486 | -0.504 | -0.585 | -0.597 | -0.578 | -0.590 | -0.663 | -0.682 | -0.635 | -0.662 | -0.535 |
| | | -0.722 | -4.486 | -5.845 | -10.090 | -11.143 | -13.374 | -16.489 | -14.492 | -14.985 | -12.289 | -1.001 | 3.343 | 0.818 |
| 5 | HINTEN | 0.030 | -0.062 | -0.099 | 0.081 | 0.019 | 0.019 | 0.142 | 0.091 | -0.047 | 0.114 | 0.064 | 0.138 | -0.030 |
| | | -0.500 | -0.538 | -0.516 | -0.456 | -0.514 | -0.589 | -0.422 | -0.461 | -0.518 | -0.549 | -0.659 | -0.683 | -0.560 |
| | | 1.620 | -4.236 | -9.435 | -8.375 | -7.344 | -10.112 | -12.601 | -11.190 | -4.581 | 18.824 | 17.999 | 13.965 | -1.061 |
| 7 | HINTEN | 0.071 | 0.050 | 0.081 | 0.110 | 0.030 | 0.031 | 0.072 | 0.113 | 0.079 | 0.064 | 0.114 | 0.095 | 0.135 |
| | | -0.401 | -0.450 | -0.456 | -0.375 | -0.450 | -0.451 | -0.407 | -0.373 | -0.454 | -0.459 | -0.549 | -0.570 | -0.425 |
| | | 3.036 | -0.000 | 2.404 | 0.866 | -1.193 | 2.382 | -3.302 | 4.149 | 10.751 | 10.952 | 10.861 | 12.222 | 7.762 |
| 1 | HINTEN | 0.061 | -0.047 | 0.089 | 0.151 | 0.135 | 0.120 | 0.166 | 0.098 | 0.039 | 0.097 | 0.242 | 0.159 | 0.121 |
| | | -0.116 | -0.293 | -0.164 | -0.146 | -0.250 | -0.280 | -0.251 | -0.223 | -0.259 | -0.292 | -0.302 | -0.339 | -0.066 |
| | | -20.213 | -31.717 | -13.536 | -8.303 | -0.372 | -1.431 | -3.094 | -15.482 | -6.785 | 7.821 | 28.886 | 29.913 | 10.188 |
| 3 | HINTEN | -0.044 | -0.059 | -0.044 | 0.030 | 0.010 | -0.016 | 0.046 | 0.081 | 0.016 | 0.038 | 0.011 | -0.009 | 0.051 |
| | | -0.131 | -0.221 | -0.296 | -0.250 | -0.475 | -0.559 | -0.631 | -0.576 | -0.641 | -0.668 | -0.441 | -0.481 | -0.121 |
| | | -39.996 | -5.310 | -16.845 | -2.043 | -5.655 | -5.035 | -7.479 | -7.283 | -1.965 | 7.805 | 12.432 | 16.003 | 3.555 |
| 7 | HINTEN | -0.073 | -0.070 | -0.029 | 0.020 | -0.020 | -0.014 | 0.087 | 0.111 | 0.097 | 0.024 | 0.028 | 0.028 | 0.066 |
| | | -0.207 | -0.440 | -0.521 | -0.585 | -0.870 | -1.061 | -1.227 | -1.326 | -1.412 | -1.589 | -1.048 | -1.128 | -0.436 |
| | | 13.283 | 1.547 | 2.333 | 0.237 | 0.337 | 2.053 | 1.965 | 1.097 | 3.904 | 5.272 | 9.217 | 11.730 | 11.749 |

HAUPTDEHNUNGEN DES BETONS

1. ZEILE = EPSILON MAX IN PROMILLE

2. ZEILE = EPSILON MIN IN PROMILLE

3. ZEILE = WINKEL ZWISCHEN EPSILON MIN UND DER LAENGSSACHSE

BELASTUNGSGRAD M/MU

| SCHNITT | LAGE | 0.229 | 0.343 | 0.571 | 0.629 | 0.743 | 0.857 | 0.857 | 0.857 | 0.857 | 0.400 | 0.400 | 0.000 | 0.857 |
|---------|------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|--------|--------|------------|
| | | | | | | | | ----- | ----- | ----- | ----- | ----- | ----- | ----- |
| | | | | | | | | 1 | 3 | 6 | 1 | 3 | 3 | 7 |
| 8 | OBEN | -0.048 | 0.012 | 0.024 | -0.075 | -0.132 | -0.041 | -0.054 | -0.078 | -0.092 | -0.006 | -0.057 | 0.035 | -0.100 |
| | | -0.182 | -0.242 | -0.199 | -0.520 | -0.748 | -0.829 | -0.921 | -1.012 | -1.203 | -0.749 | -0.793 | -0.250 | -1.060 |
| | | 6.497 | 12.780 | 17.023 | 8.811 | 4.196 | 6.225 | 1.819 | 7.762 | 13.801 | 21.954 | 21.949 | 29.691 | 7.235 |
| 11 | OBEN | -0.003 | 0.069 | 0.086 | 0.021 | 0.022 | 0.077 | 0.103 | 0.048 | 0.053 | 0.046 | 0.053 | 0.079 | 0.051 |
| | | -0.172 | -0.244 | -0.296 | -0.496 | -0.582 | -0.567 | -0.568 | -0.643 | -0.743 | -0.506 | -0.548 | -0.099 | -0.651 |
| | | 5.988 | 9.796 | 2.257 | 1.944 | 3.327 | 3.121 | 3.642 | 6.062 | 12.639 | 17.709 | 23.174 | 19.079 | 8.701 |
| 13 | OBEN | 0.030 | 0.049 | 0.095 | 0.060 | 0.061 | 0.115 | 0.124 | 0.097 | 0.104 | 0.104 | 0.067 | 0.072 | 0.090 |
| | | -0.140 | -0.139 | -0.135 | -0.255 | -0.306 | -0.260 | -0.294 | -0.342 | -0.369 | -0.214 | -0.287 | -0.017 | -0.315 |
| | | -20.118 | -12.601 | -1.245 | -1.363 | -7.491 | -1.145 | -5.520 | 4.249 | 17.769 | 12.073 | 22.500 | -8.195 | 6.072 |
| 1 | VORN | 0.038 | 0.050 | 0.055 | -0.035 | 0.128 | 0.197 | 0.271 | 0.492 | 1.069 | 0.869 | 1.039 | 0.392 | 0.849 |
| | | -0.018 | -0.005 | 0.005 | -0.070 | -0.138 | -0.122 | -0.171 | -0.282 | -0.549 | -0.419 | -0.574 | -0.137 | -0.469 |
| | | 22.500 | 42.403 | 39.345 | 85.935 | 35.101 | 31.517 | 42.403 | 32.380 | 29.974 | 31.618 | 31.439 | 26.728 | 29.966 |
| 3 | VORN | 0.075 | 0.098 | 0.070 | -0.056 | 0.090 | 0.216 | 0.214 | 0.281 | 0.771 | 0.542 | 0.774 | 0.386 | 0.626 |
| | | -0.045 | -0.058 | -0.055 | -0.134 | -0.160 | -0.156 | -0.134 | -0.226 | -0.431 | -0.327 | -0.444 | -0.101 | -0.336 |
| | | 57.222 | 37.534 | 43.855 | 64.903 | 33.251 | 37.982 | 35.783 | 30.582 | 35.029 | 38.182 | 38.838 | 34.481 | 31.717 |
| 8 | VORN | 0.010 | 0.001 | 0.033 | 0.077 | -0.056 | 0.041 | 0.062 | 0.096 | 0.272 | 0.144 | 0.090 | 0.089 | 0.226 |
| | | -0.115 | -0.106 | -0.183 | -0.057 | -0.164 | 0.019 | -0.037 | -0.011 | -0.217 | -0.234 | -0.305 | -0.089 | -0.001 |
| | | -43.855 | 85.935 | -51.696 | 24.006 | -73.155 | -31.717 | 65.457 | 22.500 | 58.675 | 51.100 | 51.225 | 31.717 | 29.735 |
| 11 | VORN | 0.001 | 0.010 | 0.074 | 0.084 | 0.118 | 0.188 | 0.226 | 0.166 | 0.105 | 0.071 | 0.103 | 0.075 | 0.251 |
| | | -0.086 | -0.000 | -0.129 | -0.094 | -0.198 | -0.103 | -0.251 | -0.146 | -0.150 | -0.116 | -0.128 | 0.010 | -0.146 |
| | | -50.004 | -45.000 | -52.876 | -31.717 | -35.783 | -19.714 | -47.107 | -19.903 | -21.704 | 10.188 | 10.786 | -2.199 | -20.967 |
| 13 | VORN | 0.024 | 0.073 | 0.080 | 0.066 | 0.111 | 0.185 | 0.256 | 0.167 | 0.052 | -0.024 | -0.020 | 0.051 | 0.192 |
| | | -0.044 | -0.088 | -0.045 | -0.231 | -0.161 | -0.180 | -0.336 | -0.187 | -0.117 | -0.056 | -0.145 | -0.006 | -0.212 |
| | | 38.243 | 36.905 | 43.855 | 47.422 | 40.787 | 44.608 | 50.845 | 30.630 | 33.625 | 54.217 | 48.421 | -7.198 | 98/01/2014 |

Balkenverformungen

WINKEL PHI (HOENMASZ)

| M | T | M/MU | T/TU | VERDREHUNG IM SCHNITT | | | | |
|-------|-------|-------|-------|-----------------------|------------|------------|------------|------------|
| (KNM) | (KNM) | ---- | ---- | I | V | VII | X | XIV |
| 80.0 | 0.0 | 0.114 | 0.000 | 0.0004908 | 0.0003455 | 0.0004363 | 0.0004181 | 0.0003819 |
| 160.0 | 0.0 | 0.229 | 0.000 | 0.0001818 | 0.0000182 | 0.0001455 | 0.0002364 | 0.0001091 |
| 160.0 | 0.0 | 0.229 | 0.000 | 0.0001273 | -0.0000727 | 0.0000546 | 0.0003092 | -0.0000181 |
| 240.0 | 0.0 | 0.343 | 0.000 | 0.0001273 | -0.0000727 | 0.0001637 | 0.0004183 | 0.0000162 |
| 280.0 | 0.0 | 0.400 | 0.000 | 0.0001455 | -0.0000546 | 0.0002000 | 0.0004363 | 0.0000545 |
| 320.0 | 0.0 | 0.457 | 0.000 | 0.0001273 | -0.0000909 | 0.0002364 | 0.0002909 | 0.0000727 |
| 360.0 | 0.0 | 0.514 | 0.000 | 0.0001637 | -0.0000728 | 0.0002545 | 0.0003091 | 0.0000727 |
| 400.0 | 0.0 | 0.571 | 0.000 | 0.0001455 | -0.0001091 | 0.0002728 | 0.0003273 | 0.0000728 |
| 440.0 | 0.0 | 0.629 | 0.000 | 0.0001455 | -0.0001273 | 0.0003091 | 0.0003092 | 0.0000728 |
| 480.0 | 0.0 | 0.686 | 0.000 | 0.0001273 | -0.0001456 | 0.0003272 | 0.0003618 | 0.0000363 |
| 520.0 | 0.0 | 0.743 | 0.000 | 0.0000910 | -0.0001636 | 0.0003453 | 0.0004362 | 0.0000182 |
| 560.0 | 0.0 | 0.800 | 0.000 | 0.0000547 | -0.0001455 | 0.0003454 | 0.0006544 | -0.0000000 |
| 600.0 | 0.0 | 0.857 | 0.000 | 0.0000182 | -0.0001454 | 0.0003618 | 0.0003272 | -0.0000182 |
| 0.0 | 0.0 | 0.000 | 0.000 | -0.0000546 | -0.0000000 | 0.0000546 | 0.0007454 | -0.0000364 |
| 600.0 | 0.0 | 0.857 | 0.000 | 0.0001092 | -0.0000000 | 0.0004181 | 0.0016181 | 0.0000547 |
| 600.0 | 16.0 | 0.857 | 0.067 | 0.0003092 | 0.0000726 | 0.0004362 | 0.0022180 | -0.0002364 |
| 600.0 | 32.0 | 0.857 | 0.133 | 0.0005454 | 0.0001636 | 0.0003454 | 0.0012180 | -0.0006182 |
| 600.0 | 48.0 | 0.857 | 0.200 | 0.0010364 | 0.0003091 | 0.0002000 | -0.0007273 | -0.0012183 |
| 600.0 | 64.0 | 0.857 | 0.267 | 0.0012365 | 0.0001818 | -0.0002000 | -0.0009638 | -0.0020364 |
| 600.0 | 80.0 | 0.857 | 0.333 | 0.0018727 | 0.0005273 | -0.0003455 | -0.0012728 | -0.0027819 |
| 480.0 | 80.0 | 0.686 | 0.333 | 0.0018907 | 0.0004182 | -0.0004546 | -0.0013091 | -0.0023729 |
| 400.0 | 80.0 | 0.571 | 0.333 | 0.0018727 | 0.0002909 | -0.0004728 | -0.0012544 | -0.0026183 |
| 280.0 | 80.0 | 0.400 | 0.333 | 0.0017455 | 0.0002364 | -0.0004545 | -0.0012000 | -0.0026910 |
| 280.0 | 96.0 | 0.400 | 0.400 | 0.0019819 | 0.0002364 | -0.0005091 | -0.0012728 | -0.0029819 |
| 280.0 | 112.0 | 0.400 | 0.467 | 0.0020909 | 0.0002728 | -0.0006546 | -0.0015636 | -0.0033818 |
| 70.0 | 112.0 | 0.100 | 0.467 | 0.0023455 | 0.0004181 | -0.0006727 | -0.0017454 | -0.0033636 |
| 0.0 | 0.0 | 0.000 | 0.000 | 0.0007271 | 0.0001455 | -0.0002546 | 0.0001272 | -0.0010363 |
| 500.0 | 0.0 | 0.429 | 0.000 | 0.0010546 | 0.0002364 | -0.0000001 | 0.0000363 | -0.0008727 |
| 600.0 | 0.0 | 0.857 | 0.000 | 0.0009637 | 0.0001453 | 0.0000545 | 0.0006544 | -0.0010728 |
| 600.0 | 32.0 | 0.857 | 0.133 | 0.0010364 | -0.0000546 | -0.0006001 | -0.0011635 | -0.0023636 |
| 600.0 | 64.0 | 0.857 | 0.267 | 0.0015092 | 0.0000909 | -0.0009454 | -0.0020182 | -0.0033636 |
| 600.0 | 96.0 | 0.857 | 0.400 | 0.0027636 | 0.0009273 | -0.0009272 | -0.0026364 | -0.0045637 |
| 600.0 | 128.0 | 0.857 | 0.533 | 0.0047454 | 0.0018910 | -0.0013455 | -0.0040366 | -0.0068183 |
| 600.0 | 160.0 | 0.857 | 0.667 | 0.0074546 | 0.0029818 | -0.0020728 | -0.0062911 | -0.0103278 |
| 600.0 | 192.0 | 0.857 | 0.800 | 0.0121101 | 0.0068363 | -0.0017455 | -0.0078368 | -0.0137647 |
| 600.0 | 208.0 | 0.857 | 0.867 | 0.0139474 | 0.0058910 | -0.0035818 | -0.0133648 | -0.0182208 |
| 600.0 | 224.0 | 0.857 | 0.933 | 0.0170580 | 0.0079276 | -0.0030001 | -0.0122740 | -0.0196033 |
| 600.0 | 240.0 | 0.857 | 1.000 | 0.0190593 | 0.0089639 | -0.0037273 | -0.0152927 | -0.0221321 |
| 660.0 | 240.0 | 0.943 | 1.000 | 0.0233361 | 0.0120186 | -0.0048909 | -0.0182948 | -0.0266629 |
| 700.0 | 240.0 | 1.000 | 1.000 | 0.0350298 | 0.0237126 | 0.0005818 | -0.0273982 | -0.0365519 |

ERMITTLUNG DER DURCHBIEGUNG
BEIM VERSUCHSBALKEN SEIMQ1

VERSUCH VOM 19. MAI 1970

DURCHBIEGUNG V (MM)

| M | I | M/MU | I/IU | DURCHBIEGUNG IM SCHNITT | | | | |
|-------|-------|-------|-------|-------------------------|--------|--------|--------|--------|
| (KNM) | (KNM) | ---- | ---- | I | V | VII | X | XIV |
| 80.0 | 0.0 | 0.114 | 0.000 | 0.365 | 1.085 | 1.210 | 1.075 | 0.385 |
| 160.0 | 0.0 | 0.229 | 0.000 | 0.770 | 2.284 | 2.550 | 2.245 | 0.790 |
| 160.0 | 0.0 | 0.229 | 0.000 | 0.795 | 2.361 | 2.644 | 2.285 | 0.817 |
| 240.0 | 0.0 | 0.343 | 0.000 | 1.175 | 3.521 | 3.955 | 3.435 | 1.193 |
| 280.0 | 0.0 | 0.409 | 0.000 | 1.420 | 4.276 | 4.795 | 4.180 | 1.434 |
| 320.0 | 0.0 | 0.457 | 0.000 | 1.625 | 4.885 | 5.505 | 4.860 | 1.640 |
| 360.0 | 0.0 | 0.514 | 0.000 | 1.865 | 5.661 | 6.380 | 5.625 | 1.890 |
| 400.0 | 0.0 | 0.571 | 0.000 | 2.080 | 6.341 | 7.155 | 6.310 | 2.100 |
| 440.0 | 0.0 | 0.629 | 0.000 | 2.330 | 7.125 | 8.045 | 7.095 | 2.340 |
| 480.0 | 0.0 | 0.686 | 0.000 | 2.615 | 8.061 | 9.140 | 7.950 | 2.629 |
| 520.0 | 0.0 | 0.743 | 0.000 | 2.905 | 9.066 | 10.305 | 8.980 | 2.913 |
| 560.0 | 0.0 | 0.800 | 0.000 | 3.284 | 10.391 | 11.875 | 10.230 | 2.794 |
| 600.0 | 0.0 | 0.857 | 0.000 | 3.692 | 11.851 | 13.635 | 11.760 | 3.708 |
| 0.0 | 0.0 | 0.000 | 0.000 | 0.545 | 6.579 | 1.784 | 1.355 | 0.481 |
| 600.0 | 0.0 | 0.857 | 0.000 | 3.800 | 10.566 | 14.105 | 11.775 | 3.794 |
| 600.0 | 16.0 | 0.857 | 0.067 | 3.975 | 12.769 | 14.731 | 12.091 | 3.955 |
| 600.0 | 32.0 | 0.857 | 0.133 | 4.020 | 12.915 | 14.885 | 12.446 | 4.000 |
| 600.0 | 48.0 | 0.857 | 0.200 | 4.175 | 13.455 | 15.505 | 12.841 | 4.156 |
| 600.0 | 64.0 | 0.857 | 0.267 | 4.270 | 13.730 | 15.796 | 13.147 | 4.231 |
| 600.0 | 80.0 | 0.857 | 0.333 | 4.395 | 14.215 | 16.347 | 13.613 | 4.347 |
| 480.0 | 80.0 | 0.686 | 0.333 | 3.800 | 12.135 | 13.896 | 11.892 | 3.742 |
| 400.0 | 80.0 | 0.571 | 0.333 | 3.365 | 10.560 | 12.051 | 10.347 | 3.287 |
| 280.0 | 80.0 | 0.409 | 0.333 | 2.710 | 8.325 | 9.456 | 8.141 | 2.621 |
| 280.0 | 96.0 | 0.409 | 0.400 | 2.675 | 8.265 | 9.381 | 8.051 | 2.612 |
| 280.0 | 112.0 | 0.409 | 0.467 | 2.705 | 8.275 | 9.381 | 8.081 | 2.612 |
| 70.0 | 112.0 | 0.100 | 0.467 | 1.595 | 4.795 | 5.416 | 4.651 | 1.537 |
| 0.0 | 0.0 | 0.000 | 0.000 | 0.810 | 2.550 | 2.921 | 2.285 | 0.745 |
| 300.0 | 0.0 | 0.429 | 0.000 | 2.260 | 6.995 | 11.327 | 6.818 | 2.220 |
| 600.0 | 0.0 | 0.857 | 0.000 | 4.155 | 13.530 | 15.583 | 13.101 | 4.136 |
| 600.0 | 32.0 | 0.857 | 0.133 | 4.315 | 13.968 | 16.067 | 13.323 | 4.271 |
| 600.0 | 64.0 | 0.857 | 0.267 | 4.425 | 14.255 | 16.381 | 14.077 | 4.347 |
| 600.0 | 96.0 | 0.857 | 0.400 | 4.701 | 15.115 | 17.406 | 14.928 | 4.579 |
| 600.0 | 128.0 | 0.857 | 0.533 | 5.069 | 16.540 | 19.052 | 16.266 | 4.932 |
| 600.0 | 160.0 | 0.857 | 0.667 | 5.563 | 18.550 | 21.342 | 18.202 | 5.445 |
| 600.0 | 192.0 | 0.857 | 0.800 | 6.276 | 20.804 | 24.442 | 20.784 | 6.122 |
| 600.0 | 208.0 | 0.857 | 0.867 | 6.715 | 23.076 | 26.836 | 23.266 | 6.633 |
| 600.0 | 224.0 | 0.857 | 0.933 | 7.032 | 24.328 | 28.298 | 24.058 | 6.951 |
| 600.0 | 240.0 | 0.857 | 1.000 | 7.369 | 25.636 | 29.877 | 25.700 | 7.278 |
| 660.0 | 240.0 | 0.943 | 1.000 | 8.560 | 30.438 | 35.733 | 30.403 | 8.561 |
| 700.0 | 240.0 | 1.000 | 1.000 | 10.873 | 40.321 | 46.985 | 40.623 | 11.079 |

AUSWERTUNG VOM 9.6.1978

ERMITTLUNG DER VERDREHUNG

BEIM VERSUCHSBALKEN SEITE 1

VERSUCH VON 19. MAI 1978

WINKEL THETA (1/CM)

| M | T | H/MU | T/TU | VERDREHUNG ZWISCHEN SCHNITT | | | |
|-------|-------|-------|-------|-----------------------------|------------|------------|-----------|
| (KNM) | (KNM) | ---- | ---- | I UND V | V UND VII | VII UND X | X UND XIV |
| 80.0 | 0.0 | 0.114 | 0.000 | 0.0000010 | -0.0000009 | 0.0000002 | 0.0000002 |
| 160.0 | 0.0 | 0.229 | 0.000 | 0.0000011 | -0.0000013 | -0.0000009 | 0.0000008 |
| 160.0 | 0.0 | 0.229 | 0.000 | 0.0000013 | -0.0000013 | -0.0000025 | 0.0000022 |
| 240.0 | 0.0 | 0.343 | 0.000 | 0.0000013 | -0.0000024 | -0.0000025 | 0.0000027 |
| 280.0 | 0.0 | 0.400 | 0.000 | 0.0000013 | -0.0000025 | -0.0000024 | 0.0000025 |
| 320.0 | 0.0 | 0.457 | 0.000 | 0.0000015 | -0.0000033 | -0.0000005 | 0.0000015 |
| 360.0 | 0.0 | 0.514 | 0.000 | 0.0000016 | -0.0000033 | -0.0000005 | 0.0000016 |
| 400.0 | 0.0 | 0.571 | 0.000 | 0.0000017 | -0.0000038 | -0.0000005 | 0.0000017 |
| 440.0 | 0.0 | 0.629 | 0.000 | 0.0000018 | -0.0000044 | -0.0000000 | 0.0000016 |
| 480.0 | 0.0 | 0.686 | 0.000 | 0.0000018 | -0.0000047 | -0.0000025 | 0.0000036 |
| 520.0 | 0.0 | 0.743 | 0.000 | 0.0000017 | -0.0000051 | -0.0000009 | 0.0000028 |
| 560.0 | 0.0 | 0.800 | 0.000 | 0.0000013 | -0.0000049 | -0.0000031 | 0.0000044 |
| 600.0 | 0.0 | 0.857 | 0.000 | 0.0000011 | -0.0000053 | 0.0000005 | 0.0000023 |
| 0.0 | 0.0 | 0.000 | 0.000 | -0.0000004 | -0.0000005 | -0.0000069 | 0.0000052 |
| 600.0 | 0.0 | 0.857 | 0.000 | 0.0000007 | -0.0000042 | -0.0000120 | 0.0000104 |
| 600.0 | 16.0 | 0.857 | 0.067 | 0.0000016 | -0.0000036 | -0.0000178 | 0.0000164 |
| 600.0 | 32.0 | 0.857 | 0.133 | 0.0000025 | -0.0000018 | -0.0000087 | 0.0000122 |
| 600.0 | 48.0 | 0.857 | 0.200 | 0.0000048 | 0.0000011 | 0.0000093 | 0.0000033 |
| 600.0 | 64.0 | 0.857 | 0.267 | 0.0000070 | 0.0000038 | 0.0000076 | 0.0000072 |
| 600.0 | 80.0 | 0.857 | 0.333 | 0.0000090 | 0.0000087 | 0.0000093 | 0.0000101 |
| 480.0 | 80.0 | 0.686 | 0.333 | 0.0000098 | 0.0000087 | 0.0000085 | 0.0000104 |
| 400.0 | 80.0 | 0.571 | 0.333 | 0.0000105 | 0.0000076 | 0.0000078 | 0.0000104 |
| 280.0 | 80.0 | 0.400 | 0.333 | 0.0000101 | 0.0000069 | 0.0000075 | 0.0000099 |
| 280.0 | 96.0 | 0.400 | 0.400 | 0.0000116 | 0.0000075 | 0.0000076 | 0.0000114 |
| 280.0 | 112.0 | 0.400 | 0.467 | 0.0000121 | 0.0000093 | 0.0000091 | 0.0000121 |
| 70.0 | 112.0 | 0.100 | 0.467 | 0.0000128 | 0.0000109 | 0.0000107 | 0.0000108 |
| 0.0 | 0.0 | 0.000 | 0.000 | 0.0000039 | 0.0000040 | -0.0000038 | 0.0000078 |
| 300.0 | 0.0 | 0.429 | 0.000 | 0.0000055 | 0.0000024 | -0.0000004 | 0.0000061 |
| 600.0 | 0.0 | 0.857 | 0.000 | 0.0000055 | 0.0000009 | -0.0000060 | 0.0000115 |
| 600.0 | 32.0 | 0.857 | 0.133 | 0.0000073 | 0.0000055 | 0.0000056 | 0.0000080 |
| 600.0 | 64.0 | 0.857 | 0.267 | 0.0000095 | 0.0000104 | 0.0000107 | 0.0000090 |
| 600.0 | 96.0 | 0.857 | 0.400 | 0.0000122 | 0.0000185 | 0.0000171 | 0.0000128 |
| 600.0 | 128.0 | 0.857 | 0.533 | 0.0000190 | 0.0000324 | 0.0000269 | 0.0000185 |
| 600.0 | 160.0 | 0.857 | 0.667 | 0.0000298 | 0.0000505 | 0.0000422 | 0.0000269 |
| 600.0 | 192.0 | 0.857 | 0.800 | 0.0000352 | 0.0000858 | 0.0000609 | 0.0000395 |
| 600.0 | 208.0 | 0.857 | 0.867 | 0.0000537 | 0.0000947 | 0.0000978 | 0.0000324 |
| 600.0 | 224.0 | 0.857 | 0.933 | 0.0000609 | 0.0001093 | 0.0000927 | 0.0000469 |
| 600.0 | 240.0 | 0.857 | 1.000 | 0.0000673 | 0.0001269 | 0.0001157 | 0.0000456 |
| 660.0 | 240.0 | 0.943 | 1.000 | 0.0000754 | 0.0001691 | 0.0001340 | 0.0000558 |
| 700.0 | 240.0 | 1.000 | 1.000 | 0.0000754 | 0.0002313 | 0.0002798 | 0.0000744 |

MU = 339.5 (KN*H)

AUSGERTUNG VON 9.6.1978

VERHAELTNIS KI/KT I

M T M/MU T/TU STEIFIGKEITSVERHAELTNIS IM BEREICH ZWISCHEN SCHNITT

(KNM) (KNM) ---- I UND V V UND VII VII UND X X UND XIV

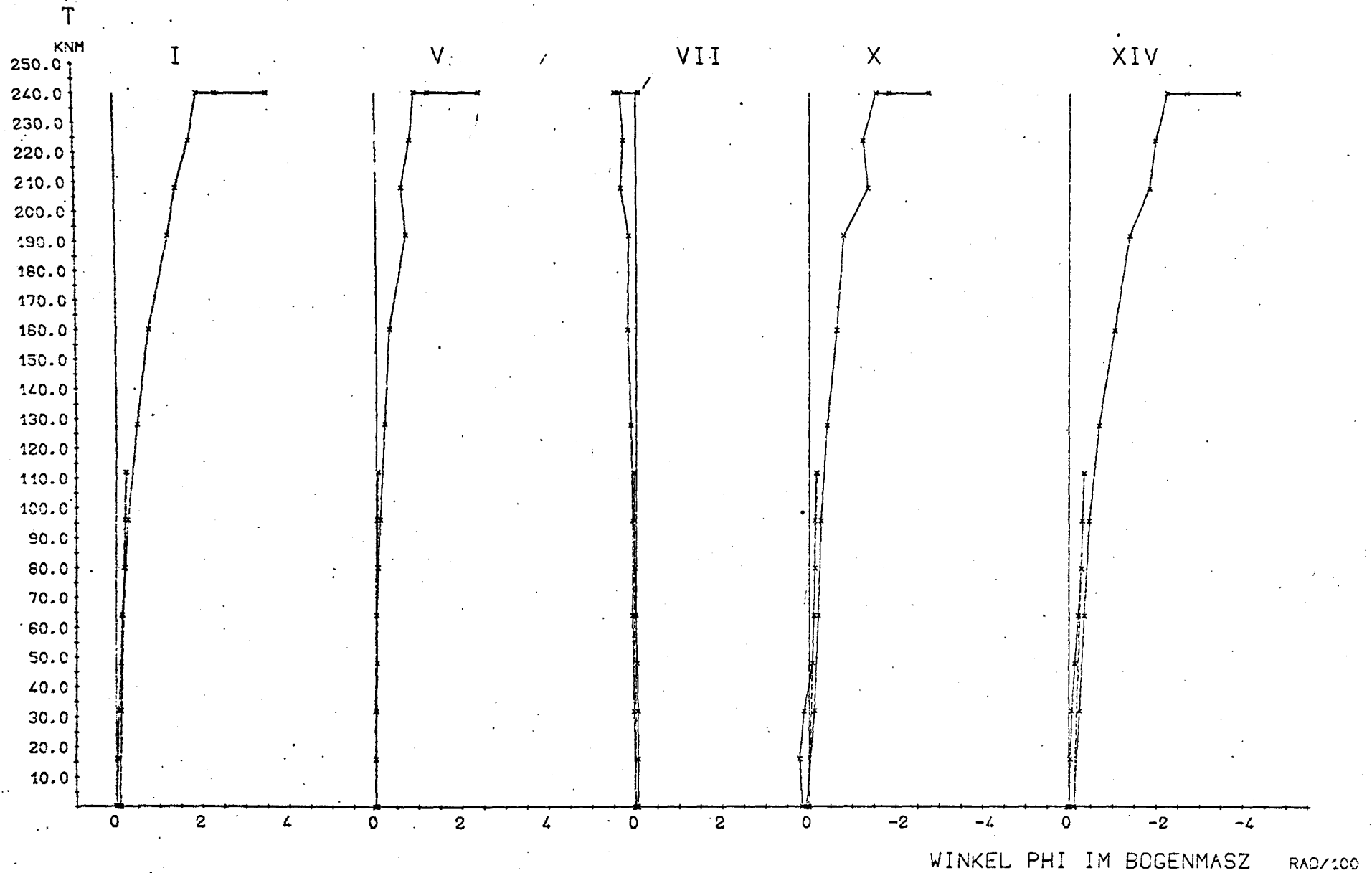
| | | | | | | | |
|-------|-------|-------|-------|-------|--------|--------|-------|
| 80.0 | 0.0 | 0.114 | 0.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| 160.0 | 0.0 | 0.229 | 0.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| 160.0 | 0.0 | 0.229 | 0.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| 240.0 | 0.0 | 0.343 | 0.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| 280.0 | 0.0 | 0.400 | 0.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| 320.0 | 0.0 | 0.457 | 0.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| 360.0 | 0.0 | 0.514 | 0.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| 400.0 | 0.0 | 0.571 | 0.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| 440.0 | 0.0 | 0.629 | 0.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| 480.0 | 0.0 | 0.686 | 0.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| 520.0 | 0.0 | 0.743 | 0.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| 560.0 | 0.0 | 0.800 | 0.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| 600.0 | 0.0 | 0.857 | 0.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| 0.0 | 0.0 | 0.000 | 0.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| 600.0 | 0.0 | 0.857 | 0.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| 600.0 | 16.0 | 0.857 | 0.067 | 0.689 | -0.299 | -0.061 | 0.066 |
| 600.0 | 32.0 | 0.857 | 0.133 | 0.853 | -1.195 | -0.249 | 0.177 |
| 600.0 | 48.0 | 0.857 | 0.200 | 0.672 | 1.000 | 0.351 | 0.495 |
| 600.0 | 64.0 | 0.857 | 0.267 | 0.618 | 1.000 | 0.569 | 0.607 |
| 600.0 | 80.0 | 0.857 | 0.333 | 0.605 | 0.622 | 0.585 | 0.540 |
| 480.0 | 80.0 | 0.686 | 0.333 | 0.553 | 0.622 | 0.635 | 0.521 |
| 400.0 | 80.0 | 0.571 | 0.333 | 0.515 | 0.711 | 0.695 | 0.521 |
| 280.0 | 80.0 | 0.400 | 0.333 | 0.540 | 0.766 | 0.728 | 0.546 |
| 280.0 | 96.0 | 0.400 | 0.400 | 0.560 | 0.874 | 0.853 | 0.572 |
| 280.0 | 112.0 | 0.400 | 0.467 | 0.627 | 0.820 | 0.836 | 0.627 |
| 70.0 | 112.0 | 0.100 | 0.467 | 0.591 | 0.697 | 0.709 | 0.704 |
| 0.0 | 0.0 | 0.000 | 0.000 | 0.591 | 0.697 | 0.709 | 0.704 |
| 300.0 | 0.0 | 0.429 | 0.000 | 0.591 | 0.697 | 0.709 | 0.704 |
| 600.0 | 0.0 | 0.857 | 0.000 | 0.591 | 0.697 | 0.709 | 0.704 |
| 600.0 | 32.0 | 0.857 | 0.133 | 0.299 | 0.398 | 0.385 | 0.271 |
| 600.0 | 64.0 | 0.857 | 0.267 | 0.459 | 0.419 | 0.405 | 0.484 |
| 600.0 | 96.0 | 0.857 | 0.400 | 0.532 | 0.351 | 0.381 | 0.507 |
| 600.0 | 128.0 | 0.857 | 0.533 | 0.456 | 0.268 | 0.323 | 0.466 |
| 600.0 | 160.0 | 0.857 | 0.667 | 0.364 | 0.215 | 0.257 | 0.403 |
| 600.0 | 192.0 | 0.857 | 0.800 | 0.371 | 0.152 | 0.214 | 0.330 |
| 600.0 | 208.0 | 0.857 | 0.867 | 0.263 | 0.149 | 0.144 | 0.436 |
| 600.0 | 224.0 | 0.857 | 0.933 | 0.250 | 0.139 | 0.164 | 0.311 |
| 600.0 | 240.0 | 0.857 | 1.000 | 0.242 | 0.128 | 0.141 | 0.357 |
| 660.0 | 240.0 | 0.943 | 1.000 | 0.216 | 0.096 | 0.122 | 0.292 |
| 700.0 | 240.0 | 1.000 | 1.000 | 0.216 | 0.070 | 0.058 | 0.219 |

MU = 339.5 (KNM)

SETMQ1

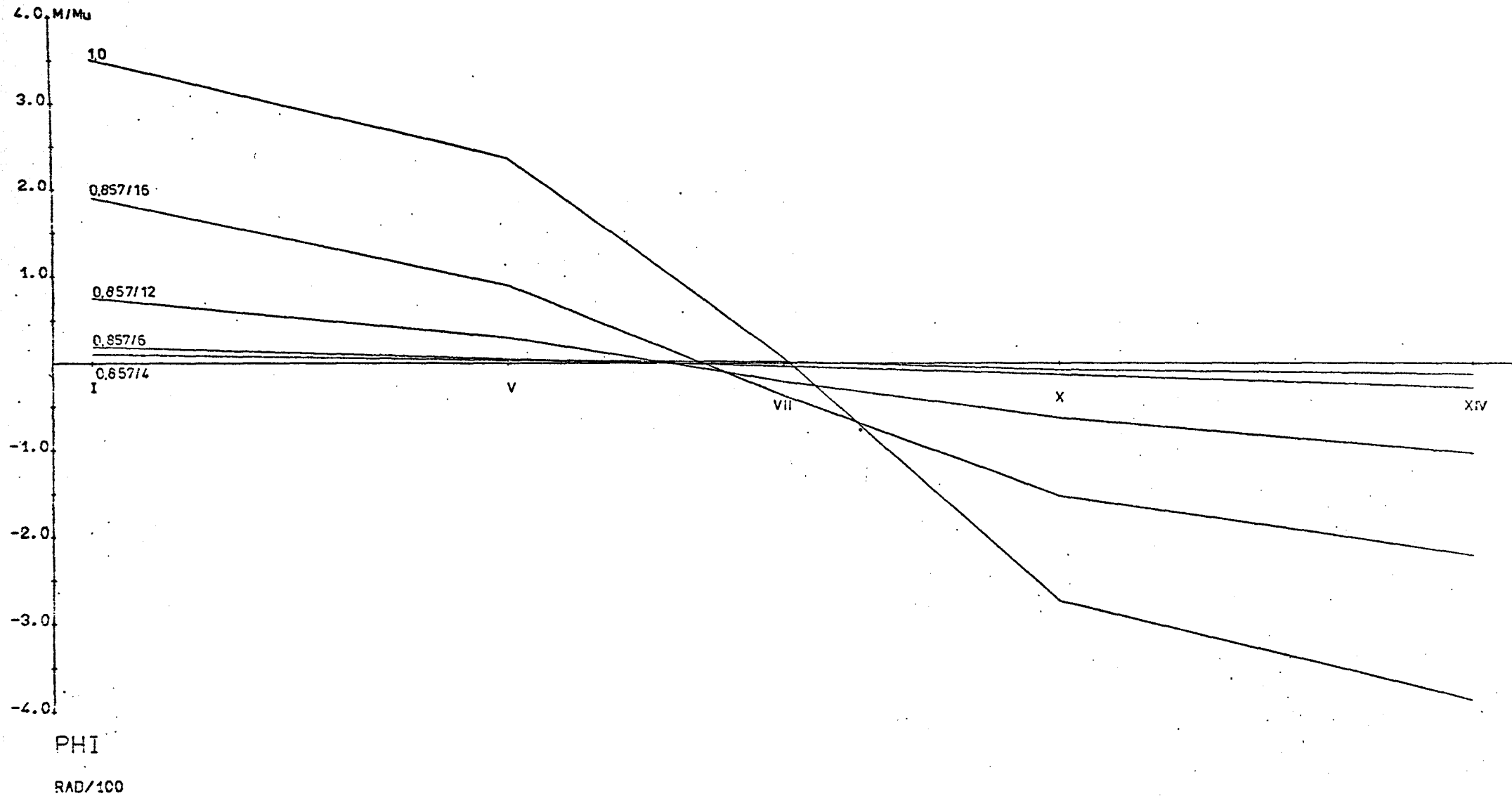
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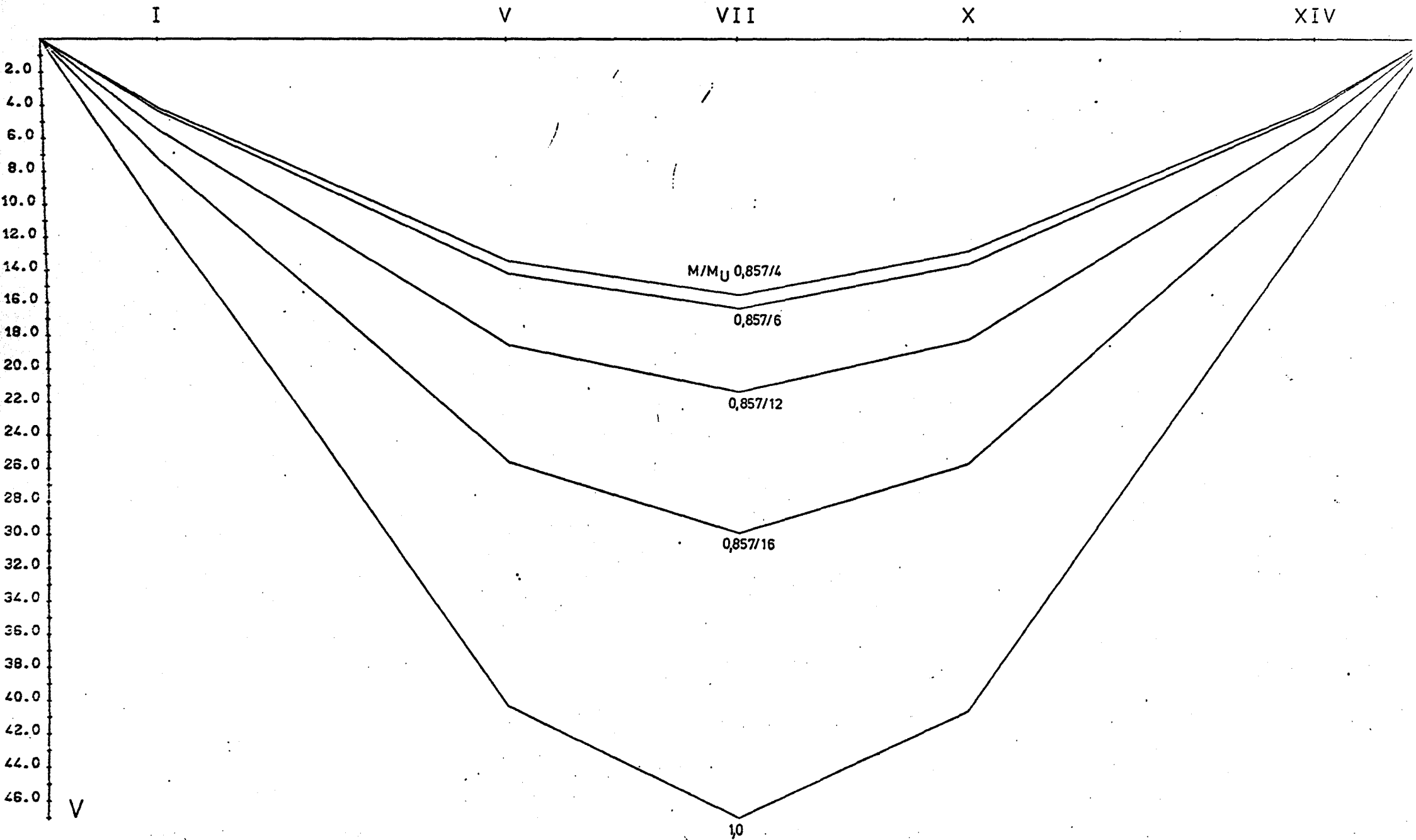
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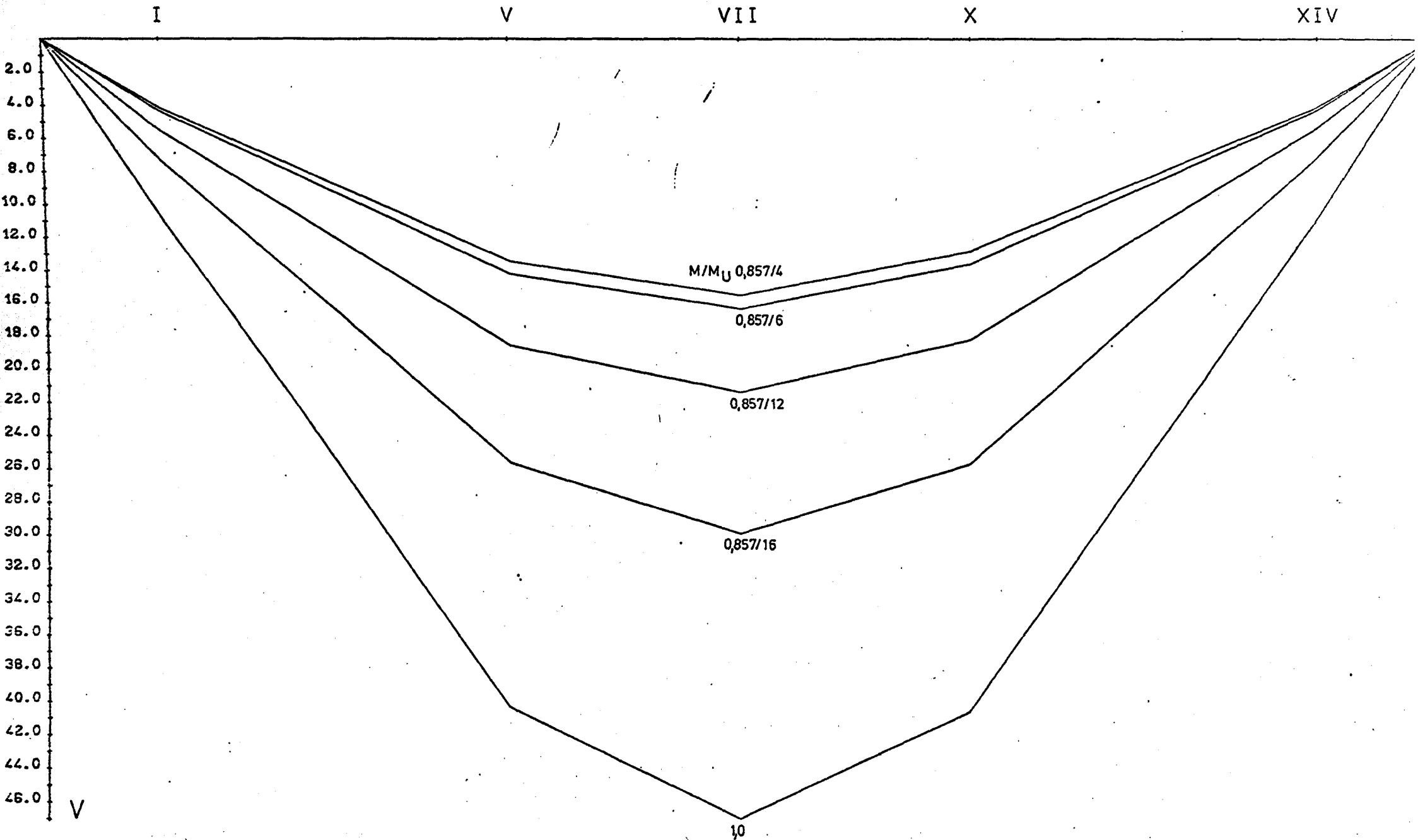


SETMQ1

QUERSCHNITTVERDREHUNG PHI ENTLANG DER BALKENLAENGESACHSE



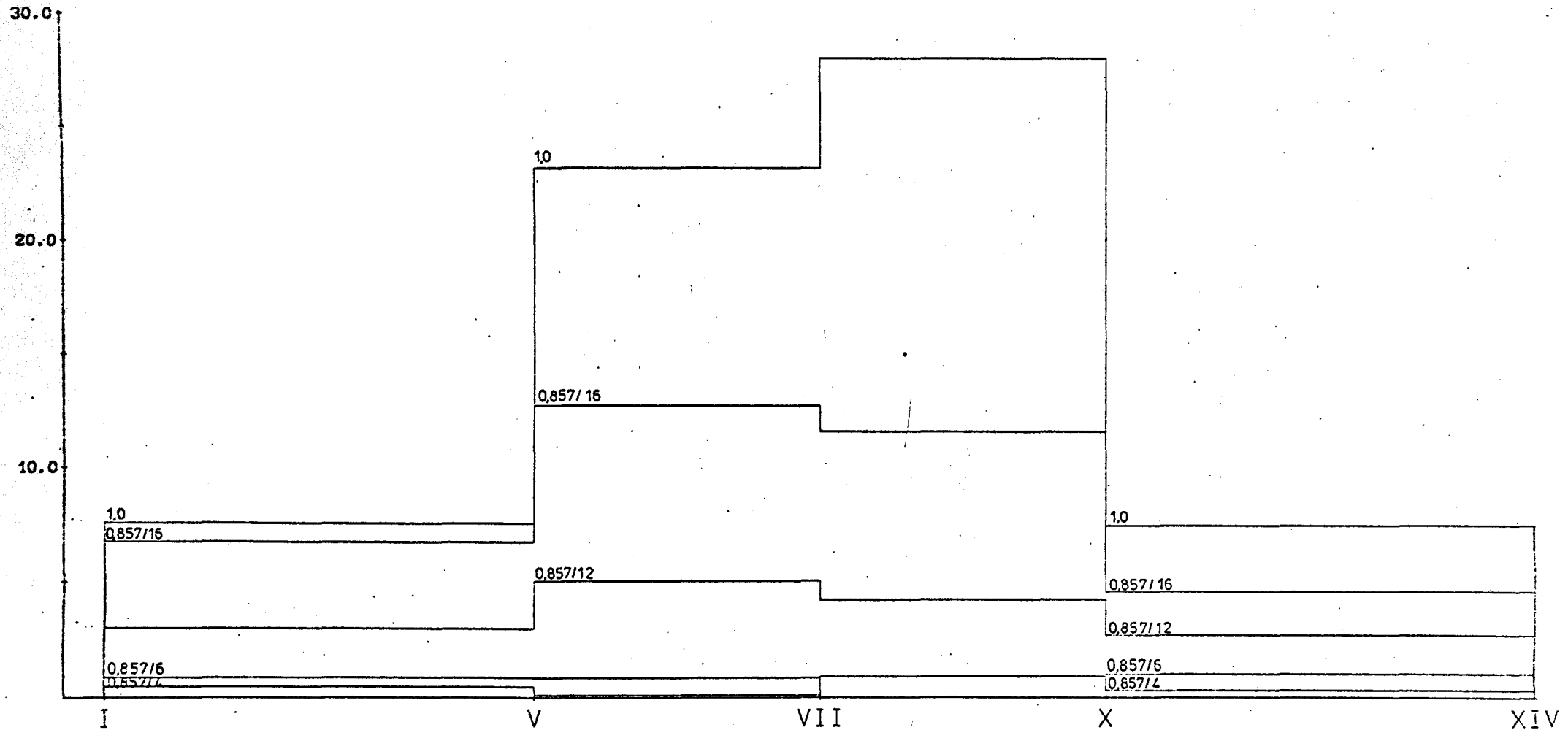




SETMQ1 BEZOGENE VERDREHUNG THETA ENTLANG DER BALKENLAENGSSACHSE

THETA

1/1



SETMQ1 TORSIONSSTEIFIGKEIT IN ABHAENGIGKEIT VOM BELASTUNGSGRAD

KT/KT1

